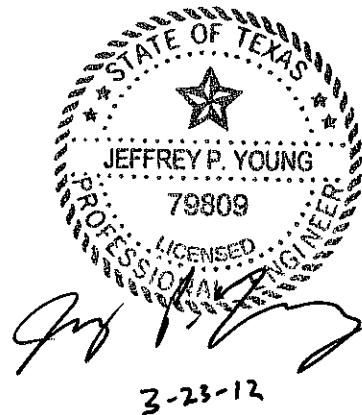


**CAMELOT LANDFILL
CITY OF LEWISVILLE, DENTON COUNTY
TCEQ PERMIT NO. MSW-1312B**

MAJOR PERMIT AMENDMENT APPLICATION

VOLUME 3 OF 6

Prepared for
City of Farmers Branch
March 2012



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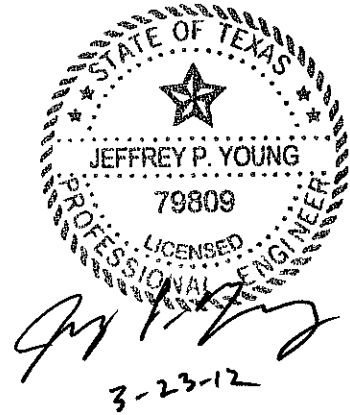
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**CAMELOT LANDFILL
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**MAJOR PERMIT AMENDMENT APPLICATION
VOLUME 3 OF 6**

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PART III – SITE DEVELOPMENT PLAN
APPENDIX III F – Surface Water Drainage Plan



**CAMELOT LANDFILL
CITY OF LEWISVILLE, DENTON COUNTY
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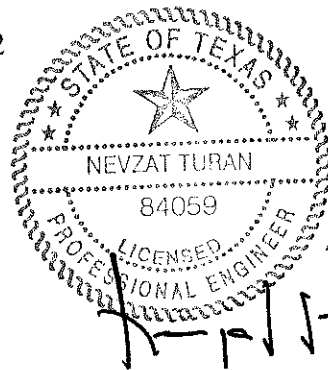
MAJOR PERMIT AMENDMENT APPLICATION

**PART III – SITE DEVELOPMENT PLAN
APPENDIX III F
SURFACE WATER DRAINAGE PLAN**

Prepared for

City of Farmers Branch

February 2012



2-28-12

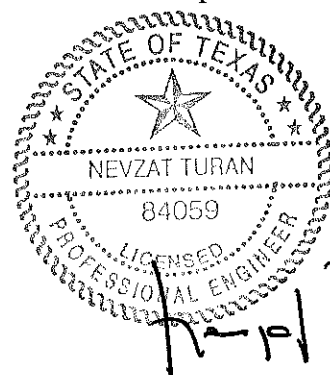
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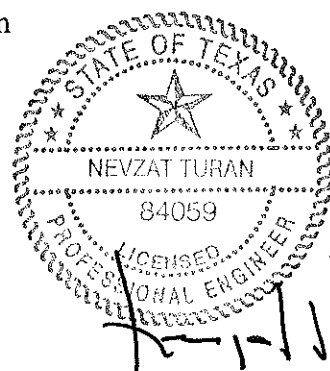
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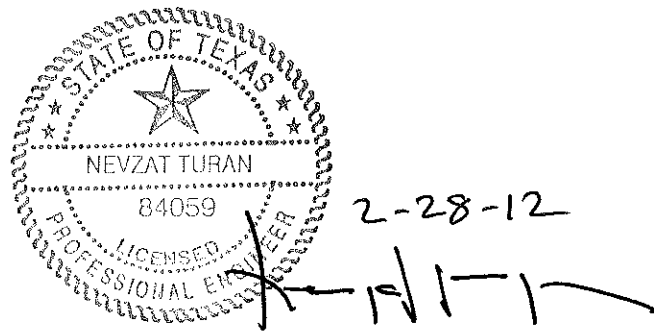
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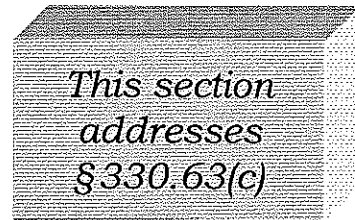
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1 INTRODUCTION

The Surface Water Drainage Plan is prepared as part of a permit amendment application for the Camelot Landfill consistent with Title 30 Texas Administrative Code (TAC) Chapter 330. This plan addresses surface water drainage design and erosion control. Permit level plans and details are presented for the proposed drainage system in this appendix. This appendix also includes a demonstration consistent with Title 30 TAC §330.305(a) that the proposed landfill development will not adversely alter permitted drainage patterns. Parts I/II, Section 11.1 and Appendix I/IIC include a demonstration showing that the site is in compliance with the floodplain location restriction. The 100-year floodplain as defined by the Federal Emergency Management Agency (FEMA) and the United States Army Corps of Engineer (USACE) is shown in Appendix IIIO. Appendix IIIO contains excerpts from the Conditional Letter of Map Revision (CLOMR) request and the Trinity River Corridor Development Certificate (CDC) application developed for the continued development of the Camelot Landfill.



This appendix includes the design of the final cover erosion layer and drainage structures (i.e., chutes and swales), perimeter drainage channels, detention ponds, as well as hydrologic calculations. Consistent with Title 30 TAC §330.63(c) and §330.305(b) and (c), these facilities are designed to convey run-off produced from the 25-year storm event. In addition, an Erosion Control Plan for all phases of landfill development is included in Appendix IIIF-F. All drainage facilities will be constructed and maintained in accordance with this plan.

This appendix also includes (Section 4) a demonstration that shows that the proposed landfill development will not adversely alter the existing permitted drainage patterns. As noted in Section 4, the proposed condition represents the proposed configuration of the site after the landfill has been completely developed. Consistent with Title 30 TAC §330.63(c)(1)(C), §330.63(c)(1)(D)(iii), and §330.305(a), the proposed completion condition is compared to the existing permitted condition to demonstrate that the continued development of the Camelot Landfill will not adversely alter the existing permitted drainage patterns.

To provide a complete comparison between the proposed condition and the existing permitted condition, the existing permitted condition was updated to include the expanded permit boundary and to incorporate analysis methods consistently accepted by the TCEQ. These updates are discussed in Section 4.

2 STORMWATER MANAGEMENT

2.1 Drainage System Layout

Stormwater runoff collected in swales located on the top dome and sideslopes of the landfill will be conveyed to drainage letdown structures (chutes) down the slopes to the perimeter channels. The perimeter channels collect runoff from drainage letdowns and conveys the runoff to stormwater detention ponds. The perimeter channels, will be constructed before fill is placed above existing grade in each adjacent landfill sector. The perimeter drainage system will be constructed in the general sequence shown on Parts I/II Drawings I/IIA-4 through I/IIA-7. As shown on Drawing IIIF.1 – Drainage Structure Plan, runoff generated from the majority of the developed areas will be discharged into one of three detention ponds to be attenuated before being discharged into the Elm Fork of the Trinity River (Elm Fork) or Midway Branch.

Pond P1 receives runoff from the northern portion of the developed landfill and discharges into a natural channel which conveys offsite flow from off-site Area O1 (refer to Figure 4.3 for off-site drainage areas) through an existing culvert under the landfill access road. This flow then merges with runoff from offsite Areas O1A, O2, and O3, and onsite Drainage Area S6 (refer to Figure IIIF.2 for onsite drainage areas), and exits the permit boundary at location DCP1 (refer to Figure 4.4). Off-site Drainage Area O4 merges with runoff from discharge point DCP1 in Midway Branch and re-enters the permit boundary from the east. Runoff from two drainage areas within the permit boundary (A6 and S8) merges with the flow in Midway Branch and exits the permit boundary again at discharge point DCP2.

Runoff from the remainder of the landfill development is collected in Ponds P2 and P3. Discharge from these ponds merges and exists the permit boundary to the south through an existing outfall channel directly into the Elm Fork at discharge point DCP3. Consistent with the existing permitted drainage layout, two post-development drainage areas, S9 and S10 (refer to Drawing IIIF.2), flow directly off the permit boundary into the Elm Fork at locations DCP5 and DCP4, respectively. Similarly, discharges at locations DCP6, DCP7, and DCP8 do not collect any runoff from the proposed landfill development and flow directly off the west side of the permit boundary, into offsite Drainage Area O5, and ultimately into the Elm Fork.

The facility has been designed to prevent discharge of pollutants into waters of the State or waters of the United States, as defined by the Texas Water Code and the Federal Clean Water Act, respectively. Camelot Landfill has a current Texas Pollution Discharge

Elimination System (TPDES) multi-sector general permit (MSGP) for industrial activity as stipulated under Section 402 of the Clean Water Act and under Chapter 26 of the Texas Water Code, the TPDES program. A copy of the multi-sector permit is included in Parts I/II, Appendix I/IIG. Any stormwater that has become contaminated by contact with the working face or with leachate will be handled in accordance with Appendix IIIC – Leachate and Contaminated Water Management Plan. The facility maintains a current Stormwater Pollution Prevention Plan prepared consistent with the provisions of TPDES MSGP TXR050000.

2.2 Erosion and Sedimentation Control Plan

The Camelot Landfill will use various interim and permanent erosion and sedimentation controls during all phases of site development to provide effective erosion stability for the external sideslopes and top dome surfaces. The interim controls will be used around active areas and external embankment sideslopes and top dome surfaces. These controls will include temporary letdown structures, soil berms, and seeding of intermediate cover areas to minimize the erosion potential. These interim controls will be used during all phases of landfill development to provide effective erosion stability for the external sideslopes and top dome surfaces until final cover is installed. Refer to Appendix IIIF-F – Erosion Control Plan for All Phases of Landfill Operation for more information.

Permanent controls include swales and chutes that will be constructed upon completion of the final cover installation. As part of the final cover construction, an erosion layer capable of sustaining vegetation will be constructed. Areas that receive final cover will be vegetated in accordance with Appendix IIIJ – Closure Plan upon completion of final cover placement. Final cover vegetation will protect the erosion layer soil against erosive runoff velocities. A soil loss and sheet flow velocity demonstration for the erosion layer is included in Appendix IIIF-D. The erosion layer will include a vegetation layer that provides for a 90 percent ground coverage, to keep soil loss below the required design values. If there are areas that do not maintain at least 90 percent vegetative coverage, vegetation in these areas will be reestablished to maintain at least 90 percent vegetative cover.

Erosion will be controlled by vegetation in drainage structures with flow velocities less than or equal to 5 feet per second (fps). For drainage structures with flow velocities greater than 5 fps, rock riprap, gabions, or other surface reinforcing materials as designed will be used for surface reinforcement.

During site development, non-structured and structural best management practices (BMPs) will be employed to control erosion and sedimentation ponds will be installed to prevent sediment discharge from the site. BMPs may include the use of temporary rock riprap, silt fences, straw bales, check dams, interceptor swales and berms, temporary and permanent seeding and sodding, surface roughening, matting and mulching, sediment traps, and surface wetting for dust control (refer to Appendix IIIF-F for more information).

Runoff volume (25-year, 24-hour storm event) from the active fill area (i.e., working face of the landfill operation) will be contained by the containment berm (refer to Part III, Appendix III C – Leachate and Contaminated Water Management Plan for details) to prevent potential discharge of contaminated runoff from the site.

2.3 Stormwater System Maintenance Plan

In accordance with Title 30 TAC §330.305(e)(1), the constructed stormwater systems such as channels, drainage swales, and chutes will be repaired and restored in the event of wash-out or failure from extreme storm events. Stormwater BMPs installed during all phases of landfill development will also be replaced or repaired in the event of failure. Excessive sediment will be removed, as needed, so that the drainage structures, such as the perimeter channels and detention ponds, function as designed. Site inspections by landfill personnel will be performed weekly or within 24 hours after any significant rainfall event of 0.5 inches or more, or as soon as the areas are accessible. Documentation of the inspection will be included in the Site Operating Record.

The following items will be evaluated during the inspections as further discussed in Appendix III F-F and Part IV – SOP:

- Erosion of daily and intermediate cover areas, final cover areas, perimeter ditches, chutes, swales, detention ponds, berms, and other drainage features.
- Settlement of intermediate cover areas, final cover areas, perimeter ditches, chutes, swales, and other drainage features.
- Silt and sediment build-up in perimeter ditches, chutes, swales, and detention ponds. Removed silt and sediment used as daily cover or to replenish intermediate cover soils.
- Obstructions in drainage features.
- Presence of erosion or sediment discharge at offsite stormwater discharge locations.
- Presence of sediment discharges along the site boundary in areas which have been disturbed by site activities.

Maintenance activities will be performed to correct damaged or deficient items noted during the site inspections. These activities will be performed as soon as possible after the inspection. The time frame for correction of damaged or deficient items will vary based on weather, ground conditions, and other site-specific conditions.

Maintenance activities will consist of the following, as needed:

- Vegetation reestablishment.

- Placement, grading, and stabilization of additional soils in eroded areas or in areas which have settled.
- Replacement or repair of riprap or other surface lining materials.
- Placement of additional riprap in eroded areas.
- Removal of obstructions from drainage features.
- Removal of silt and sediment build-up from drainage features.
- Repairs to erosion and sedimentation controls.
- Installation of additional erosion and sedimentation controls.

3 DRAINAGE SYSTEM DESIGN

3.1 Methodology

Drainage calculations for the final cover system erosion control structures and perimeter drainage system are based on the peak flow rates resulting from the 25-year frequency rainfall event for the area. The United States Army Corps of Engineers (USACE) HEC-1 computer program was used to compute peak flow rates produced from the design storm. The hydraulic methods employed in this study are consistent with those presented in the TCEQ *Guidelines for Preparing a Surface Water Drainage Report for Municipal Solid Waste Facility (RG-417, August 2006)* and TxDOT *Bridge Division Hydraulic Manual*, December 1985.

Water surface profiles were determined for the perimeter channels using the Channel Analysis Program (HYDROCALC HYDRAULICS Version 1.2a for Windows, Dodson & Associates, 1996) that is based on Manning's formula for uniform flow. The perimeter channels are designed to collect and route runoff from the 25-year frequency storm event to the detention ponds.

3.2 Hydrologic Analysis

3.2.1 Description of Computer Program

HEC-1 was developed by the USACE Hydrologic Engineering Center to simulate the surface runoff response of a watershed. The HEC-1 model represents a watershed as a network of hydrologic and hydraulic components. The modeling process results in the computation of stream-flow hydrographs at desired locations in the watershed. The hydrologic analysis for the post-development condition is presented in Appendix III F-A. The hydrologic analysis for the permitted landfill completion condition is included in Appendix III F-E.

3.2.2 Watershed Subareas and Schematization

The landfill areas that contribute flow to each detention pond were delineated into subareas to derive peak flow rates for the design of the perimeter channel and final cover drainage letdowns. Hydrographs are developed for each subarea and appropriately combined and routed through the swales and perimeter channels. The subareas are shown on Drawing III F.2 – Post-Development Drainage Area Plan as well as in Appendix III F-E for the permitted completion condition.

Offsite areas (areas outside the permit boundary) incorporated into the hydrologic analyses as appropriate have been delineated using topography obtained from the North Central Texas Council of Governments (NCTOG) compiled from aerial photography flown from January to March 2007. The offsite drainage area delineation is shown on Figure 4.3 for the post-development discharge analysis. The offsite areas are also included in the hydrologic analysis for the permitted landfill completion condition, as shown in Appendix III F-E.

3.2.3 Time Step

The time step, or the program computation interval, is the time interval at which the flow rates for the hydrographs are generated by the program. Time step used for a design storm event hydrograph generation is 5 minutes.

3.2.4 Hypothetical Precipitation

The hypothetical precipitation for the hydrologic analysis is consistent with the currently permitted hypothetical precipitation data. The hypothetical storm data was obtained from the National Weather Service (NWS) Technical Paper 40 (TP-40) (NWS, 1961) and NOAA Technical Memorandum NW3 Hydro-35 for the project area. For the design storm event analysis, a return period (frequency) of 25 years and a duration of 24 hours is used. The precipitation is assumed to be evenly distributed over the entire area modeled for each time interval.

3.2.5 Precipitation Losses

Precipitation losses (the precipitation that does not contribute to the runoff) are calculated using the Soil Conservation Service (SCS) Curve Number (CN) method. CN is a function of soil cover, land use, and antecedent moisture conditions. A CN of 86 was selected to represent the final cover sideslopes, and a CN of 84 was selected for final cover top dome surfaces. A CN of 100 was used for the detention pond areas. Further discussion on selection of CN values is provided in Appendices III F-A and III F-E for post-development and permitted landfill completion conditions, respectively.

3.2.6 Hydrograph Information

Two different types of hydrograph generation methods have been used in the drainage analyses: distributed runoff methods and the Snyder unit hydrograph method using the Espey "10-Minute" method for parameter estimation. Muskingum-Cunge and pond storage discharge methods were used for hydrograph routings. Example hydrograph development information for both distributed runoff and Snyder unit hydrograph methods is provided in Appendix III F-A.

Distributed Runoff Methods

The distributed runoff method (e.g., kinematic wave method) is applicable to small-water catchments with uniformly sloped overland flow plains that drain into channels. Landfill

final cover areas consist of relatively short (typically 120 feet on 4H:IV sideslopes) overland flow lengths that drain into landfill final cover swales. Distributed runoff estimation methods are applicable to landfill final cover areas because of the following:

- These methods were developed for uniform slopes that drain to collection channels. For a landfill final cover area, this translates to an overland flow segment of final cover that drains to a swale.
- These methods were developed for a network of relatively small drainage areas. Typically, to design the various perimeter channels, landfill drainage areas need to be subdivided to determine a peak flow at several points.
- These methods are also inherently conservative because it is based on watershed dimensions as opposed to other methods that use empirical information. Also, this method is conservative because flow attenuation is not accounted for.
- This method is also more conservative than the rational method because watershed lag time is computed as a function of real flow time without any limitations such as using a minimum time of concentration (i.e., 10 minutes), which is common practice for the rational method.

The kinematic wave method has been used for estimating peak runoff rates from the landfill final cover areas. A hydrograph from each drainage area with channelized flow (e.g., landfill final cover areas to swales) was developed using the kinematic wave method to simulate both overland and channelized flow. This method utilizes a simplified form of the energy equation and is based on the characteristics of the drainage area, swale, or channel. This method uses physical (measurable) characteristics (e.g., flow lengths, slopes, surface roughness coefficients, channel cross sections) of a watershed to estimate peak discharges.

Snyder Unit Hydrograph Method

The Snyder unit hydrograph method has been used mainly for non-landfill drainage areas (e.g., offsite drainage areas). The method is applicable to drainage areas with a wide range of characteristics. Several different methods have been developed to estimate Snyder unit hydrograph parameters (watershed lag and peaking coefficient). Espey “10-Minute” method was used in this project to estimate Snyder unit hydrograph parameters. The Espey “10-Minute” method was developed using flow records from 41 different watersheds in Texas and other states. The main advantage of the Espey “10-Minute” method is that it is one of the best methods for small-size drainage areas.

Hydrograph Routing

The Muskingum-Cunge Method (RD record in HEC-1) was used for routing of the flood wave through the drainage channels. This method is capable of accounting for hydrograph attenuation based on physical channel properties such as length, bottom slope, channel shape, and channel roughness.

Hydrographs at pond outlets were generated by routing the combined incoming flow hydrographs through the ponds. Pond routings (RS – Storage Routing record in HEC-1) were performed by using storage/elevation relationships for each pond by defining pond surface area versus depth. Additionally, discharge structure (low level outlet and spillway) characteristics of each pond are used for pond routing.

3.3 Hydraulic Analysis

3.3.1 Swale and Channel Analysis

Drainage structure details are illustrated on Drawings III F.9 through III F.12. The swales and channels are designed to convey the peak flow rate generated by the design storm event. These swales and channels will also reduce maintenance at the site after closure by minimizing erosion.

Hydraulic analyses of the swales and channels are conducted using Manning's uniform flow formula. The uniform flow assumption is applicable to long prismatic channels of uniform slope, as proposed at the site.

The general form of Manning's equation is

$$V = \frac{1.49 R^{0.667} S^{0.5}}{n}$$

in which

V = Velocity of flow, fps (feet per second)

n = Manning's "n" (unitless)

$R = \frac{A}{P}$ = Hydraulic radius, ft (feet)

S = Friction slope for nonuniform flow or channel slope for uniform flow, ft/ft

A = Area of water perpendicular to direction of flow, sf (square feet)

P = Wetted perimeter, ft.

Using the relationship

$$Q = VA$$

Manning's equation can be written as

$$Q = \frac{1.49 A R^{0.667} S^{0.5}}{n}$$

The uniform flow assumption equates the channel slope to the friction slope; therefore, the slope of the channel can be used for “S” in Manning's formula for computation of uniform flow.

Typical values for Manning's “n” are presented in the 2009 TXDOT *Bridge Division Hydraulic Manual* (“Suggested Manning’s Roughness Coefficients” Table, Chapter 6, Section 1). A value of 0.030 is used for “n” for swales, a value of 0.040 is used for gabion-lined chutes, and a value of 0.030 is used for perimeter channels. These values represent typical roughness coefficients to the proposed drainage structures, after vegetation has become established.

3.3.2 Drainage Letdown Structure (or Chute) Analysis

A typical chute detail is illustrated on Drawing III F.9. The final cover drainage letdown structures are designed to convey the flow rate generated by the design storm event. Hydraulic analysis of the letdown structures is conducted under the principles of tumbling flow. Tumbling flow is a function of channel slope, discharge, spacing and sizing of energy dissipating elements. The tumbling flow regime consists of a series of hydraulic jumps and overfalls that maintain critical velocity down the chute. The spacing and sizing of the energy dissipaters controls the velocity and flow of the water in the chutes, thereby reducing erosive conditions at slope transitions with the perimeter road low water crossings and chute/perimeter channel confluences.

Appendix III F-C presents calculations for the energy dissipaters.

3.3.3 Hydraulic Analysis of The Elm Fork Trinity River

A hydraulic analysis has been developed for the Elm Fork Trinity River as a part of the Conditional Letter of Map Revision (CLOMR) request and Corridor Development Certificate (CDC) application. As shown on Figure 4.6 and 4.7 Elm Fork forms the south side of the permit boundary.

The USACE Hydraulic Engineering Center’s River Analysis System (HEC-RAS) v.4.1.0 computer program was used for the hydraulic analysis of the Elm Fork (refer to Appendix III O for additional information). The analysis was developed for the 1-, 2-, 5-, 10-, 25-, 50- 100-, 500-year and standard project flood (SPF) frequency storm events. The 25-year and 100-year frequency storm flow rates used in the hydraulic analysis were obtained from FEMA and the USACE. Refer to Appendix III O for more information on the analyses performed on the Elm Fork.

4 DRAINAGE PATTERNS

Consistent with Title 30 TAC §330.63(c)(1)(C), §330.63(c)(1)(D)(iii), and §330.305(a), this section provides a demonstration showing that the proposed landfill development will not adversely alter the existing permitted landfill completion condition drainage patterns. The appendices containing the two drainage conditions analyzed are listed below.

- Appendix IIF-A (Post-Development Condition Hydrologic Calculations) – This appendix contains analysis and supporting calculations for the proposed configuration of the site after development of the expanded landfill is complete.
- Appendix IIF-E (Permitted Condition Hydrologic Calculations) – This appendix contains analysis and supporting calculations for the updated permitted configuration of the site and excerpts from the currently permitted drainage analysis. Section 4.3.1 includes a discussion of how the existing permitted drainage analysis has been updated to provide an equivalent comparison with the post-development condition.

The following three sections discuss: (1) regional drainage associated with the site; (2) site drainage patterns; (3) effect of the proposed development on peak flows, volumes, and velocities discharged from the site.

4.1 Regional Drainage Information

As shown on Figure 4.1, the 469.6-acre Camelot Landfill permit boundary is located approximately 2 miles south of Lake Lewisville. The Elm Fork Trinity River forms the southern boundary of the site. Midway Branch, a tributary of the Elm Fork, flows along the east side of the permit boundary.

Lake Lewisville is one of the largest man made surface water impoundments in Texas with a 46.24 square mile (25,592 acres) surface area at the crest elevation of the Lake Lewisville Dam. As shown on Figure 4.2, the Lake Lewisville watershed encompasses approximately 1,660 square miles. The total drainage area of the Elm Fork (which includes Prairie Creek and Stewart Creek) between Lake Lewisville Dam and the downstream end of the permit boundary is approximately 17 square miles. The permit boundary drainage area, which is comprised of the permit boundary and offsite areas discharging onto or directly receiving flow from the permit boundary, is 2.82 square miles (0.17 percent of the Elm Fork's drainage area upstream of the site).

The main influence on regional drainage patterns is the Lake Lewisville Dam. For example, the USACE operates the dam outlet structures, and their standard operating procedure is to close the outlet structures, during the 50-year and higher frequency storm events. As discussed in Section 4.3.5 and Appendix III O, the peak flow rates in the Elm Fork have been determined by the USACE for the Trinity River hydrologic model as a part of the development of the CDC permit application for the year 2050 (refer to Appendix III O for more information). A discussion of the effect of the continued development of the landfill on the 100-year floodplain is provided in the Section 4.3.5.

Figure 4.3 – Offsite Drainage Area Map shows the watershed associated with flows entering and leaving the permit boundary. The majority of the area within the permit boundary discharges south or west into the Elm Fork. A smaller portion of the area within the permit boundary drains east into Midway Branch and ultimately discharges into the Elm Fork approximately 200 feet southeast of the permit boundary.

4.2 Site Drainage Patterns

The permitted and proposed site drainage patterns are shown on Figure 4.4 – Site Drainage Patterns. As shown on Figure 4.4, the proposed drainage patterns are consistent with the currently permitted and updated permitted drainage patterns. The entire permit boundary drains directly into Elm Fork or through the Midway Branch into the Elm Fork of the Trinity River. The drainage patterns that include the individual outfalls at the permit boundary and individual runoff locations (locations where upstream offsite areas flow onto the permit boundary) for both the permitted and proposed conditions are the same. Run-on and runoff locations have been added or removed due to the expansion of the permit boundary relative to the existing permitted condition (i.e., removal of DCPN20 and addition of run-on Point DCP01). Runoff and run-on locations of the expanded permit boundary are the same for the updated permitted condition and the post-development condition. Also, the onsite drainage areas draining to Midway Branch and the Elm Fork under the proposed landfill completion conditions are consistent with the permitted conditions.

As shown on Figure 4.4, the total drainage area of the permit boundary is increased by 114.92 acres from the permitted condition to the updated permitted condition. This increase in the permit boundary allows for a direct comparison to be made between the two conditions. As shown in the onsite drainage area information on Figure 4-4, the updated permitted and proposed onsite drainage delineations are consistent.

Areas drain directly to the Elm Fork from discharge locations DCP3, DCP4, and DCP5 as shown on 4.4 for the permitted and proposed conditions. Discharge from DCP6, DCP7, and DCP8 traverses offsite Drainage Area O5 before discharging into the Elm Fork. The total drainage area to these six outfalls is comparable for the updated permitted (230.79 acres) and post-developed conditions (245.35 acres). Slight changes among the areas draining to these six outfall locations are shown on Figure 4.4. The difference in total drainage areas is due to changes in landfill final cover drainage areas (i.e., Areas 1, 2, and

3). In the proposed condition approximately 14 acres that were draining into Midway Branch have been diverted to drain into the Elm Fork.

As shown on Figure 4.4, discharge locations DCP1 and DCP2 discharge directly into Midway Branch. The Midway Branch converges with the Elm Fork approximately 200 feet south of discharge location DCP2. The total drainage area to the Midway Branch is 1,445.76 acres and 1,460.32 acres for the post-development and updated permitted conditions, respectively. The difference of 14.55 acres is the same difference in the total area flowing into the Elm Fork for the updated permitted and post-development conditions. In total, runoff from the same area, 1,691.11 acres, is discharged from the permit boundary for the updated permitted and post-development conditions. Note that Area O5 does not drain onto the permit boundary and is not included in the 1,691.11 acres discharging from the permit boundary. As mentioned above, changes to the design of the landfill final cover areas (i.e., Areas 1, 2, and 3) result in 14 acres of Midway Branch Drainage Area being diverted to drain to the Elm Fork.

4.3 Effect of Site Development on Drainage from the Site

The purpose of this section is to evaluate the peak flow rates, runoff volumes, and peak flow velocities of the existing permitted, updated permitted, and post-development hydrologic conditions. A summary of peak flow rates, runoff volumes, and peak flow velocities entering and exiting the permit boundary is provided in Table 4.1 and Figure 4.5 – Site Drainage Patterns, Runon/Runoff. Section 4.3.1 discusses the updates made to the currently permitted landfill completion condition drainage analysis to facilitate a complete and relevant comparison to be made between permitted and post-development landfill completion conditions.

Sections 4.3.2 through 4.3.5 discuss the impact of the proposed landfill conditions on peak flow rates, runoff volumes, and peak flow velocities entering and exiting the permit boundary.

4.3.1 Comparison of Existing Permitted and Updated Permitted Conditions

4.3.1.1 Purpose of the Updated Permitted Condition

As shown in Drawing 4.4, the drainage analysis included in TCEQ Permit No. 1312A (for the purpose of this appendix, this case will be designated the “existing permitted condition”) developed by Reed Engineering Group, Inc. in November 2000 utilizes a different landfill permit boundary and offsite drainage areas than those used in the post-development condition. An update to the existing permitted condition was necessary to allow an accurate comparison to be made with the results from the post-development condition. As noted in Section 1.2, to comply with Title 30 TAC §330.63(c)(1)(C), the proposed landfill completion condition is compared to the existing permitted condition of the landfill to demonstrate that the continued development of the landfill will not adversely alter the existing permitted drainage patterns. This comparison is only

meaningful if both the post-development and existing permitted conditions are based on consistent drainage information, including the same permit boundary. A discussion of the model parameters used in the existing permitted condition and the “updated permitted condition” is included in Section 4.3.1.2.

4.3.1.2 Model Parameter Comparison

Updates to the existing permitted condition are listed below.

- The landfill permit boundary was updated to the currently permitted landfill permit boundary. Changing the permit boundary requires that the offsite drainage areas must also be re-delineated to determine flow rates, volumes, and velocities entering and leaving the new permit boundary.
- Offsite Areas O1 through O5 were delineated for the updated permit boundary. As noted in Section 3.2.2, these offsite areas were delineated using the 2007 topography provided by NCTCOG.
- To be consistent with methods utilized in recently approved TCEQ applications, precipitation loss, hydrograph development, channel routing, and pond storage routing methods were updated as follows:
 - Curve numbers for all drainage methods were updated to 84 for most non-landfill drainage areas, 84 for landfill top dome surfaces, 86 for landfill side slope surfaces, and 100 for ponds based on tabulated curve numbers for the land uses of these areas (see Appendix III F-E). Curve numbers in the existing permitted condition are 80 for all non-landfill drainage areas, and 84 for landfill drainage areas.
 - Hydrographs are developed in the updated permitted landfill completion condition using distributed runoff methods or Snyder’s unit hydrograph, as discussed in Section 3.2.6. The existing permitted condition utilizes the SCS unit dimensionless hydrograph for all drainage areas.
 - The channel routing mechanism was updated to the Muskingum-Cunge Method for all channels, and routing through the Elm Fork or Midway Branch was removed from the HEC-1 Model.
 - Pond routing is accomplished using the storage routing method, with storage/elevation data, and spillway and low-water outlet information input into HEC-1. The existing permitted condition utilized unverified (storage/elevation supporting information was not cited) rating curves for pond routing.
- The drainage area delineation for the currently permitted final cover drainage letdowns has been updated to model top dome surfaces and sideslope areas separately to better represent the final cover drainage areas. This update provides more accurate flow rates for the top dome area drainage letdown structures.

4.3.1.3 Comparison of Peak Flows at the Permit Boundary

As shown in Figure 4.4, discharges to the east of the permit boundary at locations DCP1 and DCP2 for the existing and updated permitted conditions are different due to the addition of over 1.5 square miles of offsite drainage areas. Offsite flows from DCPO3 are approximately equal for the existing and updated permitted condition. The discharge at location DCP3 is higher in the updated permitted condition by 41 cfs, and is attributable to the change in Pond Routing Methodology. Flow rates at locations DCP4, DCP5, DCP6, and DCP7 are lower for the updated permitted condition.

4.3.2 Peak Flow Rates

As shown on Figure 4.5 and in Table 4-1, the peak flow rates entering the permit boundary from DCPO1, DCPO2, and DCPO3 are identical for the updated permitted and post-development conditions. The peak flow rate for DCPO3 is higher for the existing permitted condition. After leaving the permit boundary at DCP1, stormwater re-enters the permit boundary at location DCPO4. Peak flow rates are not comparable at this location between the existing permitted and the updated permitted or post development conditions due to the addition of over 1,200 acres in the latter two conditions. The peak flow rate for the post-development condition at location DCPO4 is 6 cfs (0.2%) lower than the updated permitted condition. This difference is due in part to the slightly lower total drainage area and the larger detention area (Pond P1) in the post-development condition.

As noted above, stormwater that enters the site from an off-site area and stormwater that is generated from within the permit boundary discharges at eight separate locations along the permit boundary (DCP1, DCP2, DCP3, DCP4, DCP5, DCP6, DCP7, and DCP8 as shown on Figure 4.4). At these discharge points, the peak flow rates from the 25-year frequency storm event that are discharged from the site for the post-development condition are all less than the updated permitted conditions. This reduction in the peak flow rates is due to the additional detention provided by the addition of Pond P3 and the slightly different delineation of drainage areas (due to the slight difference between permitted and in-place drainage channels and Pond P2).

The 25-year peak flow rate in the Elm Fork at the upstream and downstream limits of the site shown on Figure 4.5 and Table 4-1 is 8,900 cfs. This flow rate is provided in the CDC hydraulic model for Elm Fork Trinity River (refer to Appendix IIIIO for peak flow rate, velocity, and other information). The peak flow rates in the CDC model were developed based on a year 2050 expected region-wide watershed development scenario.

4.3.3 Volumes

As shown in Table 4-1, the volumes entering the permit boundary are consistent for the updated permitted and post-development landfill conditions (the volume increase for the site is 10 ac-ft or 1.26%). The increase in the runoff volume for the entire site is a result of the final cover improvements and additional detention pond area for which a CN of 100 is used. This volume increase is insignificant, because the reduced peak flow rate

results in a better regulated release of the increased storm volume. Runoff volume calculations are provided in Appendices III F-A and III F-E.

4.3.4 Velocities

A summary of the 25-year frequency storm peak flow velocities that enter and exit the site are shown on Table 4-1. As shown, the velocities at each discharge point are equal or lower for the post-development condition compared to the permitted conditions. This is due to the lower flow rates, given that the cross-sectional area at each drainage outfall remains unchanged. Velocity calculations are provided in Appendices III F-A and III F-E for the post-development and permitted conditions, respectively.

4.3.5 Floodplain

Because of the nature of the Trinity River as a major drainage conduit in heavily developed areas, development within the Trinity River corridor is regulated by the ACOE and FEMA. As a part of this application, a CDC permit and CLOMR request were developed and submitted to the ACOE and FEMA, respectively. The effective models for the region around the permit boundary are maintained independently by FEMA and ACOE, however there are only very small differences in the effective models.

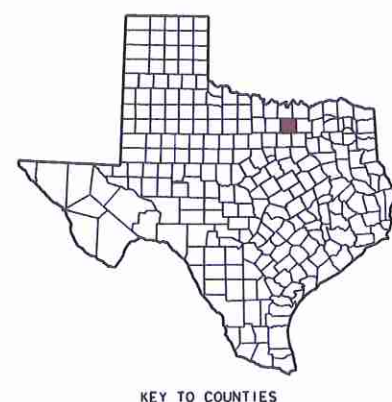
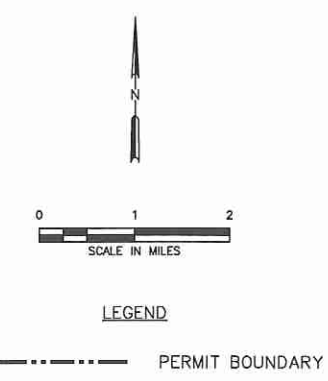
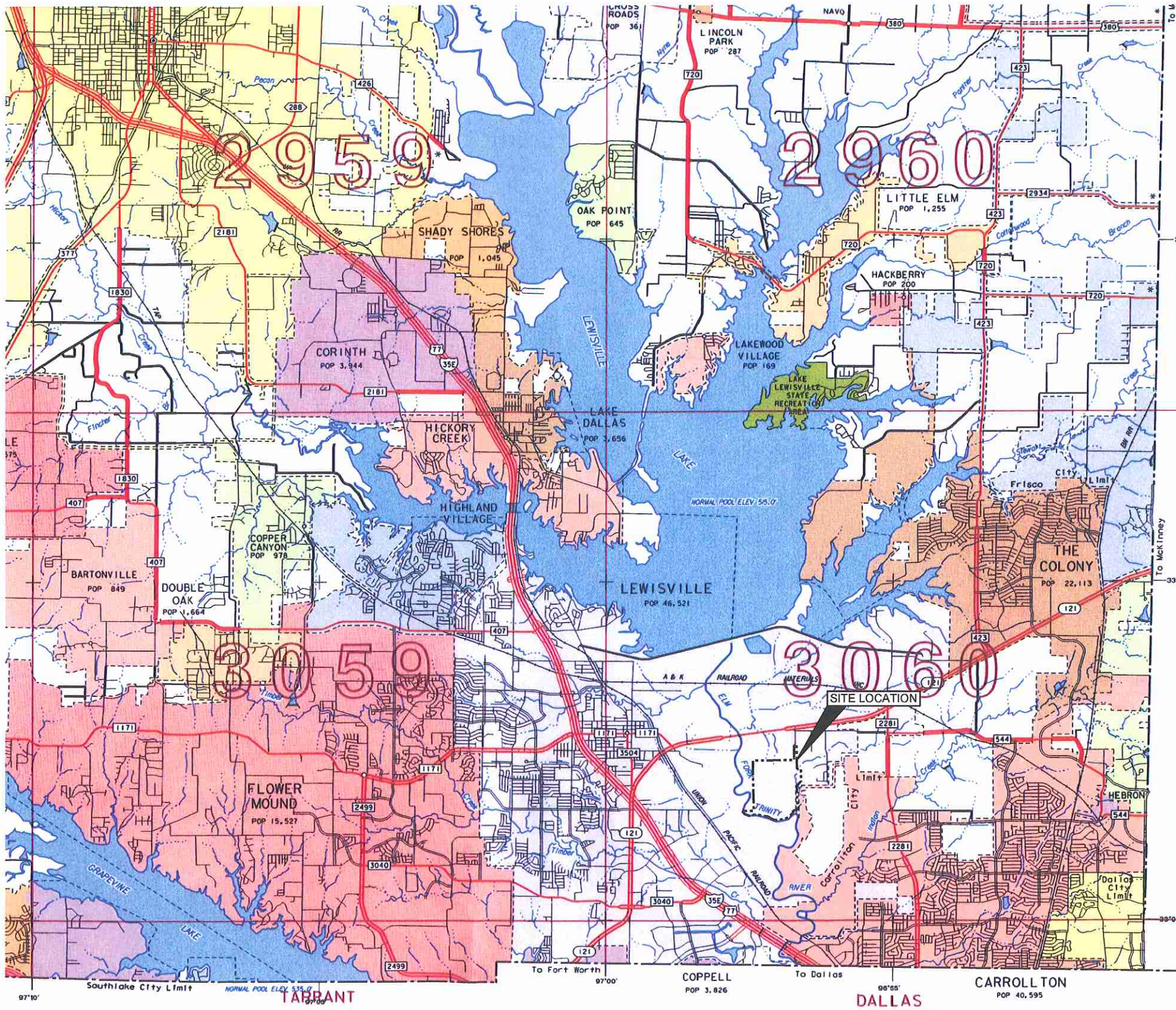
A comparison of the floodplain elevations for both the currently permitted landfill configuration and the proposed landfill expansion configuration using both the CDC and CLOMR models are presented in Table 4-2. As shown in Table 4-2, the floodplain elevations for the Elm Fork during the 100-year storm are generally unaffected due to the proposed landfill expansion. Creation of additional floodplain valley storage in the area between the landfill and the Elm Fork results in a very slight decrease in flood plain elevations in some of the cross sections. To meet the CDC requirements, the amount of floodplain valley storage created has to be more than the amount of existing valley storage consumed. In this case, the valley storage is increased by over 106 acre-feet for the 100-year storm event because of the development of the landfill.

From this analysis, it is concluded that the proposed landfill development will not adversely alter the floodplain of the Elm Fork. This conclusion is supported by the City of Lewisville, the USACE, and FEMA's approval of the proposed project and resulting 100-year floodplain delineation. Approval letters are included in Appendix III O.

4.4 Summary

From the hydrologic evaluations of the updated permitted and proposed conditions, the existing drainage conditions at the permit boundary will not be adversely altered by the proposed development. Given that: (1) drainage patterns are not adversely altered, (2) total design stormwater peak discharge rate at the permit boundary is less than the permitted total stormwater peak discharge rate (and the post-development peak flows entering the site are less than or equal to the updated permitted peak flows entering the

site), (3) the hydrograph time to peak at the permit boundary is not significantly altered for the proposed landfill expansion, (4) total volume of stormwater entering and leaving the permit boundary is not significantly altered, (5) there is no increase in velocity at the permit boundary, (6) the stormwater discharge outfall locations are consistent with the permitted configuration, and (7) the permitted floodplain is not increased at the permit boundary and the limits of waste is at a minimum of 3 feet above the corresponding floodplain elevation, it is concluded that the proposed landfill development will not adversely alter permitted drainage patterns consistent with Title 30 TAC 330.63(c)(1)(C), §330.63(c)(1)(D)(iii), and §330.305(a).



GENERAL HIGHWAY MAP DENTON COUNTY TEXAS

PREPARED BY THE
TEXAS DEPARTMENT OF TRANSPORTATION
TRANSPORTATION PLANNING AND PROGRAMMING DIVISION
IN COOPERATION WITH THE
U.S. DEPARTMENT OF TRANSPORTATION
FEDERAL HIGHWAY ADMINISTRATION

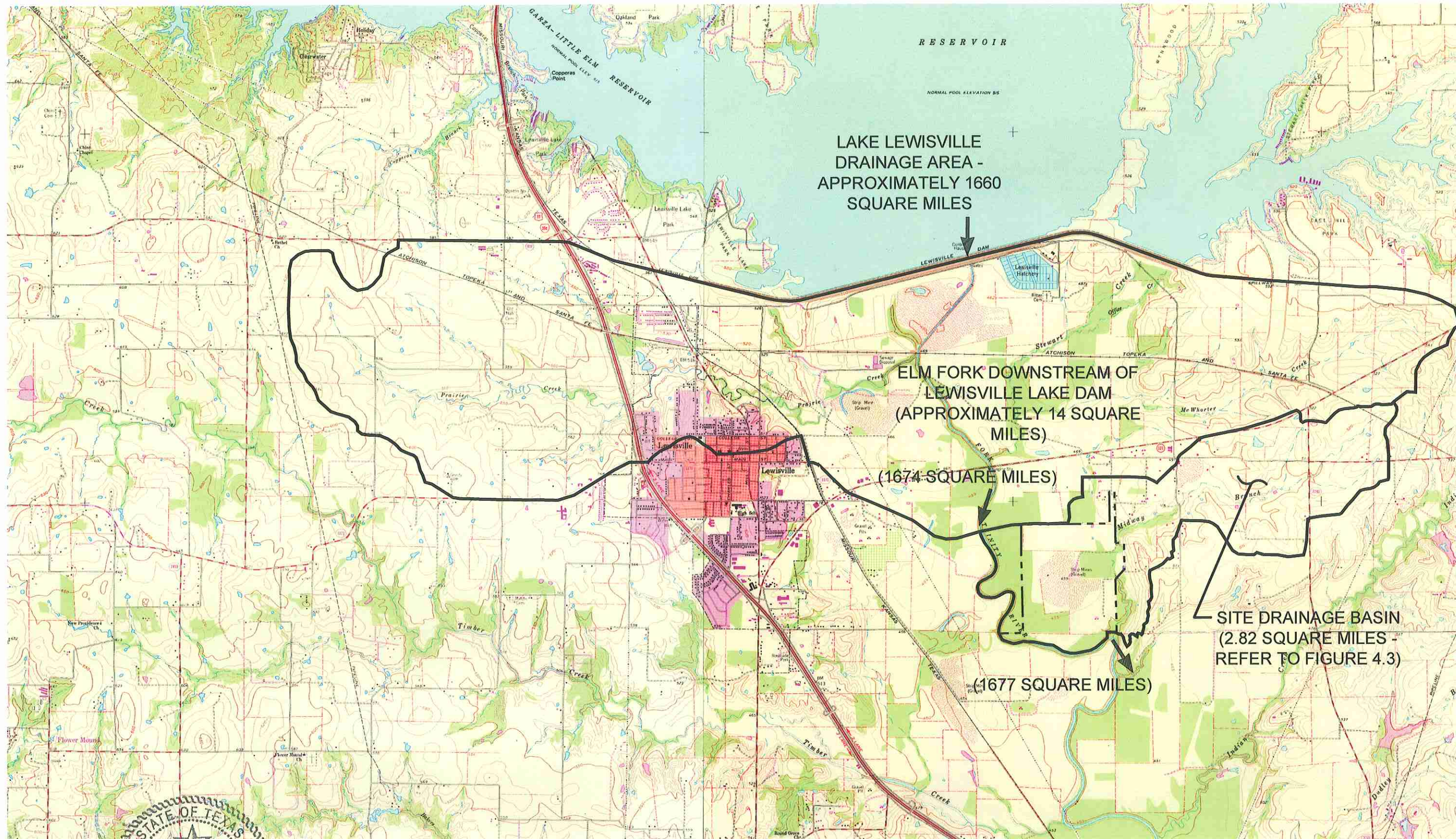


1990
1990 CENSUS FIGURES
HIGHWAYS REVISED TO
NOTICE
This map has been prepared for internal use within the Texas Department of Transportation. Accuracy is limited to the validity of available data as of dates shown.

2-28-12

O:\1039\351\EXPANSION 2009\PART III-SDB\JHP\4.1-SITE LOCATION MAP.dwg, jwilson, 1:2

<input type="checkbox"/> DRAFT <input checked="" type="checkbox"/> FOR PERMITTING PURPOSES ONLY <input type="checkbox"/> ISSUED FOR CONSTRUCTION <input type="checkbox"/> CLIENT APPROVAL BY:	PREPARED FOR CITY OF FARMERS BRANCH	MAJOR PERMIT AMENDMENT SITE LOCATION MAP CAMELOT LANDFILL DENTON COUNTY, TEXAS <i>Weaver Boos Consultants</i> TBPE REGISTRATION NO. F-3727 <small>CHICAGO, IL FORT WORTH, TX GRIFFITH, IN NAPERVILLE, IL (817) 735-9770 SOUTH BEND, IN COLUMBUS, OH SPRINGFIELD, IL DENVER, CO ST. LOUIS, MO</small>												
DATE: 02/2012 FILE: 1339-351-11 CAD: 4.1-SITE LOC MAP.DWG	DRAWN BY: VRS DESIGN BY: CRM REVIEWED BY: JPY													
REUSE OF DOCUMENTS <small>THIS DOCUMENT, AND THE DESIGNS INCORPORATED HEREIN, AS AN INSTRUMENT OF PROFESSIONAL SERVICE, IS THE PROPERTY OF WEAVER BOOS CONSULTANTS, LLC - SOUTHWEST AND IS NOT TO BE USED IN WHOLE OR IN PART, WITHOUT THE WRITTEN AUTHORIZATION OF WEAVER BOOS CONSULTANTS, LLC - SOUTHWEST.</small>		REVISIONS <table border="1"> <thead> <tr> <th>NO.</th> <th>DATE</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> </tbody> </table>	NO.	DATE	DESCRIPTION									
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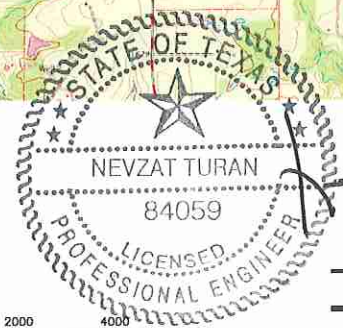
LAKE LEWISVILLE DRAINAGE AREA - APPROXIMATELY 1660 SQUARE MILES

ELM FORK DOWNSTREAM OF LEWISVILLE LAKE DAM (APPROXIMATELY 14 SQUARE MILES)

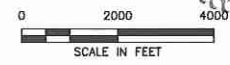
(1674 SQUARE MILES)

(1677 SQUARE MILES)

SITE DRAINAGE BASIN (2.82 SQUARE MILES - REFER TO FIGURE 4.3)



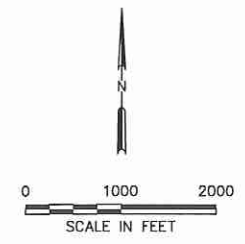
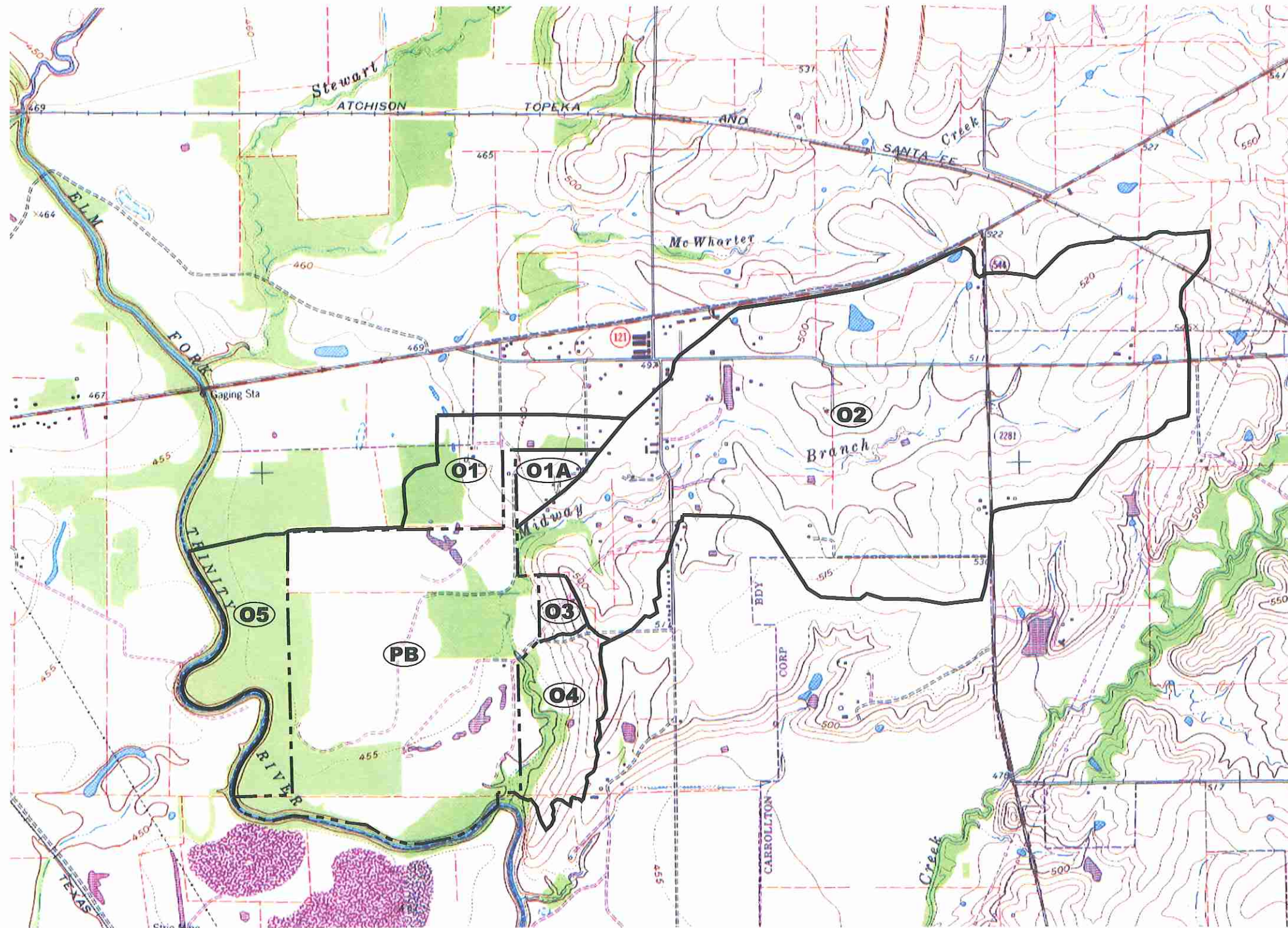
2-28-12
 17/1
 LEGEND
 --- PERMIT BOUNDARY
 ——— DRAINAGE AREA BOUNDARY



NOTES:

1. TOPOGRAPHIC MAP SHOWN IS THE USGS 7.5 MINUTE QUADRANGLE MAPS: LEWISVILLE WEST, TEXAS PRINTED 1960 (PHOTOREVISED 1968) LEWISVILLE EAST, TEXAS PRINTED 1960 (PHOTOREVISED 1968)
2. WATERSHED BOUNDARIES SHOWN ONLY FOR THE AREAS DOWNSTREAM OF THE LEWISVILLE DAM AND ARE APPROXIMATED BY USING USGS TOPOGRAPHIC MAP.

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	CITY OF FARMERS BRANCH													
DATE: 02/2012 FILE: 1339-351-11 CAD: 4.2-REG WATERSHED.DWG	DRAWN BY: VRS DESIGN BY: CRM REVIEWED BY: JPY	REVISIONS <table border="1"> <thead> <tr> <th>NO.</th> <th>DATE</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> </tr> </tbody> </table>	NO.	DATE	DESCRIPTION									
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LEGEND

--- PERMIT BOUNDARY

— DRAINAGE AREA BOUNDARY

○ DRAINAGE AREA LABEL

DRAINAGE AREA NO.	AREA (ACRES)
01	87.5
01A	23.4
02	1,008.4
03	16.2
04	86.0
05	116.5
PB	462.6
TOTAL	1,807.6

ROAD CLASSIFICATION

Heavy-duty ——— Light-duty ———

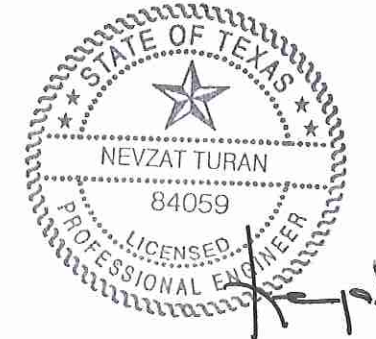
Medium-duty ——— Unimproved dirt ———

○ Interstate Route ○ U.S. Route ○ State Route

LEWISVILLE EAST, TEX.
 SW/4 FRISCO 15' QUADRANGLE
 N3300-W9652.5/7.5

1960
 PHOTO REVISIED 1968
 AMS 6650 111 SW-SERIES V882

- NOTES:**
- DRAINAGE AREA DELINEATION WITHIN THE PERMIT BOUNDARY IS INCLUDED IN APPENDICES III F-A AND III F-E.
 - TOPOGRAPHY PROVIDED BY USGS 7.5 MINUTE QUADRANGLE TOPOGRAPHIC MAP (LEWISVILLE EAST, TX, PHOTO REVISED 1981).



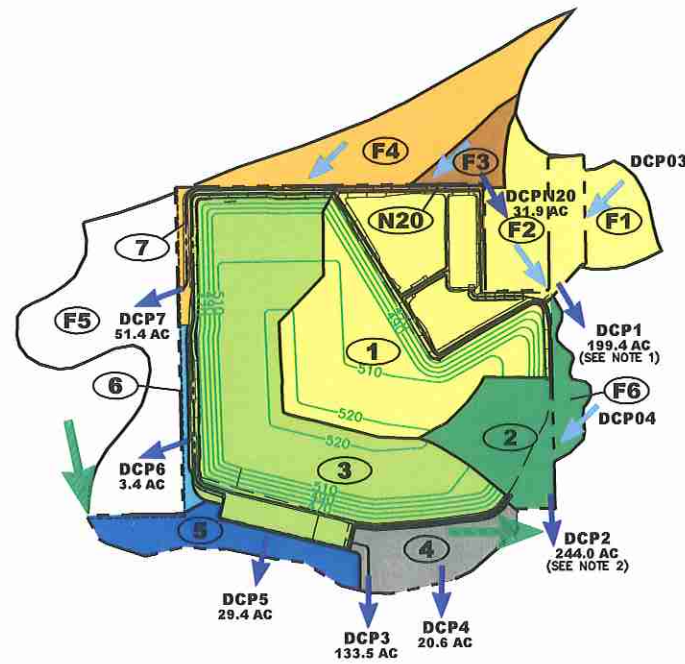
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 2-28-12

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	DATE: 02/2012 FILE: 1339-351-11 CAD: 4.3 OFFSITE DRAINAGE.DWG		DRAWN BY: VRS DESIGN BY: CRM REVIEWED BY: JPY	REVISIONS <table border="1"> <thead> <tr> <th>NO.</th> <th>DATE</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> </tr> </tbody> </table>	NO.	DATE	DESCRIPTION				
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<small>COPYRIGHT © 2012 WEAVER BOOS CONSULTANTS, LLC - SOUTHWEST. ALL RIGHTS RESERVED.</small>		CHICAGO, IL FORT WORTH, TX GRIFFITH, IN <small>NAPERVILLE, IL (817) 735-9770 SOUTH BEND, IN COLUMBUS, OH SPRINGFIELD, IL DENVER, CO ST. LOUIS, MO</small>									

FIGURE 4.3

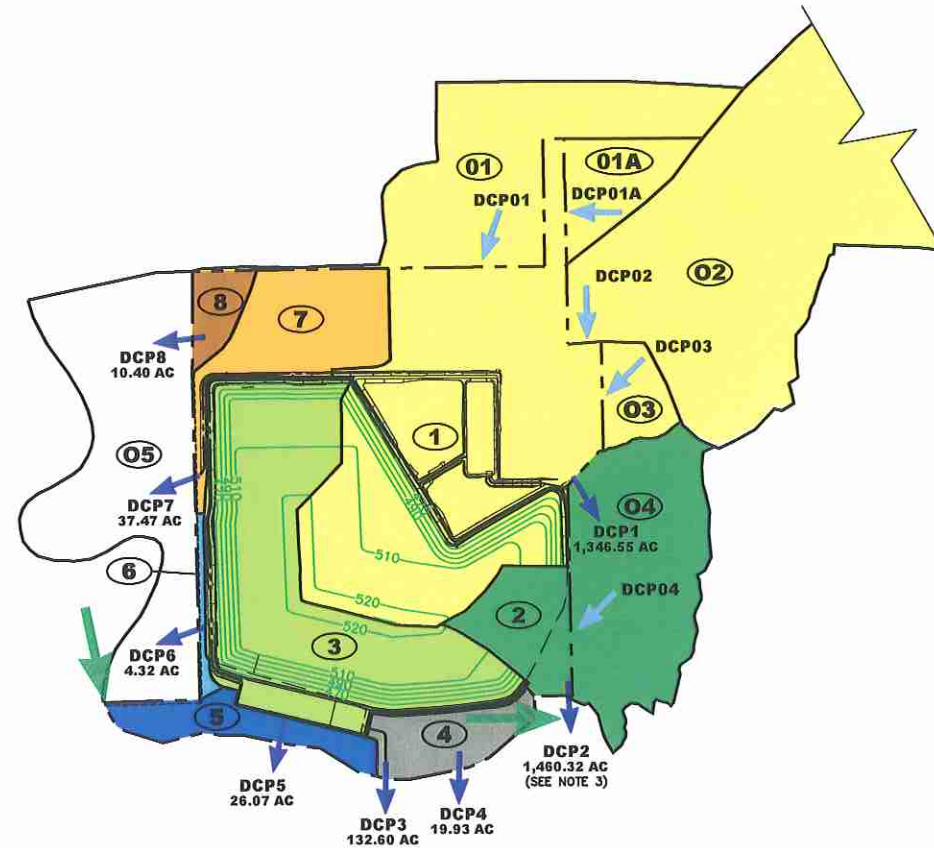
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D:\1339\051\EXPANSION 2009\PART III-SDP\III-4-SITE DRAINAGE PATTERNS.dwg, jwilson, 1:2



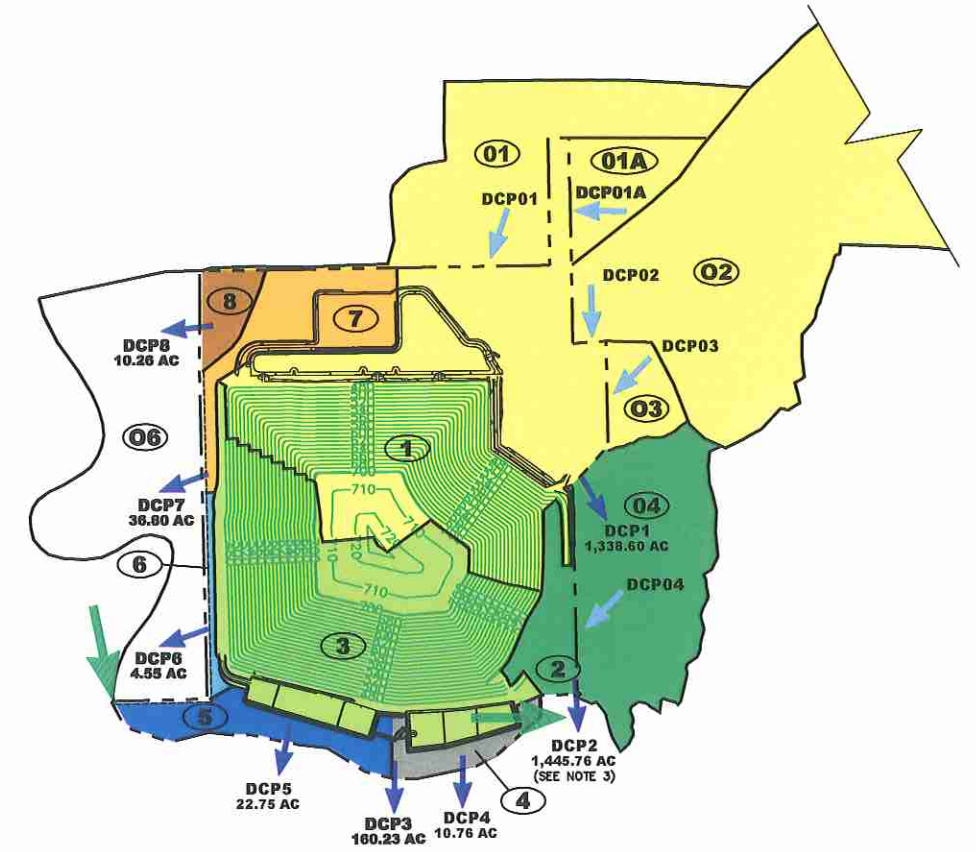
EXISTING PERMITTED CONDITION

- ON-SITE AREAS (SEE NOTE 5)**
- 1 = 131.3 ACRES
 - 2 = 27.5 ACRES
 - 3 = 133.5 ACRES
 - 4 = 20.6 ACRES
 - 5 = 29.4 ACRES
 - 6 = 3.4 ACRES
 - 7 = 6.5 ACRES
 - N20 = 2.5 ACRES
- PERMIT BOUNDARY TOTAL = 354.7 ACRES
- OFF-SITE AREAS (SEE NOTE 5)**
- F1 = 16.0 ACRES
 - F2 = 20.2 ACRES
 - F3 = 29.4 ACRES
 - F4 = 44.9 ACRES
 - F5 = 81.0 ACRES
 - F6 = 17.1 ACRES
- OFF-SITE TOTAL = 208.6 ACRES
- GRAND TOTAL = 563.3 ACRES



UPDATED PERMITTED CONDITION

- ON-SITE AREAS**
- 1 = 211.10 ACRES
 - 2 = 27.73 ACRES
 - 3 = 132.60 ACRES
 - 4 = 19.93 ACRES
 - 5 = 26.07 ACRES
 - 6 = 4.32 ACRES
 - 7 = 37.47 ACRES
 - 8 = 10.40 ACRES
- PERMIT BOUNDARY TOTAL = 469.62 ACRES
- OFF-SITE AREAS**
- O1 = 87.47 ACRES
 - O1A = 23.42 ACRES
 - O2 = 1,008.38 ACRES
 - O3 = 16.18 ACRES
 - O4 = 86.04 ACRES
 - O5 = 116.47 ACRES
- OFF-SITE TOTAL = 1,337.96 ACRES
- GRAND TOTAL = 1,807.58 ACRES

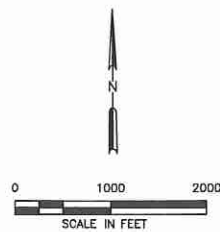


POST-DEVELOPMENT CONDITION

- ON-SITE AREAS**
- 1 = 203.15 ACRES
 - 2 = 21.12 ACRES
 - 3 = 160.23 ACRES
 - 4 = 10.76 ACRES
 - 5 = 22.75 ACRES
 - 6 = 4.55 ACRES
 - 7 = 36.80 ACRES
 - 8 = 10.26 ACRES
- PERMIT BOUNDARY TOTAL = 469.62 ACRES
- OFF-SITE AREAS**
- O1 = 87.47 ACRES
 - O1A = 23.42 ACRES
 - O2 = 1,008.38 ACRES
 - O3 = 16.18 ACRES
 - O4 = 86.04 ACRES
 - O5 = 116.47 ACRES
- OFF-SITE TOTAL = 1,337.96 ACRES
- GRAND TOTAL = 1,807.58 ACRES

LEGEND

- PERMIT BOUNDARY
- PERMITTED / PROPOSED FINAL COVER CONTOUR
- DRAINAGE AREA DESIGNATION
- DRAINAGE AREA BOUNDARY
- UPLAND DRAINAGE ENTERING THE SITE
- STORMWATER DISCHARGE POINT
- FLOW IN THE ELM FORK ENTERING/EXITING THE SITE



NOTES:

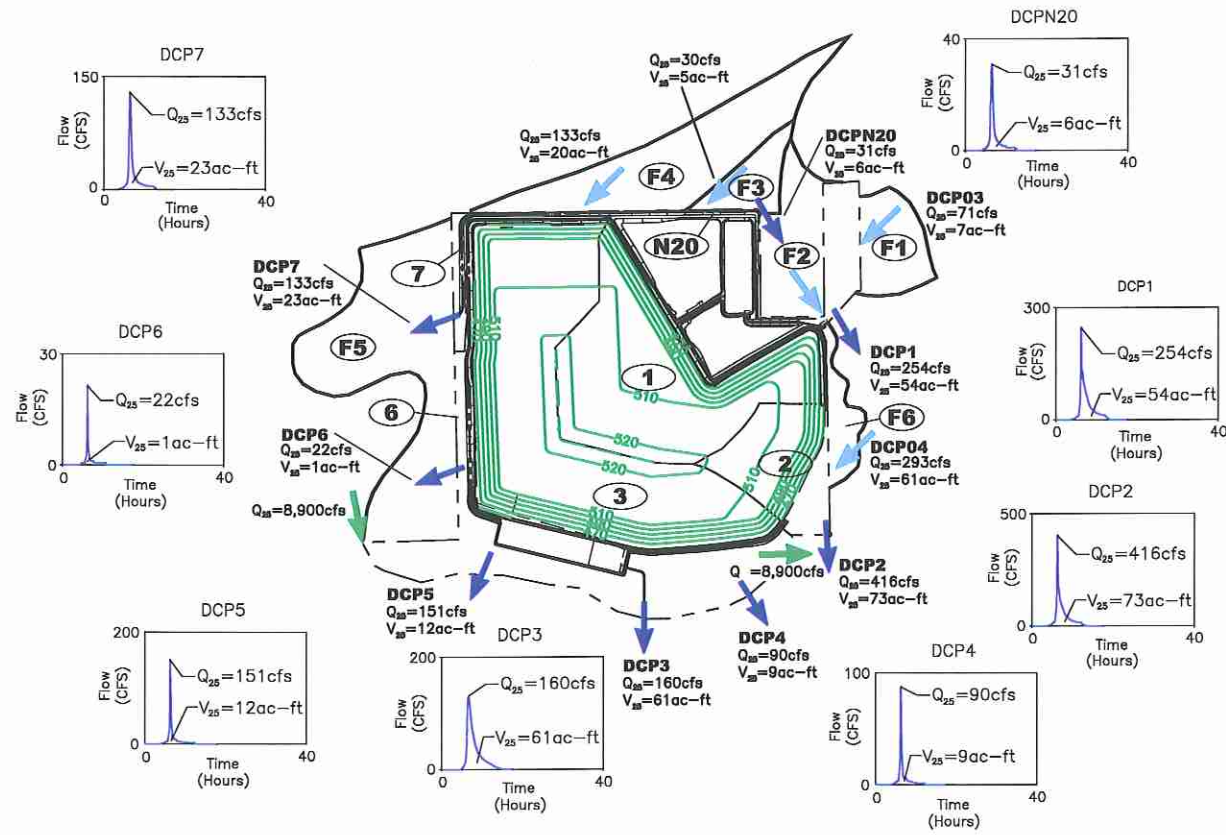
1. DCP1 AREA INCLUDES THE 31.9 ACRES DRAINING FROM DCPN20.
2. DCP2 AREA INCLUDES THE 199.4 ACRES DRAINING FROM DCP1.
3. DCP2 AREA INCLUDES THE 1,346.55 ACRES DRAINING FROM DCP1.
4. DCP2 AREA INCLUDES THE 1,338.60 ACRES DRAINING FROM DCP1.
5. AREAS SHOWN ARE OBTAINED FROM ATTACHMENT 6B-2 AND THE HEC-1 MODEL INCLUDED IN THE SDP FOR TCEQ PERMIT NO. MSW-1312A.



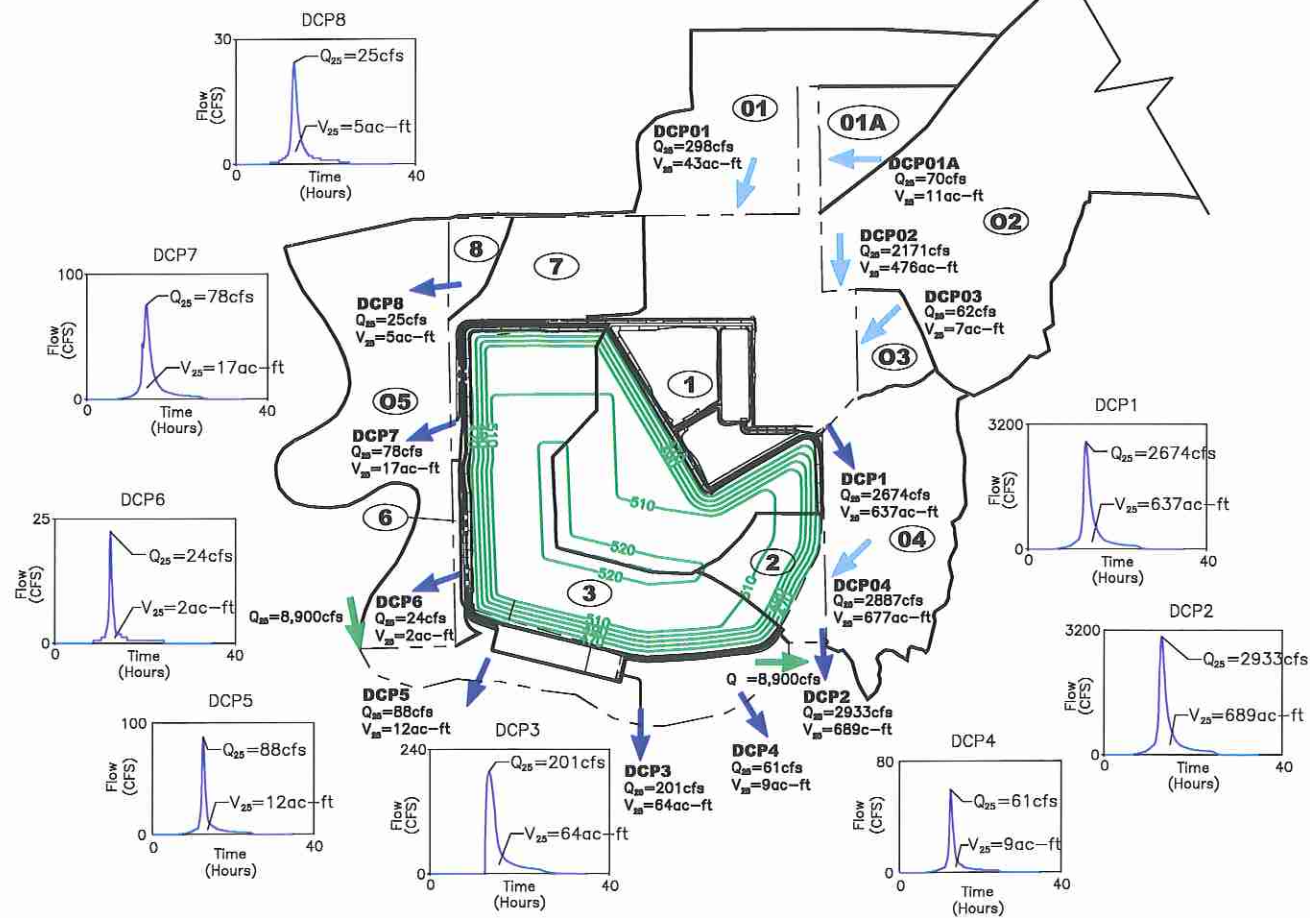
Handwritten signature and date: 2-28-12

<input type="checkbox"/> DRAFT <input checked="" type="checkbox"/> FOR PERMITTING PURPOSES ONLY <input type="checkbox"/> ISSUED FOR CONSTRUCTION <input type="checkbox"/> CLIENT APPROVAL BY: _____	PREPARED FOR CITY OF FARMERS BRANCH		MAJOR PERMIT AMENDMENT SITE DRAINAGE PATTERNS CAMELOT LANDFILL DENTON COUNTY, TEXAS <i>Weaver Boos Consultants</i> TBPE REGISTRATION NO. F-3727											
	DATE: 02/2012 FILE: 1339-351-11 CAD: 4.4-DRAINAGE PATTERNS.DWG	DRAWN BY: VRS DESIGN BY: CRM REVIEWED BY: JPY		REVISIONS <table border="1"> <thead> <tr> <th>NO.</th> <th>DATE</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> </tbody> </table>	NO.	DATE	DESCRIPTION							
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<small>CHICAGO, IL NAPERVILLE, IL COLUMBUS, OH DENVER, CO</small>		<small>FORT WORTH, TX (817) 735-9770</small>	<small>GRIFFITH, IN SOUTH BEND, IN SPRINGFIELD, IL ST. LOUIS, MO</small>											
			FIGURE 4.4											

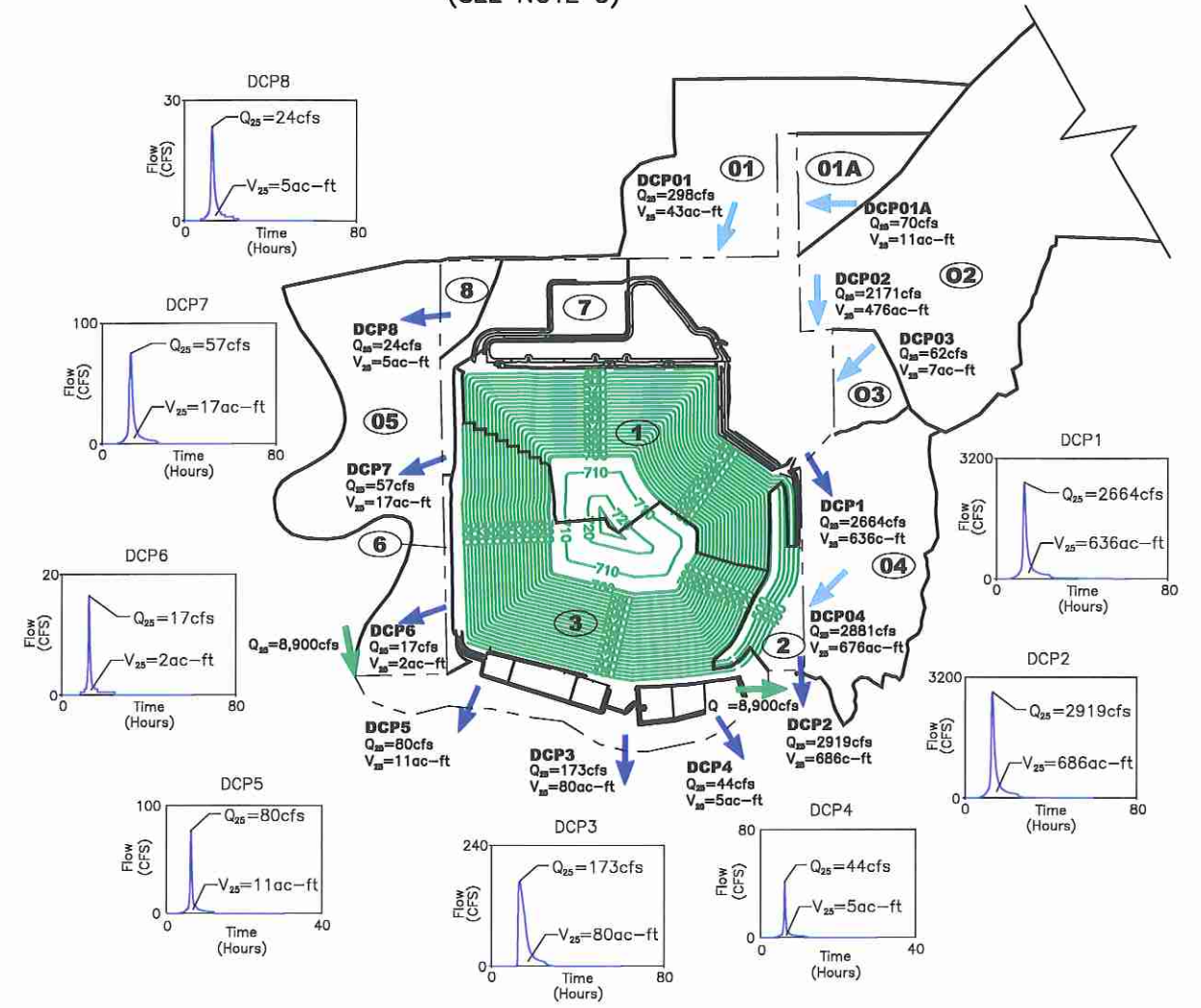
EXISTING PERMITTED CONDITION
(SEE NOTE 1)



UPDATED PERMITTED CONDITION
(SEE NOTE 2)



POST-DEVELOPMENT CONDITION
(SEE NOTE 3)



LEGEND

- PERMIT BOUNDARY
- 520 PERMITTED / PROPOSED FINAL COVER CONTOUR
- ① DRAINAGE AREA DESIGNATION
- UPLAND DRAINAGE ENTERING THE SITE
- STORMWATER DISCHARGE POINT
- DCP3 Q₂₅=201cfs V₂₅=64ac-ft
- FLOW IN THE ELM FORK ENTERING/EXITING THE SITE (SEE NOTE 4)

NOTES:

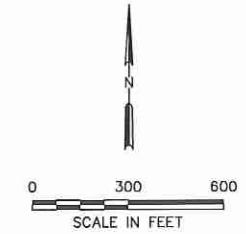
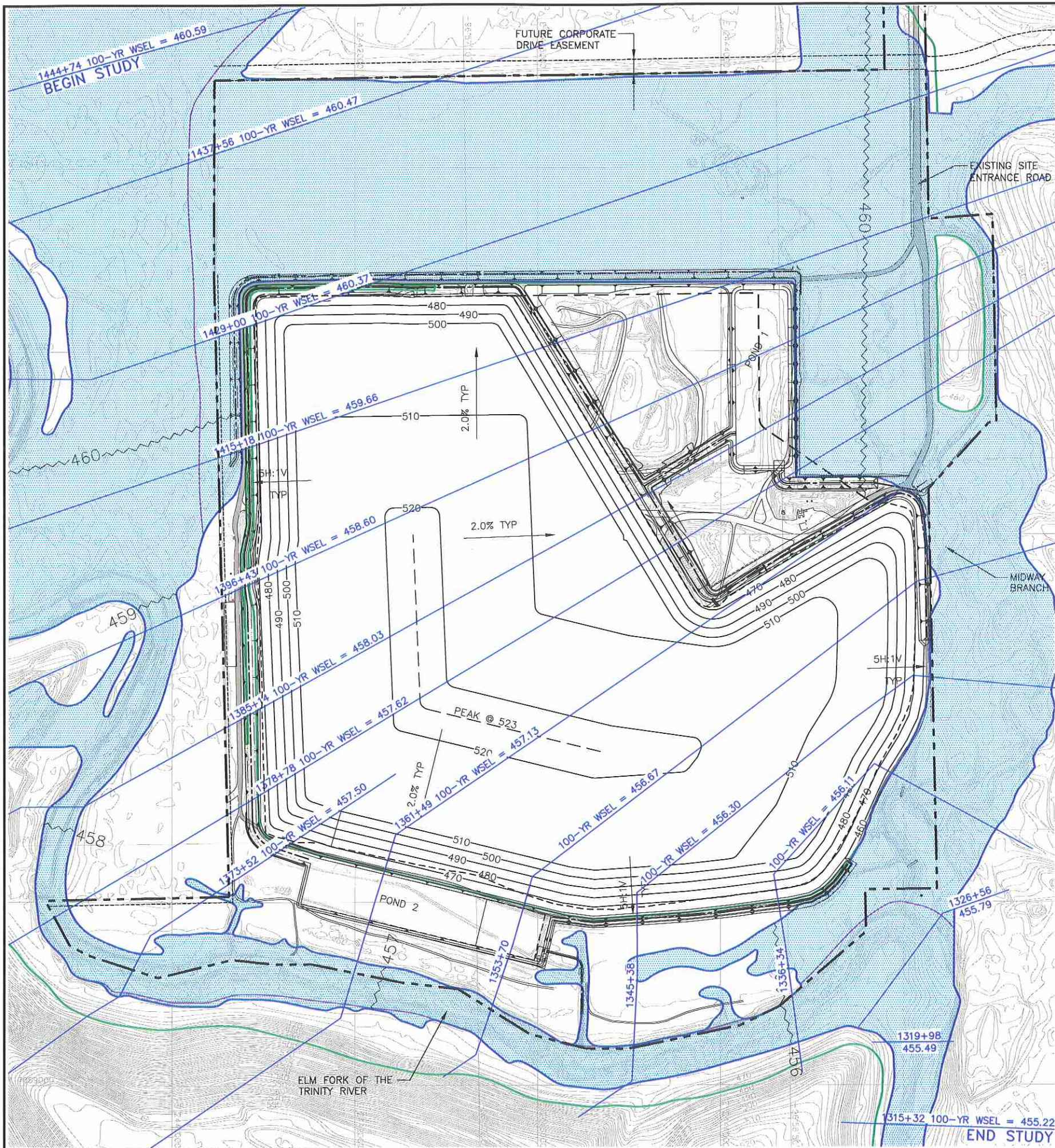
1. PEAK FLOW RATES AND VOLUMES SHOWN ARE OBTAINED FROM ATTACHMENT 6B-2 AND THE HEC-1 MODEL INCLUDED IN THE SDP FOR TCEQ PERMIT NO. MSW-1312A.
2. HYDROLOGIC INFORMATION FOR THE 25-YEAR LANDFILL UPDATED PERMITTED CONDITION IS PROVIDED IN APPENDIX III F-E.
3. HYDROLOGIC INFORMATION FOR THE 25-YEAR LANDFILL POST-DEVELOPMENT CONDITION IS PROVIDED IN APPENDIX III F-A.
4. FLOW RATES WITHIN THE ELM FORK ARE REPRODUCED FROM THE CDC HYDRAULIC MODEL FOR ELM FORK TRINITY RIVER. REFER TO APPENDIX III O FOR MORE INFORMATION.



2-28-12

<input type="checkbox"/> DRAFT <input checked="" type="checkbox"/> FOR PERMITTING PURPOSES ONLY <input type="checkbox"/> ISSUED FOR CONSTRUCTION <input type="checkbox"/> CLIENT APPROVAL BY:		PREPARED FOR CITY OF FARMERS BRANCH		MAJOR PERMIT AMENDMENT SITE DRAINAGE PATTERNS RUNOFF CAMELOT LANDFILL DENTON COUNTY, TEXAS													
DATE: 02/2012 FILE: 1339-351-11 CAD: 4.5-RUNON-RUNOFF.DWG		DRAWN BY: VRS DESIGN BY: CRM REVIEWED BY: JPY		REVISIONS <table border="1"> <thead> <tr> <th>NO.</th> <th>DATE</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> </tr> </tbody> </table>		NO.	DATE	DESCRIPTION									
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GRIFITH, IN SOUTH BEND, IN SPRINGFIELD, IL ST. LOUIS, MO		Weaver Boos Consultants TBPE REGISTRATION NO. F-3727		FIGURE 4.5													

O:\1339\351\EXPANSION 2009\PART III - SDR\1111\4.6-PERMITTED FLOODPLAIN.dwg, jwilson, 1:2



- LEGEND**
- PERMIT BOUNDARY
 - - - PROPOSED LIMIT OF WASTE
 - - - - AUTHORIZED LIMIT OF WASTE
 - N 7084000 STATE PLANE COORDINATE SYSTEM
 - 3.5'@2'@00" GEODETIC COORDINATE SYSTEM
 - EXISTING CONTOURS (SEE NOTE 1)
 - 520— EXISTING PERMITTED FINAL CONTOUR (SEE NOTE 3)
 - 500-YEAR FLOODPLAIN (CLOMR CASE NO. 02-06-1950R)
 - 100-YEAR FLOODPLAIN (CLOMR CASE NO. 02-06-1950R)
 - ▲▲ FILL/CUT SLOPE INDICATORS
 - 1319+98 FEMA/USACE CROSS SECTIONS

- NOTE:**
- CONTOURS AND ELEVATIONS PROVIDED BY METROPOLITAN AERIAL SURVEYS COMPILED FROM AERIAL PHOTOGRAPHY FLOWN 8-28-2010. THE GRID SYSTEM IS TIED TO THE TEXAS STATE PLANE COORDINATE SYSTEM NORTH CENTRAL ZONE NAD 1983. ELEVATIONS ARE BASED ON NAVD 1988. OFF-SITE CONTOURS AND ELEVATIONS PROVIDED BY DFWMAPS.COM FROM AERIAL SURVEYS COMPILED FROM AERIAL PHOTOGRAPHY FLOWN JANUARY TO MARCH 2007.
 - FLOODPLAIN BOUNDARIES REPRODUCED FROM WORK MAPS CREATED BY O'BRIEN ENGINEERING, INC. AND INCLUDED IN CLOMR CASE NO. 02-06-1950R, DEVELOPED FOR THE PROPOSED FINAL CONDITIONS IN TCEQ PERMIT NO. MSW-1312A.
 - PERMITTED CONDITIONS ARE TAKEN FROM THE PROPOSED FINAL CONDITIONS IN TCEQ PERMIT NO. MSW-1312A AND CLOMR CASE NO. 02-06-1950R.



2-28-12

<input type="checkbox"/> DRAFT <input checked="" type="checkbox"/> FOR PERMITTING PURPOSES ONLY <input type="checkbox"/> ISSUED FOR CONSTRUCTION <input type="checkbox"/> CLIENT APPROVAL BY:	PREPARED FOR	MAJOR PERMIT AMENDMENT PERMITTED 100-YEAR FLOODPLAIN DELINEATION CAMELOT LANDFILL DENTON COUNTY, TEXAS <i>Weaver Boos Consultants</i> TBPE REGISTRATION NO. F-3727												
	CITY OF FARMERS BRANCH													
DATE: 02/2012 FILE: 1339-351-11 CAD: 4.6-PERMITTED FLOOD.DWG	DRAWN BY: VRS DESIGN BY: CRM REVIEWED BY: JPY	<table border="1"> <thead> <tr> <th colspan="3">REVISIONS</th> </tr> <tr> <th>NO.</th> <th>DATE</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> </tr> </tbody> </table>	REVISIONS			NO.	DATE	DESCRIPTION						
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CHICAGO, IL NAPERVILLE, IL COLUMBUS, OH DENVER, CO		FORT WORTH, TX SOUTH BEND, IN SPRINGFIELD, IL ST. LOUIS, MO												
DRAWING 4.6														

**Table 4-1
Flow Rates, Drainage Areas, Hydrograph Time to Peak Values, Runoff Volumes, and Velocities
for the 25-Year Design Storm Event**

Stormwater Discharge Point ¹	Existing Permitted Condition						Updated Permitted Condition					Post-Development Condition				
	Existing Permitted Location HEC-1 ID	Flow Rate (cfs)	Drainage Area (acres)	Time to Peak (hrs)	Runoff Volume (ac-ft)	Velocity at Permit Boundary (fps)	Flow Rate (cfs)	Drainage Area (acres)	Time to Peak (hrs)	Runoff Volume ¹ (ac-ft)	Velocity at Permit Boundary ³ (fps)	Flow Rate (cfs)	Drainage Area (acres)	Time to Peak (hrs)	Runoff Volume ¹ (ac-ft)	Velocity at Permit Boundary ³ (fps)
Flow onto the Site																
DCPO1	---	---	---	---	---	---	298	87	12.42	43	1.38	298	87	12.42	43	1.38
DCPO1A	---	---	---	---	---	---	70	23	12.58	11	3.27	70	23	12.58	11	3.27
DCPO2	---	---	---	---	---	---	2,171	1,008	12.75	476	8.08	2,171	1,008	12.75	476	8.08
DCPO3	APF1	71	16	12.25	7	---	62	16	12.33	7	4.38	62	16	12.33	7	4.38
DCPO4 ⁴	C4MWY	293	198	12.25	61	---	2,887	1,433	12.75	677	8.29	2,881	1,425	12.67	676	8.28
Discharge from the Site																
DCP1 (Southeast-Midway) ⁵	MWY@RD	254	181	12.17	54	---	2,674	1,347	12.75	637	7.64	2,664	1,339	12.75	636	7.63
DCP2 (South-Midway) ⁶	CABELM	416	225	12.25	74	---	2,933	1,460	12.75	689	12.64	2,919	1,446	12.67	686	12.63
DCP3 (South-Elm Fork) ⁷	PD2OUT	160	134	13.17	61	---	201	133	13.00	64	11.00	173	160	12.75	80	10.60
DCP4 (Southeast-Elm Fork) ⁸	AN15	90	21	12.25	9	---	61	20	12.50	9	2.89	44	11	12.33	5	2.67
DCP5 (Southwest-Elm Fork) ⁹	APN14	151	29	12.17	12	---	88	26	12.42	12	10.64	80	23	12.42	11	10.39
DCP6 (Southwest-O5) ¹⁰	APN17	22	3	12.08	1	---	24	4	12.17	2	3.76	17	5	12.42	2	3.44
DCP7 (West-O5) ¹¹	C2D1	133	54	12.67	23	---	78	37	13.00	17	1.91	57	37	13.33	17	1.72
DCP8 (Northwest) ¹²	---	---	---	---	---	---	25	10	12.75	5	0.70	24	10	12.83	5	0.69

¹ Stormwater discharge points are shown on Figure 4.4. The volume shown is the total volume of runoff for the hydrograph duration.

² Existing permitted location HEC-1 ID is included for certain areas, as some locations were not included in the previously developed drainage analysis. Only available information is shown for the existing permitted conditions (e.g., if velocities are not already estimated in the currently approved documents, they are not listed).

³ Runoff volume and velocity calculations are provided in Appendix III-F-A and III-F-E.

⁴ Discharge Point DCPO4 includes all of Discharge Point DCP1 and offsite Drainage Area O4.

⁵ Discharge Point DCP1 includes several drainage areas within the permit boundary and DCPO1, DCPO2, and DCPO3 for the post-development and updated permitted cases. For the existing permitted case, DCP1 includes onsite drainage areas and DCPO3.

⁶ Discharge point DCP2 includes all of discharge point DCPO4 and DCP1 and onsite drainage areas.

⁷ Discharge Point DCP3 contains only onsite drainage areas.

⁸ Discharge Point DCP4 contains only onsite Drainage Area N15 for the existing and updated permitted conditions and only S10 for the post-development condition.

⁹ Discharge Point DCP5 contains only onsite Drainage Area N14 for the existing and updated permitted conditions and only S9 for the post-development condition.

¹⁰ Discharge Point DCP6 contains only onsite Drainage Area N17 for the existing and updated permitted conditions and only S3 for the post-development condition.

¹¹ Discharge Point DCP7 contains onsite Drainage Areas F4, N18, and N19 for the existing permit condition, onsite Drainage Areas S2, N18, and N19 for the updated permitted condition, and onsite Drainage Areas S2 and CH1 for the post-development condition.

¹² Discharge Point DCP8 contains only onsite Drainage Area S1.

**Table 4-2
100-Year Floodplain Elevation Comparison**

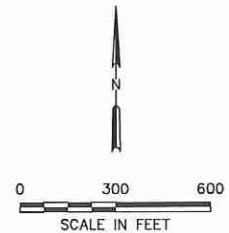
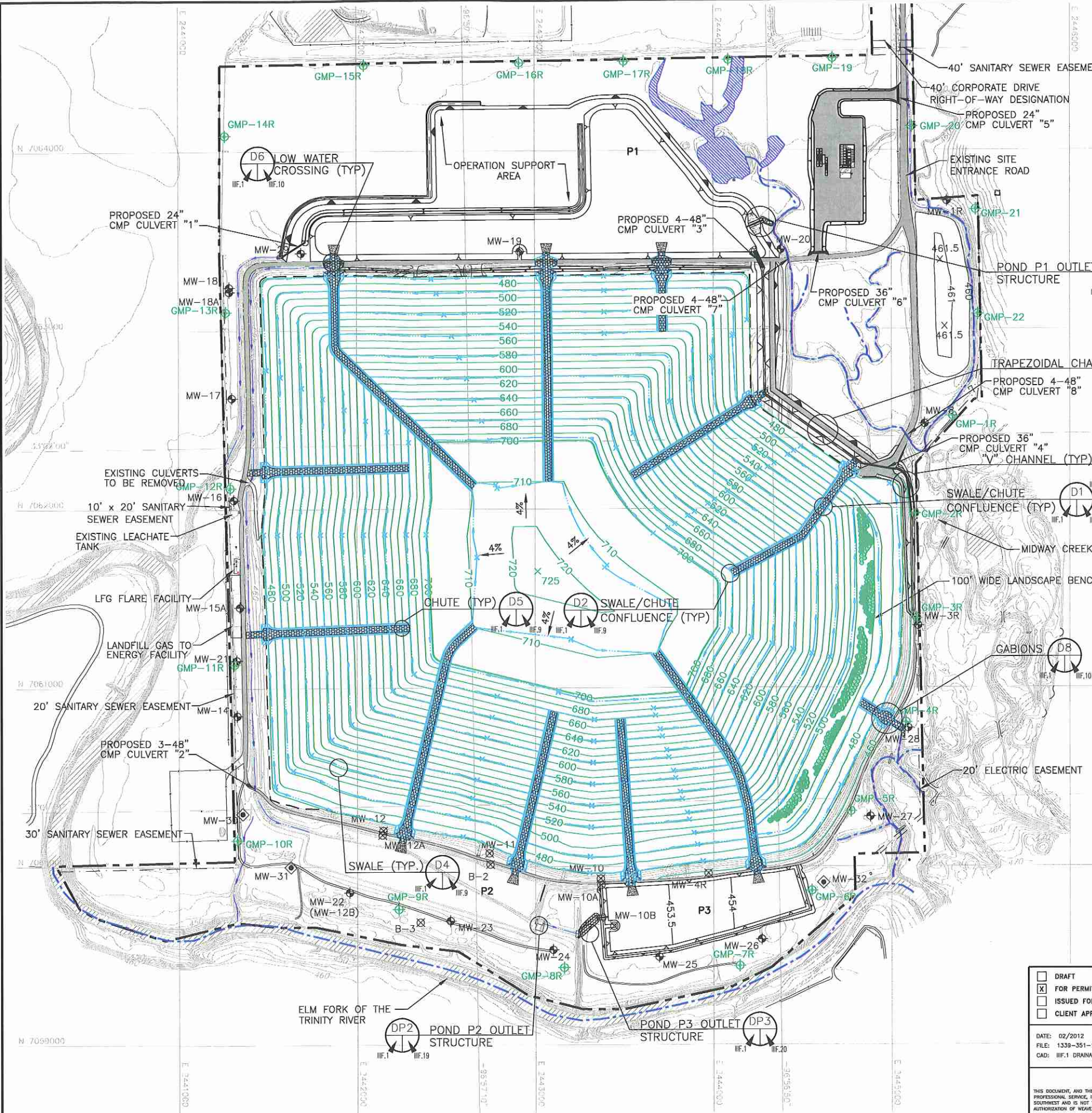
Section No ¹	CDC APPLICATION			CLOMR REQUEST		
	100-Year Peak Flow Rate (cfs)	100-Year Water Surface Elevations (ft-msl)		100-Year Peak Flow Rate (cfs)	100-Year Water Surface Elevations (ft-msl)	
		Existing Permitted	Proposed Expansion		Existing Permitted	Proposed Expansion
1315+32	10300	455.22	455.22	10300	455.10	455.10
1319+98	10300	455.49	455.49	10300	455.35	455.35
1326+56	10300	455.79	455.79	10300	455.67	455.67
1336+34	10300	456.11	456.11	10300	455.99	455.99
1345+38	10300	456.30	456.30	10300	456.22	456.22
1353+70	10300	456.68	456.67	10300	456.61	456.60
1361+49	10300	457.14	457.13	10300	457.07	457.07
1373+52	10300	457.51	457.50	10300	457.44	457.44
1378+78	10300	457.62	457.62	10300	457.56	457.55
1385+14	10300	458.04	458.03	10300	458.17	458.17
1396+43	21000	458.61	458.60	21000	458.78	458.78
1415+18	21000	459.66	459.66	21000	459.76	459.76
1429+00	21000	460.37	460.37	21000	460.35	460.34
1437+56	21000	460.48	460.47	21000	460.44	460.44
1444+74	21000	460.59	460.59	21000	460.57	460.57

¹ Section locations are shown on Figure 4.6 and Appendix III.O.

DRAWINGS

- III.F.1 – Drainage Structure Plan**
- III.F.2 – Post-Development Drainage Area Plan**
- III.F.3 – Post-Development Offsite Drainage Areas**
- III.F.4 – Perimeter Drainage Plan**
- III.F.5 – Perimeter Channel Profile**
- III.F.6 – Perimeter Channel Profile**
- III.F.7 – Perimeter Channel Profile**
- III.F.8 – Perimeter Channel Profile**
- III.F.9 – Drainage Details**
- III.F.10 – Drainage Details**
- III.F.11 – Drainage Details**
- III.F.12 – Drainage Details**
- III.F.13 – Pond P1 Plan**
- III.F.14 – Pond P1 Sections**
- III.F.15 – Pond P2 Plan**
- III.F.16 – Pond P2 Sections**
- III.F.17 – Pond P3 Plan**
- III.F.18 – Pond P3 Sections**
- III.F.19 – Pond Outlet Structure Details**
- III.F.20 – Pond Outlet Structure Details**

O:\1339\351\EXPANSION 2009\PART III-SDP\IIIF.1--DRAINAGE PLAN.dwg, jwilson, 1-2



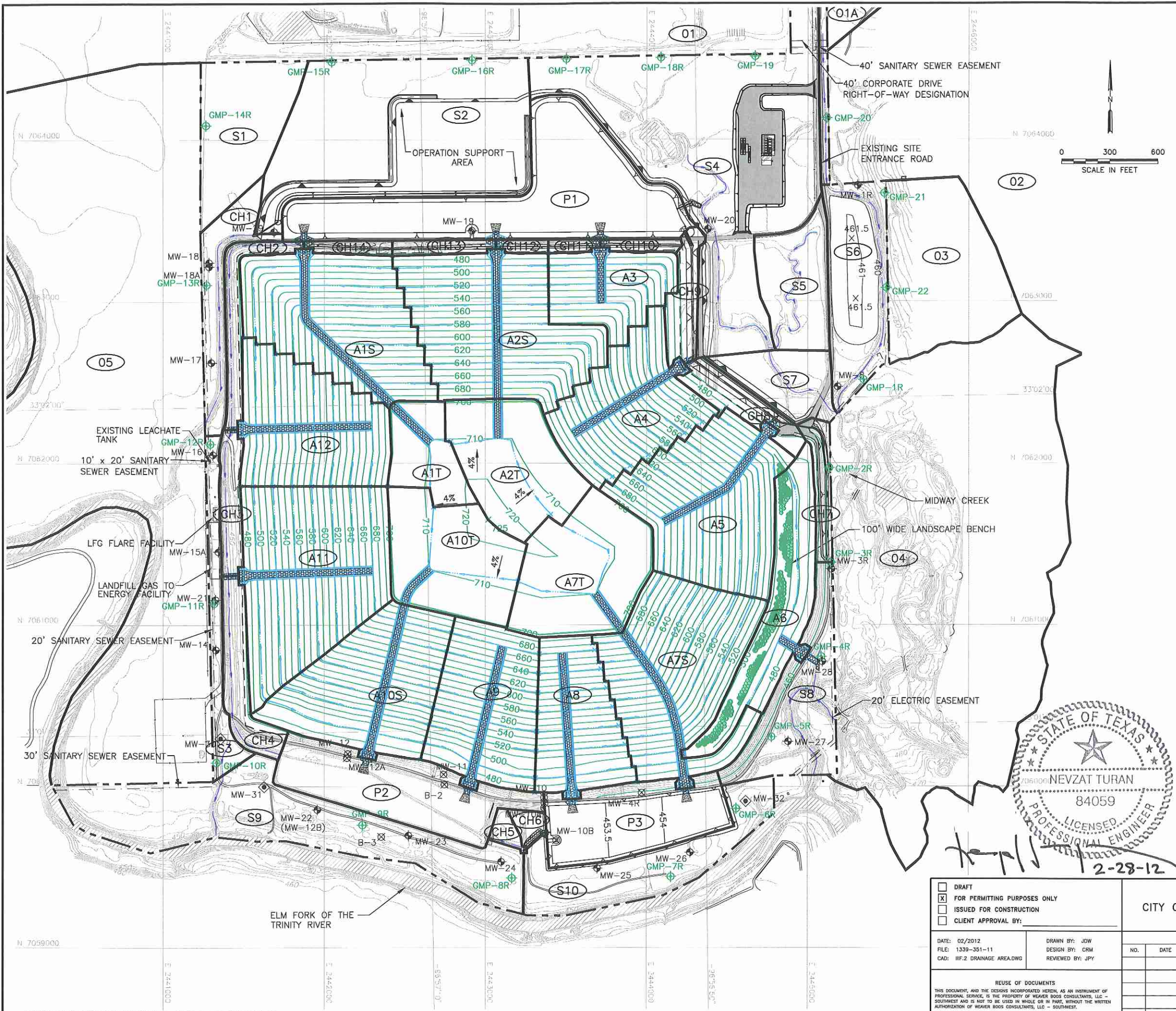
- LEGEND**
- PERMIT BOUNDARY
 - PROPOSED LIMIT OF WASTE
 - STATE PLANE COORDINATE SYSTEM
 - GEODETIC COORDINATE SYSTEM
 - EXISTING CONTOUR (SEE NOTE 1)
 - 600 FINAL COVER CONTOUR
 - DRAINAGE LETDOWN
 - DRAINAGE SWALE
 - EASEMENT BOUNDARY
 - MW-8 GROUNDWATER MONITORING WELL
 - MW-30 PROPOSED GROUNDWATER MONITORING WELL
 - GMP-20 PROPOSED LANDFILL GAS MONITORING PROBE
 - MW-12 OBSERVATION WELL
 - USACE SECTION 404 JURISDICTIONAL WATERS OF THE U.S. (SEE NOTE 4)
 - USACE JURISDICTIONAL WETLANDS

- NOTE:**
1. CONTOURS AND ELEVATIONS PROVIDED BY METROPOLITAN AERIAL SURVEYS COMPILED FROM AERIAL PHOTOGRAPHY FLOWN 8-28-2010. THE GRID SYSTEM IS TIED TO THE TEXAS STATE PLANE COORDINATE SYSTEM NORTH CENTRAL ZONE NAD 1983. ELEVATIONS ARE BASED ON NAVD 1988.
 2. PERMIT BOUNDARY WAS PREPARED BY PEISER SUREYING CO. IN NOVEMBER 2010.
 3. MAXIMUM FINAL COVER ELEVATION IS 725 FT-MSL. MAXIMUM TOP OF WASTE ELEVATION IS 721.5 FT-MSL.
 4. SECTION 404 JURISDICTIONAL WATERS OF THE U.S. AND WETLANDS REPRODUCED FROM THE GOSHAWK ENVIRONMENTAL CONSULTANTS, INC. SEPTEMBER 2010 REPORT WHICH IS INCLUDED IN PARTS I/II, APPENDIX I/II.
 5. FINAL COVER DETAILS ARE PROVIDED IN APPENDIX IIIA-A LINER, OVERLINER, AND FINAL COVER SYSTEM DETAILS.



2-28-12

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DATE: 02/2012 FILE: 1339-351-11 CAD: IIF.1 DRAINAGE PLAN.DWG	DRAWN BY: JDW DESIGN BY: CRM REVIEWED BY: JPY	<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th colspan="3">REVISIONS</th> </tr> <tr> <th>NO.</th> <th>DATE</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> </tr> </tbody> </table>	REVISIONS			NO.	DATE	DESCRIPTION						
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CHICAGO, IL MAPERVILLE, IL GRIFITH, IN DENVER, CO FORT WORTH, TX SOUTH BEND, IN (817) 735-9770 (817) 735-9770 (817) 735-9770		DRAWING IIF.1												



LEGEND

- PERMIT BOUNDARY
- PROPOSED LIMIT OF WASTE
- N 7064000 STATE PLANE COORDINATE SYSTEM
- 33°02'00" GEODETIC COORDINATE SYSTEM
- 500 EXISTING CONTOUR (SEE NOTE 1)
- 600 REGRADED BUFFER ZONE AREA
- 600 FINAL COVER CONTOUR
- DRAINAGE LETDOWN
- DRAINAGE SWALE
- EASEMENT BOUNDARY
- ◆ MW-8 EXISTING GROUNDWATER MONITORING WELL
- ◆ MW-30 PROPOSED GROUNDWATER MONITORING WELL
- ◆ GMP-20 PROPOSED LANDFILL GAS MONITORING PROBE
- ⊗ MW-12 OBSERVATION WELL
- DRAINAGE AREA BOUNDARY
- (A7T) DRAINAGE AREA DESIGNATION

- NOTE:**
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 - PERMIT BOUNDARY WAS PREPARED BY PEISER SUREYING CO. IN NOVEMBER 2010.
 - MAXIMUM FINAL COVER ELEVATION IS 725 FT-MSL. MAXIMUM TOP OF WASTE ELEVATION IS 721.5 FT-MSL.
 - REFER TO DRAWING IIF.3 FOR COMPLETE OFFSITE DRAINAGE AREA DELINEATIONS.

DRAINAGE AREA NO.	AREA (ACRES)	DRAINAGE AREA NO.	AREA (ACRES)
S1	10.26	A10T	12.37
S2	30.86	A10S	16.60
S3	4.55	A11	22.08
S4	43.34	A12	15.17
S5	7.34	CH1	5.94
S6	13.92	CH2	3.29
S7	5.39	CH3	2.71
S8	10.12	CH4	4.45
S9	22.75	CH5	0.76
S10	10.76	CH6	0.83
A1T	5.47	CH7	2.33
A1S	18.48	CH8	3.37
A2T	11.83	CH9	3.09
A2S	20.59	CH10	0.85
A3	8.07	CH11	0.56
A4	13.51	CH12	0.59
A5	19.01	CH13	1.29
A6	11.00	CH14	1.02
A7T	13.58	P1	23.10
A7S	20.36	P2	12.55
A8	10.75	P3	10.74
A9	13.99		



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 ISSUED FOR CONSTRUCTION
 CLIENT APPROVAL BY:

DATE: 02/2012
 FILE: 1339-351-11
 CAD: IIF.2 DRAINAGE AREA.DWG

DRAWN BY: JDW
 DESIGN BY: CRM
 REVIEWED BY: JPY

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PREPARED FOR
CITY OF FARMERS BRANCH

REVISIONS		
NO.	DATE	DESCRIPTION

**MAJOR PERMIT AMENDMENT
 POST DEVELOPMENT DRAINAGE
 CAMELOT LANDFILL
 DENTON COUNTY, TEXAS**

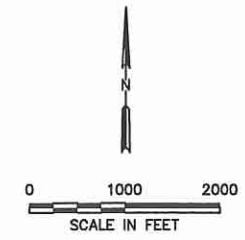
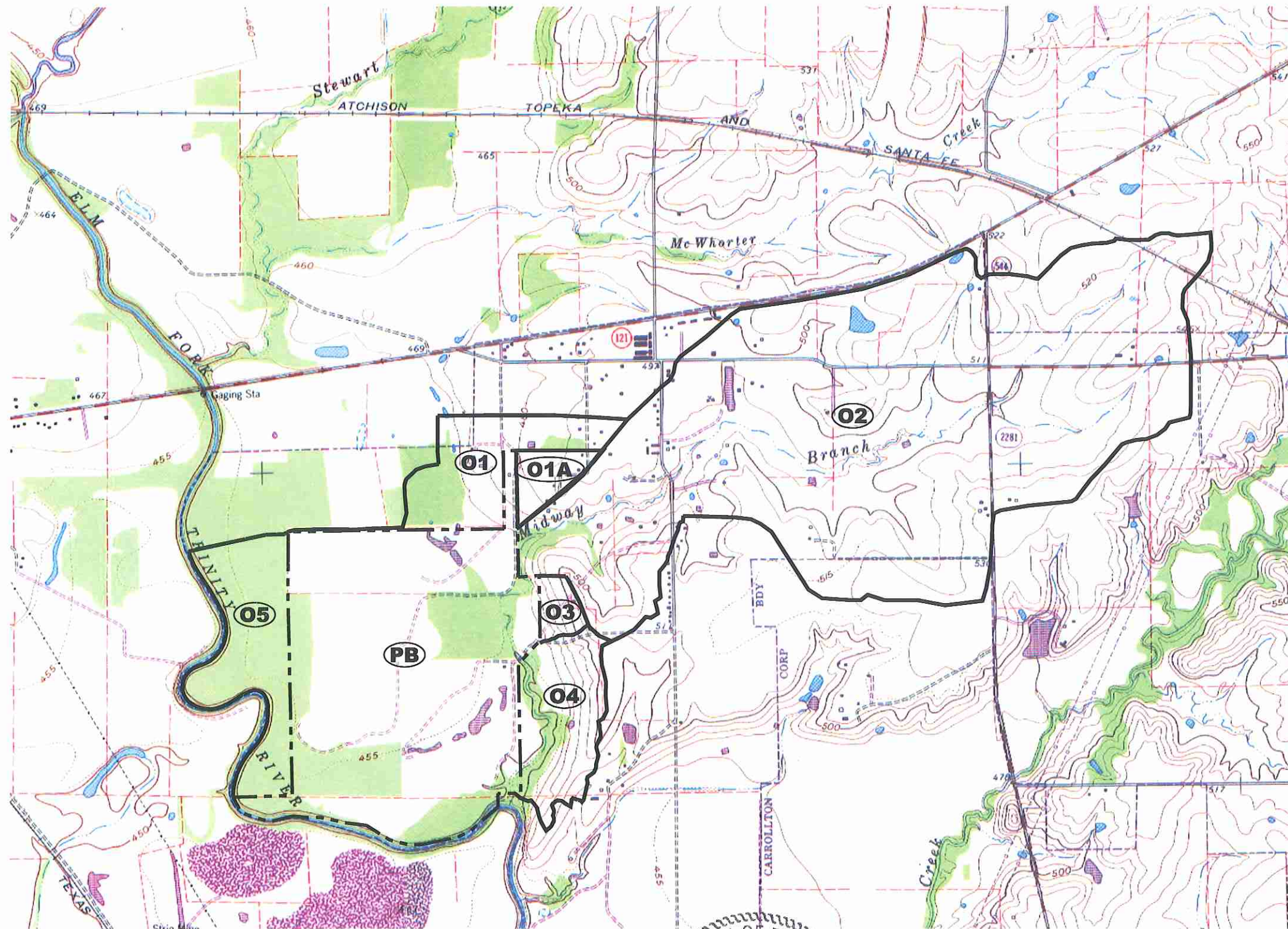
Weaver Boos Consultants
 TBPE REGISTRATION NO. F-3727

CHICAGO, IL FORT WORTH, TX GRIFFITH, IN
 WAPERVILLE, IL (817) 735-9770 SOUTH BEND, IN
 COLUMBUS, OH DENVER, CO SPRINGFIELD, IL ST. LOUIS, MO

DRAWING IIF.2

O:\1339\351\EXPANSION 2009\PART III-SDF\IIF.2-DRAINAGE AREAS.dwg, jwilson, 1/2

C:\1399\351\EXPANSION 2009\PART III-SDP\IIIF\IIIF.3-OFFSITE DRAINAGE.dwg, cellinger, 1:2



LEGEND

--- PERMIT BOUNDARY

— DRAINAGE AREA BOUNDARY

⓪ DRAINAGE AREA LABEL

DRAINAGE AREA NO.	AREA (ACRES)
O1	87.5
O1A	23.4
O2	1,008.4
O3	16.2
O4	86.0
O5	116.5
PB	462.6
TOTAL	1,807.6

ROAD CLASSIFICATION

Heavy-duty ——— Light-duty ———

Medium-duty ——— Unimproved dirt ———

Ⓜ Interstate Route Ⓜ U.S. Route Ⓜ State Route

LEWISVILLE EAST, TEX.
 SW/4 FRISCO 15' QUADRANGLE
 N3300-W9652.5/7.5
 1960
 PHOTOREVISED 1968
 AMS 6650 III SW-SERIES V882

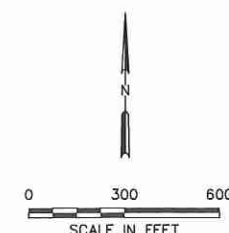
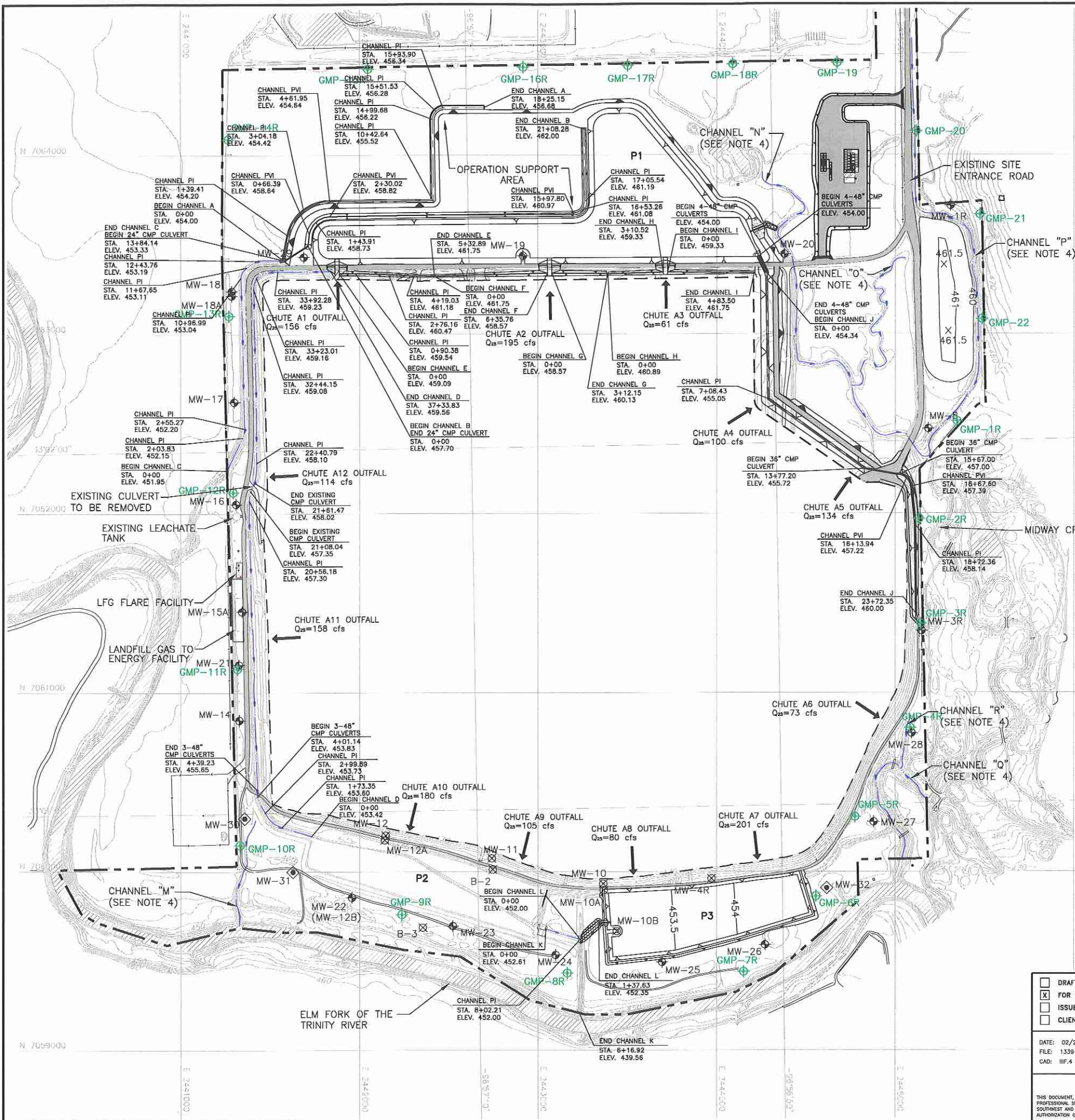
- NOTES:**
- REFER TO DRAWING IIIF.2 DRAINAGE AREA DELINEATION WITHIN THE PERMIT BOUNDARY.
 - TOPOGRAPHY IS REPRODUCED FROM USGS 7.5 MINUTE QUADRANGLE TOPOGRAPHIC MAP (LEWISVILLE EAST, TX, PHOTO REVISED 1981).



[Handwritten Signature]
 2-28-12

<input type="checkbox"/> DRAFT <input checked="" type="checkbox"/> FOR PERMITTING PURPOSES ONLY <input type="checkbox"/> ISSUED FOR CONSTRUCTION <input type="checkbox"/> CLIENT APPROVAL BY:	PREPARED FOR CITY OF FARMERS BRANCH	MAJOR PERMIT AMENDMENT OFFSITE DRAINAGE AREA MAP CAMELOT LANDFILL DENTON COUNTY, TEXAS <i>Weaver Boos Consultants</i> TBPE REGISTRATION NO. F-3727												
	DATE: 02/2012 FILE: 1339-351-11 CAD: IIIF.3 OFFSITE DRAINAGE.DWG		DRAWN BY: JDW DESIGN BY: CRM REVIEWED BY: JPY	REVISIONS <table border="1"> <thead> <tr> <th>NO.</th> <th>DATE</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> </tr> </tbody> </table>	NO.	DATE	DESCRIPTION							
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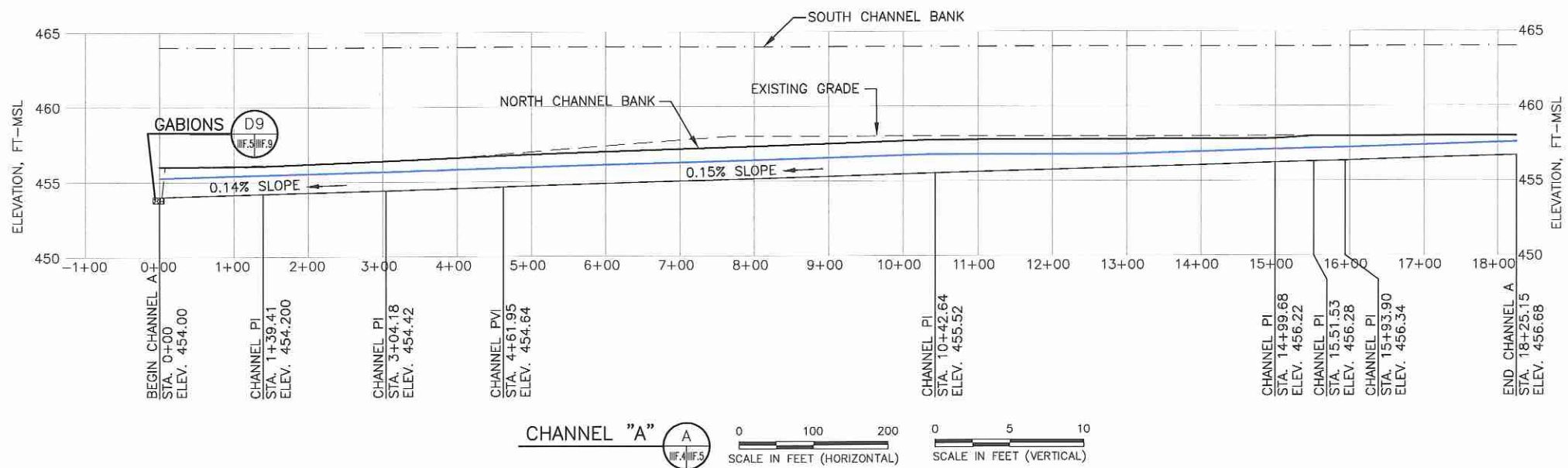
- LEGEND**
- PERMIT BOUNDARY
 - LIMIT OF WASTE
 - N 7064000 STATE PLANE COORDINATE SYSTEM
 - 33°02'00" GEODETIC COORDINATE SYSTEM
 - EXISTING CONTOUR (SEE NOTE 1)
 - STA. STATION (FT)
 - ELEV. ELEVATION (FT-MSL)
 - Q₂₅=60 cfs 25-YEAR PEAK FLOW RATE (CUBIC FEET/SECOND)
 - MW-8 EXISTING GROUNDWATER MONITORING WELL
 - MW-30 PROPOSED GROUNDWATER MONITORING WELL
 - GMP-20 PROPOSED LANDFILL GAS MONITORING PROBE
 - MW-12 OBSERVATION WELL
 - PROPOSED CHANNEL CENTERLINE
 - EXISTING CHANNEL CENTERLINE
 - GABIONS
 - 600 REGRADED BUFFER ZONE AREA

- NOTE:**
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 - PROPOSED PERMIT BOUNDARY WAS PREPARED BY PEISER SUREYING CO. IN NOVEMBER 2010.
 - CHANNEL PROFILE INFORMATION BASED ON THE STATIONS SHOWN IS PROVIDED ON DRAWINGS IIIF.5 THROUGH IIIF.8.
 - ANALYSIS OF CHANNELS K,M,N,O,P,Q, AND R IS INCLUDED IN APPENDIX IIIF.B.



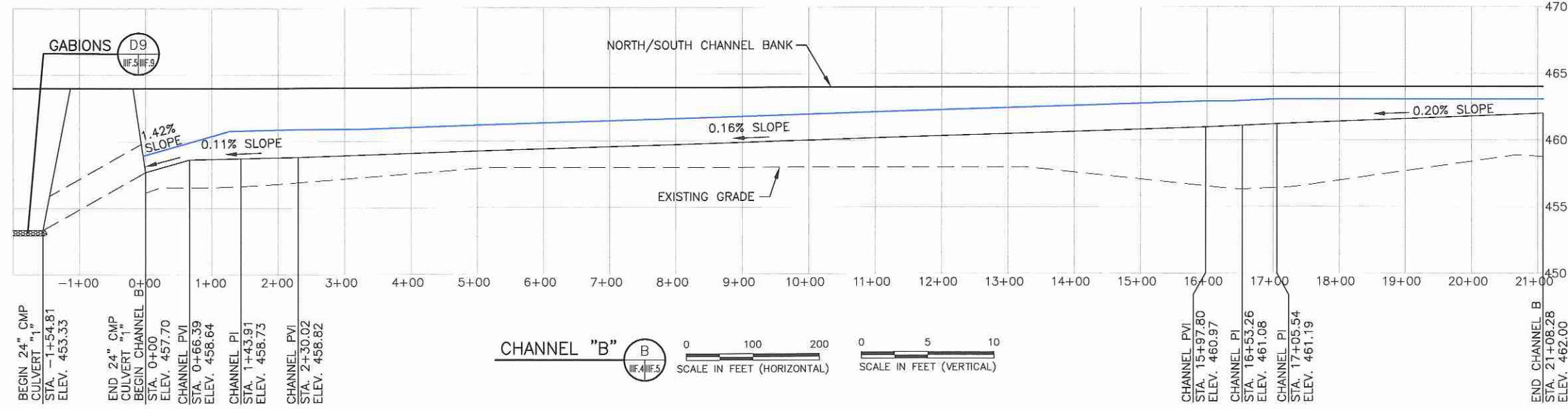
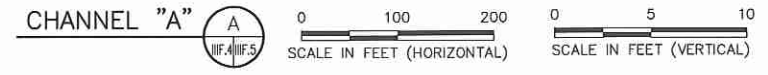
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	CITY OF FARMERS BRANCH							
DATE: 02/2012 FILE: 1339-351-11 CAD: IIIF.4 CHANNEL PLAN.DWG	DRAWN BY: JDW DESIGN BY: CRM REVIEWED BY: JPY	REVISIONS <table border="1"> <thead> <tr> <th>NO.</th> <th>DATE</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr> <td> </td> <td> </td> <td> </td> </tr> </tbody> </table>	NO.	DATE	DESCRIPTION			
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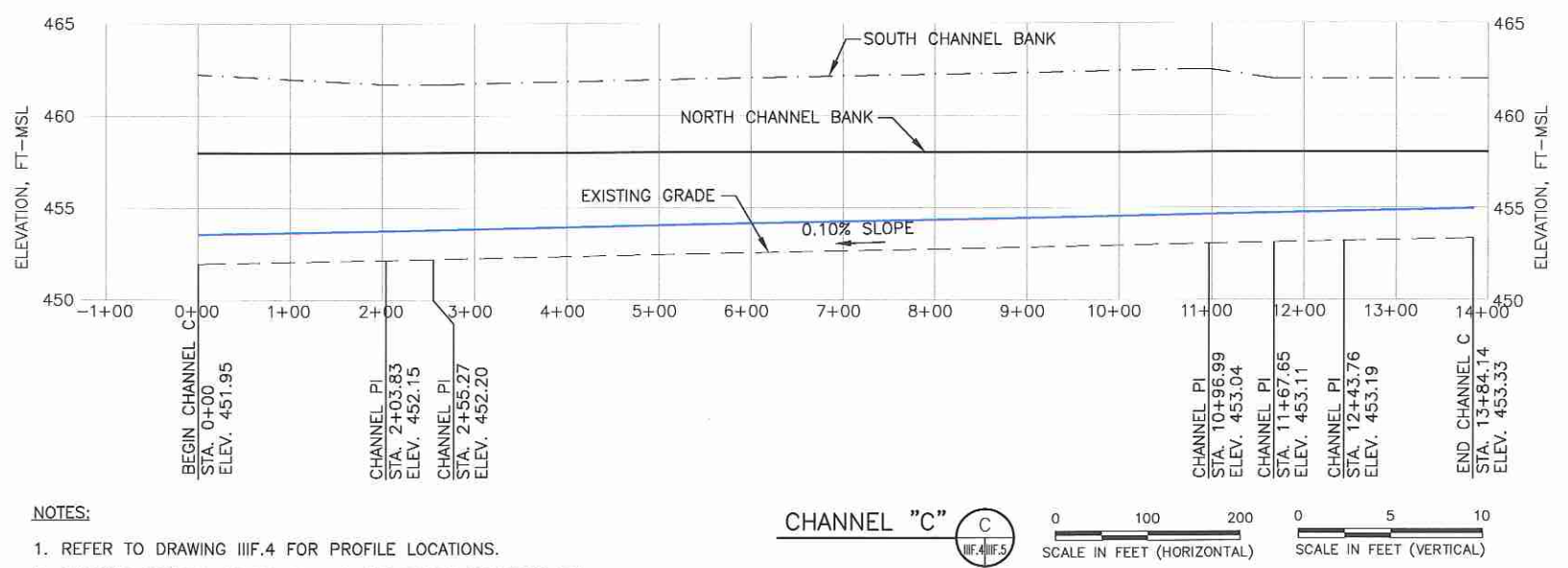
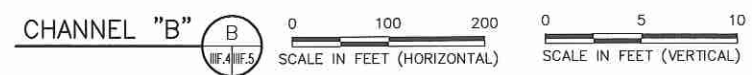
CHANNEL STATION FROM	CHANNEL STATION TO	BOTTOM WIDTH (FT)	PEAK INFLOW (CFS)	SLOPE (%)	FLOW DEPTH (FT.)	VELOCITY (FT/S)
0+00	4+61.95	10	31	0.14	1.25	1.80
4+61.95	10+42.64	10	31	0.15	1.23	1.85
10+42.64	18+25.15	20	31	0.15	0.86	1.60

NOTE: NORMAL DEPTH CALCULATION DOES NOT ACCOUNT FOR BACK WATER WHICH WILL INCREASE FLOW DEPTH (SEE PROFILE) AND DECREASE VELOCITY.



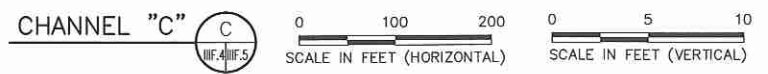
CHANNEL STATION FROM	CHANNEL STATION TO	BOTTOM WIDTH (FT)	PEAK INFLOW (CFS)	SLOPE (%)	FLOW DEPTH (FT.)	VELOCITY (FT/S)
0+00	0+66.39	0	21	1.42	1.28	4.24
0+66.39	2+30.02	0	21	0.11	2.07	1.63
2+30.02	15+97.80	0	21	0.16	1.93	1.87
15+97.80	17+05.54	0	21	0.20	1.85	2.04
17+05.54	21+08.28	15	21	0.20	0.74	1.66

NOTE: NORMAL DEPTH CALCULATION DOES NOT ACCOUNT FOR BACK WATER WHICH WILL INCREASE FLOW DEPTH (SEE PROFILE) AND DECREASE VELOCITY.



CHANNEL STATION FROM	CHANNEL STATION TO	BOTTOM WIDTH (FT)	PEAK INFLOW (CFS)	SLOPE (%)	FLOW DEPTH (FT.)	VELOCITY (FT/S)
0+00	13+84.14	15	57	0.10	1.59	1.82

NOTE: NORMAL DEPTH CALCULATION DOES NOT ACCOUNT FOR BACK WATER WHICH WILL INCREASE FLOW DEPTH (SEE PROFILE) AND DECREASE VELOCITY.



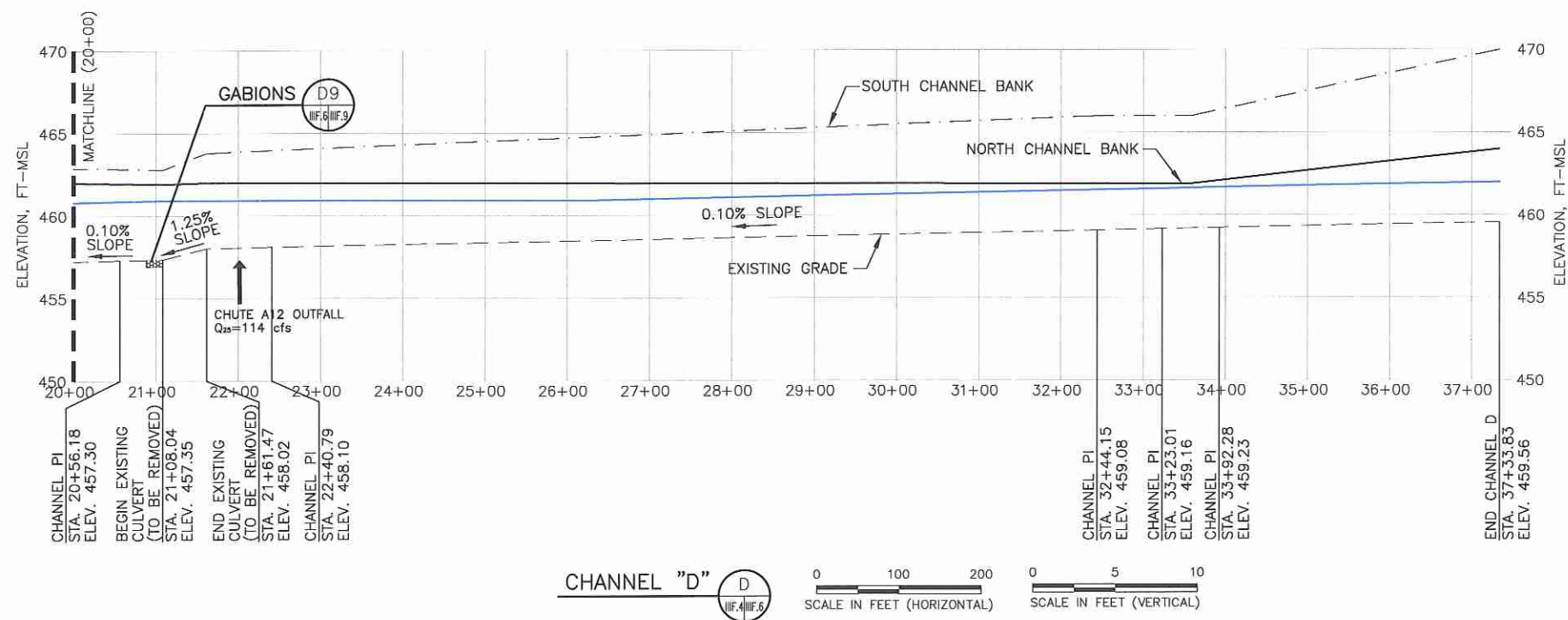
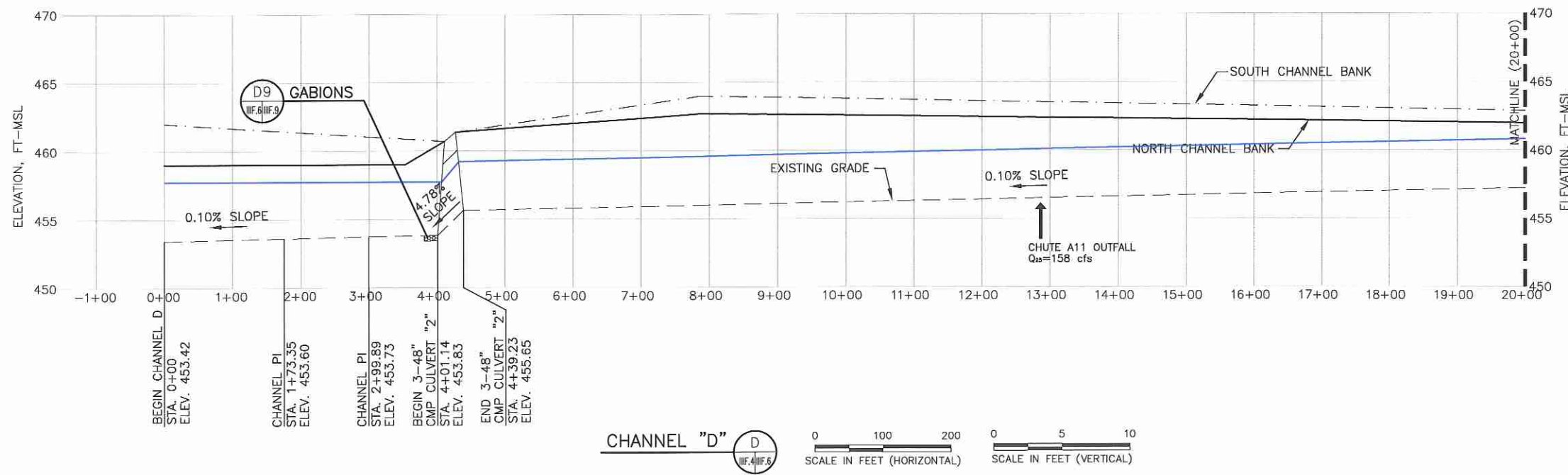
[Signature]
2-28-12

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- CULVERT CALCULATIONS INCLUDED IN APPENDIX III.F.-B.

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	DATE: 02/2012 FILE: 1339-351-11 CAD: III.F.5 CHANNEL PLAN.DWG	
REVISIONS NO. DATE DESCRIPTION		CHICAGO, IL NAPERVILLE, IL COLUMBUS, OH DENVER, CO
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CHANNEL FROM	CHANNEL TO	BOTTOM WIDTH (FT)	PEAK INFLOW (CFS)	SLOPE (%)	FLOW DEPTH (FT.)	VELOCITY (FT/S)	
0+00	4+01.14	15	261	0.10	3.57	2.84	
4+01.14	4+39.23	42" CMP CULVERT "2"					
4+39.23	21+08.04	15	261	0.10	3.57	2.84	
21+08.04	21+61.47	15	126	1.25	1.22	5.54	
21+61.47	37+33.83	15	126	0.10	2.44	2.31	

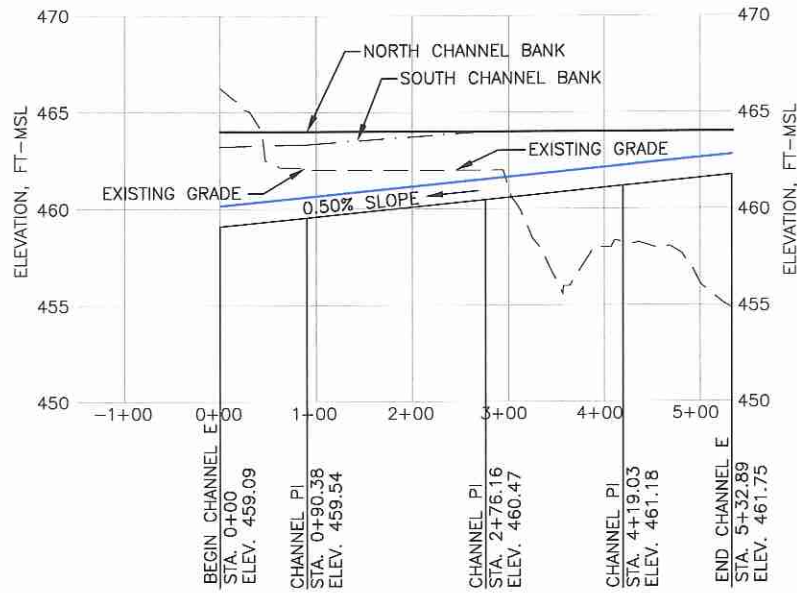
NOTE: NORMAL DEPTH CALCULATION DOES NOT ACCOUNT FOR BACK WATER WHICH WILL INCREASE FLOW DEPTH (SEE PROFILE) AND DECREASE VELOCITY.



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			DRAWING III.F.6

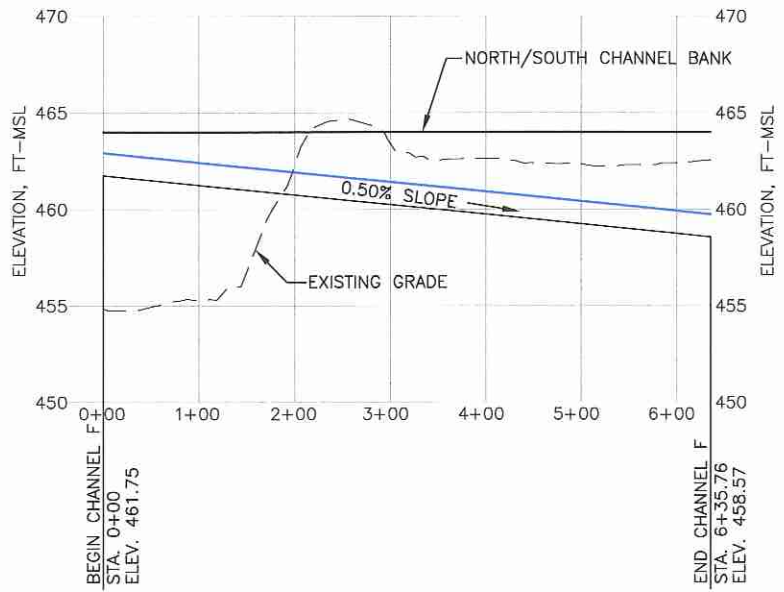


25-YEAR CHANNEL "E" INFORMATION						
CHANNEL STATION		BOTTOM WIDTH (FT)	PEAK INFLOW (CFS)	SLOPE (%)	FLOW DEPTH (FT.)	VELOCITY (FT/S)
FROM	TO					
0+00	5+32.89	0	7	0.50	1.04	2.18

NOTE: NORMAL DEPTH CALCULATION DOES NOT ACCOUNT FOR BACK WATER WHICH WILL INCREASE FLOW DEPTH (SEE PROFILE) AND DECREASE VELOCITY.

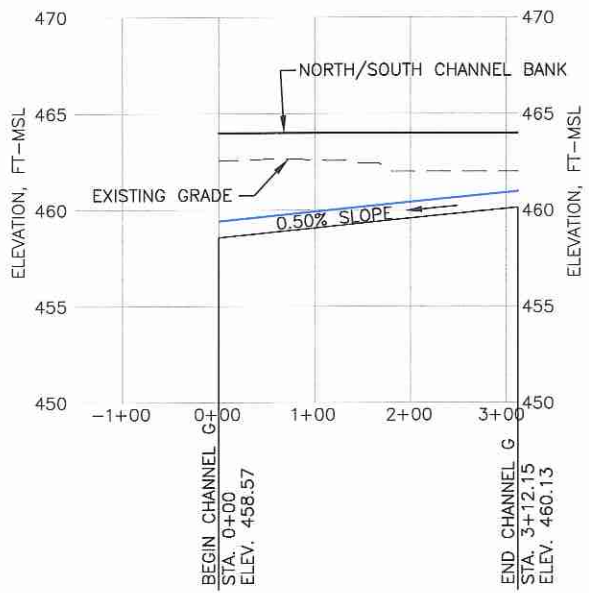
25-YEAR CHANNEL "F" INFORMATION						
CHANNEL STATION		BOTTOM WIDTH (FT)	PEAK INFLOW (CFS)	SLOPE (%)	FLOW DEPTH (FT.)	VELOCITY (FT/S)
FROM	TO					
0+00	6+35.76	0	9	0.50	1.14	2.32

NOTE: NORMAL DEPTH CALCULATION DOES NOT ACCOUNT FOR BACK WATER WHICH WILL INCREASE FLOW DEPTH (SEE PROFILE) AND DECREASE VELOCITY.



CHANNEL "F" SCALE IN FEET (HORIZONTAL) 0 100 200 SCALE IN FEET (VERTICAL) 0 5 10

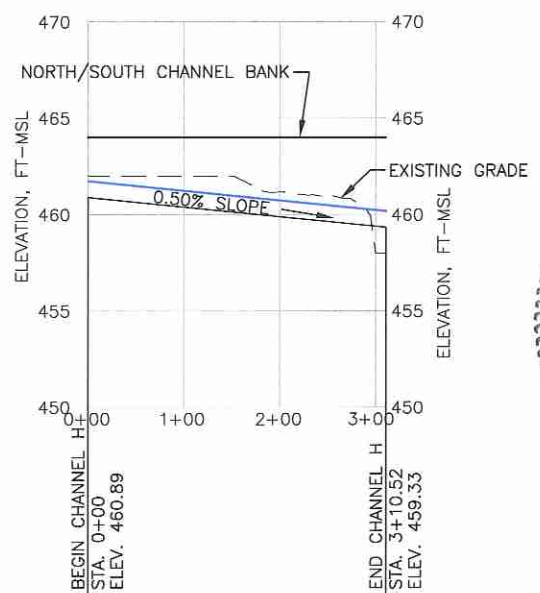
CHANNEL "E" SCALE IN FEET (HORIZONTAL) 0 100 200 SCALE IN FEET (VERTICAL) 0 5 10



CHANNEL "G" SCALE IN FEET (HORIZONTAL) 0 100 200 SCALE IN FEET (VERTICAL) 0 5 10

25-YEAR CHANNEL "G" INFORMATION						
CHANNEL STATION		BOTTOM WIDTH (FT)	PEAK INFLOW (CFS)	SLOPE (%)	FLOW DEPTH (FT.)	VELOCITY (FT/S)
FROM	TO					
0+00	3+12.15	0	4	0.50	0.84	1.89

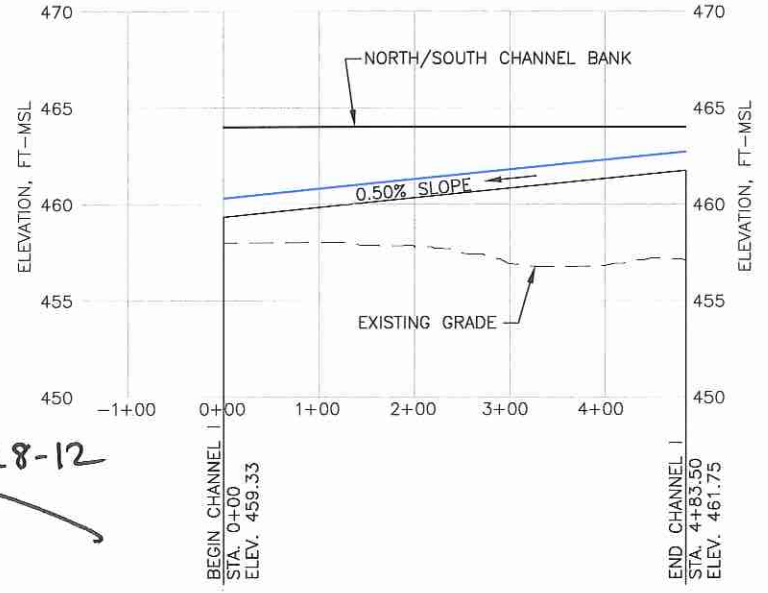
NOTE: NORMAL DEPTH CALCULATION DOES NOT ACCOUNT FOR BACK WATER WHICH WILL INCREASE FLOW DEPTH (SEE PROFILE) AND DECREASE VELOCITY.



CHANNEL "H" SCALE IN FEET (HORIZONTAL) 0 100 200 SCALE IN FEET (VERTICAL) 0 5 10

25-YEAR CHANNEL "H" INFORMATION						
CHANNEL STATION		BOTTOM WIDTH (FT)	PEAK INFLOW (CFS)	SLOPE (%)	FLOW DEPTH (FT.)	VELOCITY (FT/S)
FROM	TO					
0+00	3+10.52	0	4	0.50	0.84	1.89

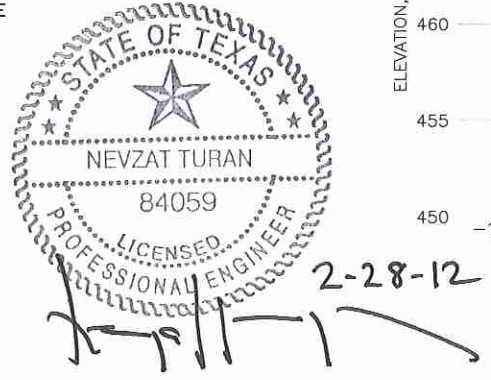
NOTE: NORMAL DEPTH CALCULATION DOES NOT ACCOUNT FOR BACK WATER WHICH WILL INCREASE FLOW DEPTH (SEE PROFILE) AND DECREASE VELOCITY.



CHANNEL "I" SCALE IN FEET (HORIZONTAL) 0 100 200 SCALE IN FEET (VERTICAL) 0 5 10

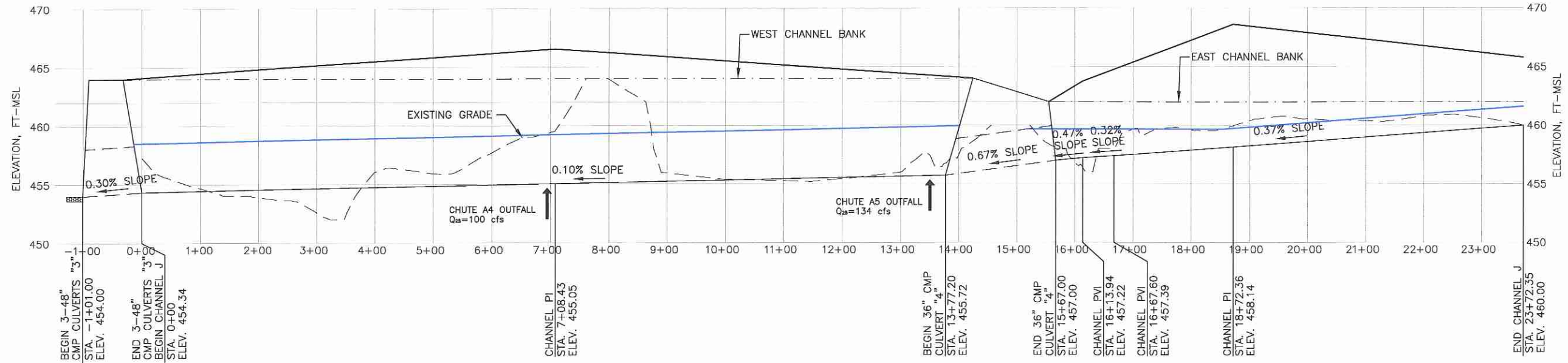
25-YEAR CHANNEL "I" INFORMATION						
CHANNEL STATION		BOTTOM WIDTH (FT)	PEAK INFLOW (CFS)	SLOPE (%)	FLOW DEPTH (FT.)	VELOCITY (FT/S)
FROM	TO					
0+00	4+83.50	0	6	0.50	0.98	2.10

NOTE: NORMAL DEPTH CALCULATION DOES NOT ACCOUNT FOR BACK WATER WHICH WILL INCREASE FLOW DEPTH (SEE PROFILE) AND DECREASE VELOCITY.



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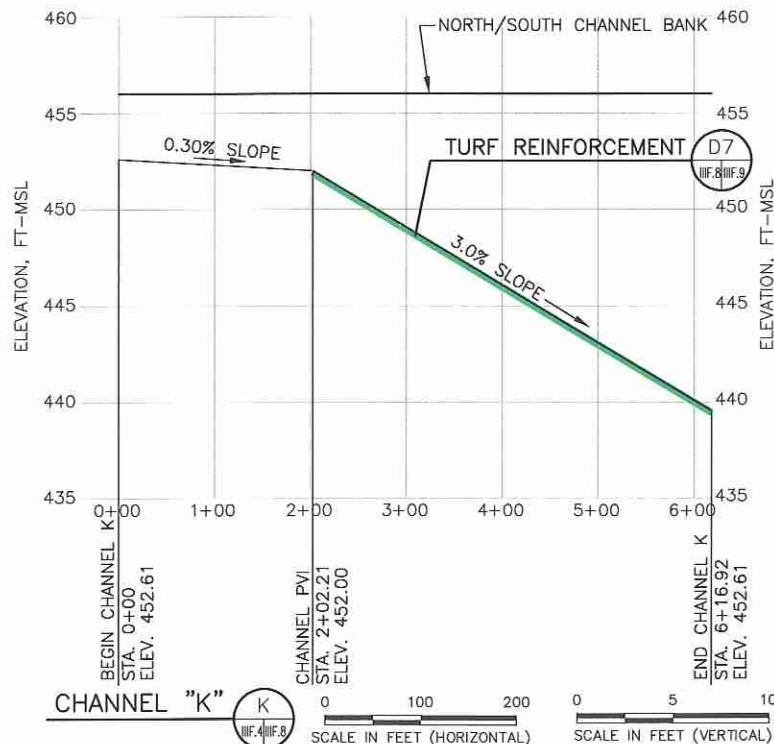
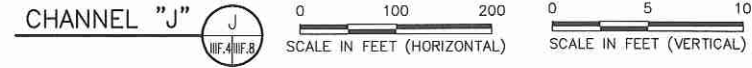
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25-YEAR CHANNEL "J" INFORMATION

CHANNEL STATION FROM	CHANNEL STATION TO	BOTTOM WIDTH (FT)	PEAK INFLOW (CFS)	SLOPE (%)	FLOW DEPTH (FT.)	VELOCITY (FT/S)	
0+00	13+77.20	10	275	0.10	4.16	2.94	
13+77.20	15+67.00	36" CMP CULVERT "4"					
15+67.00	16+13.94	0	17	0.47	1.46	2.66	
16+13.94	16+67.60	0	17	0.32	1.57	2.30	
16+67.60	23+72.35	0	17	0.37	1.53	2.43	

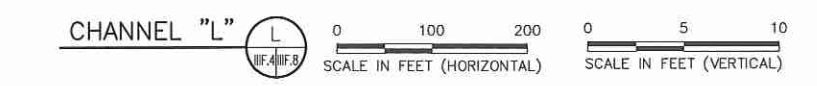
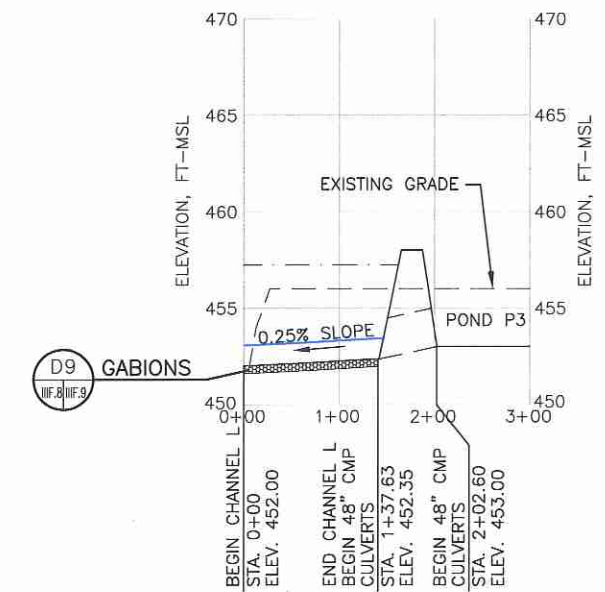
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25-YEAR CHANNEL "K" INFORMATION

CHANNEL STATION FROM	CHANNEL STATION TO	BOTTOM WIDTH (FT)	PEAK INFLOW (CFS)	SLOPE (%)	FLOW DEPTH (FT.)	VELOCITY (FT/S)
0+00	2+02.21	15	118	0.30	1.75	3.33
2+02.21	6+16.92	0	173	3.00	2.46	9.51

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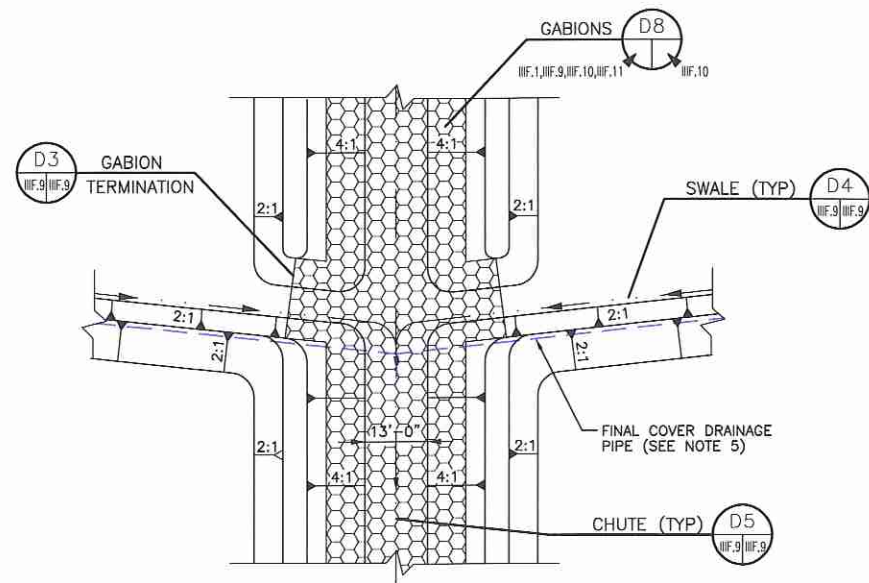
25-YEAR CHANNEL "L" INFORMATION

CHANNEL STATION FROM	CHANNEL STATION TO	BOTTOM WIDTH (FT)	PEAK INFLOW (CFS)	SLOPE (%)	FLOW DEPTH (FT.)	VELOCITY (FT/S)
0+00	1+37.63	25	53	0.25	1.06	1.78

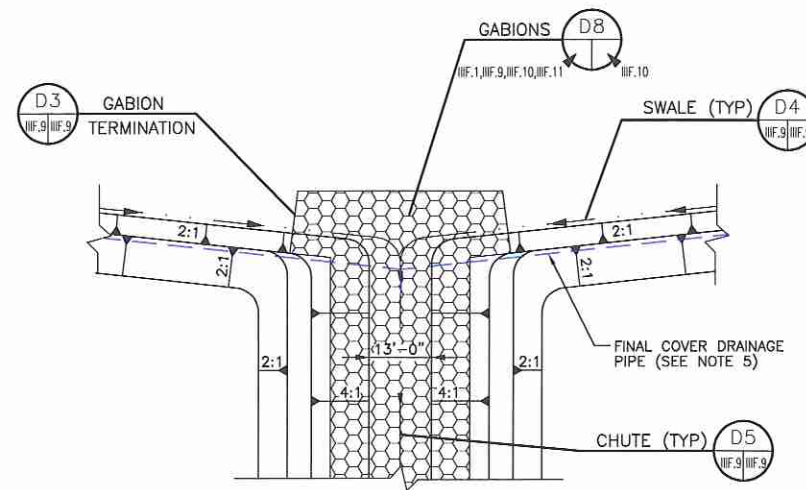
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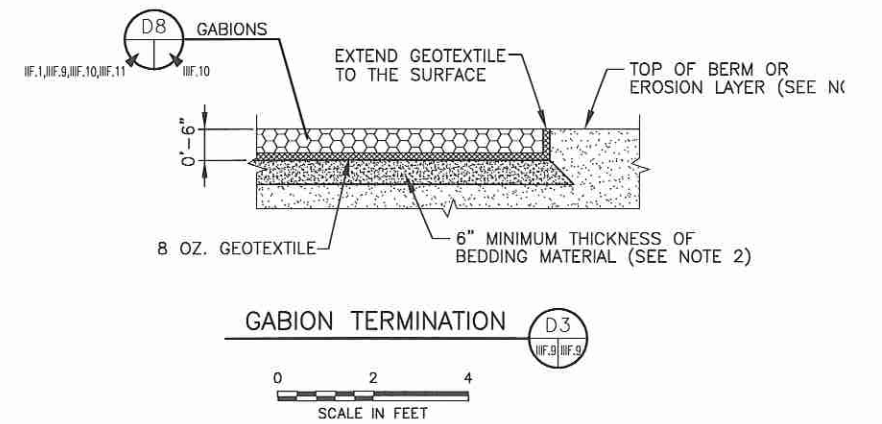
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		FORT WORTH, TX SOUTH BEND, IN SPRINGFIELD, IL ST. LOUIS, MO
		DRAWING IIIF.8



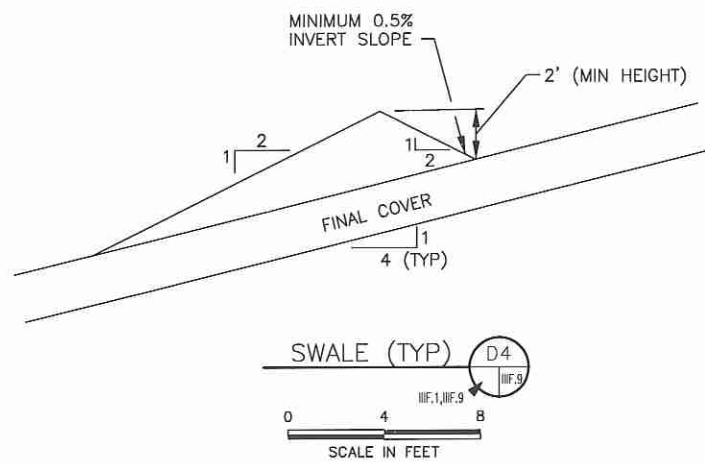
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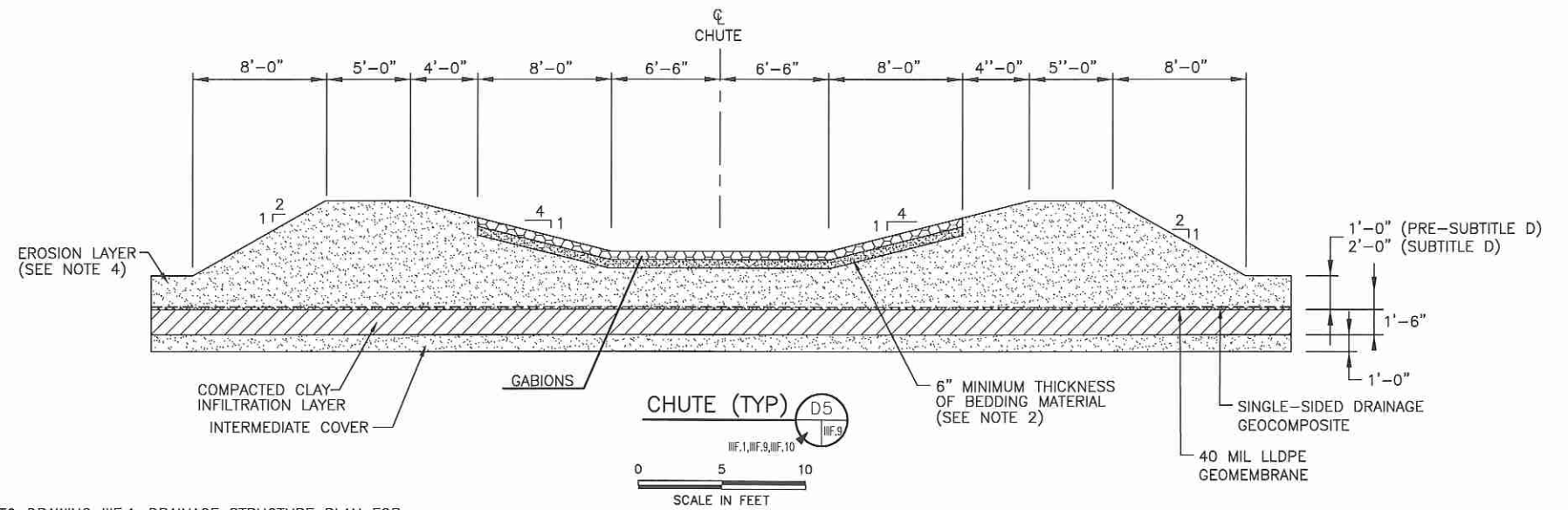
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GABION TERMINATION D3
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SWALE (TYP) D4
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 SCALE IN FEET



CHUTE (TYP) D5
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 SCALE IN FEET

NOTES:

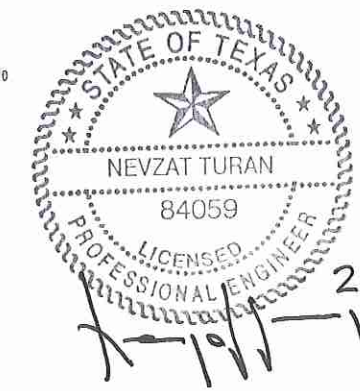
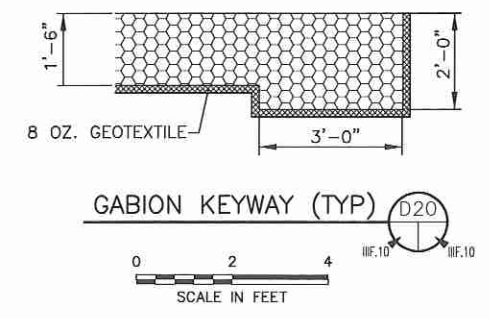
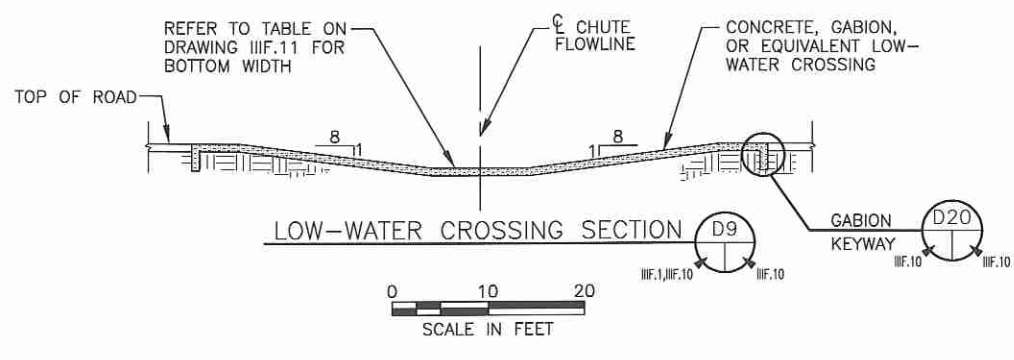
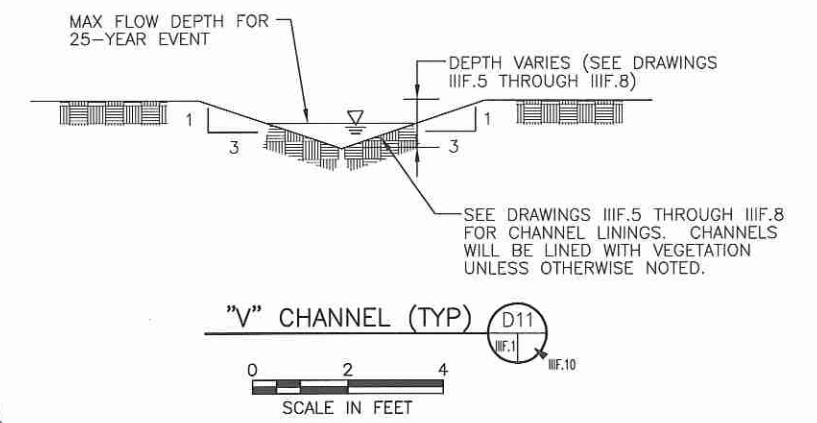
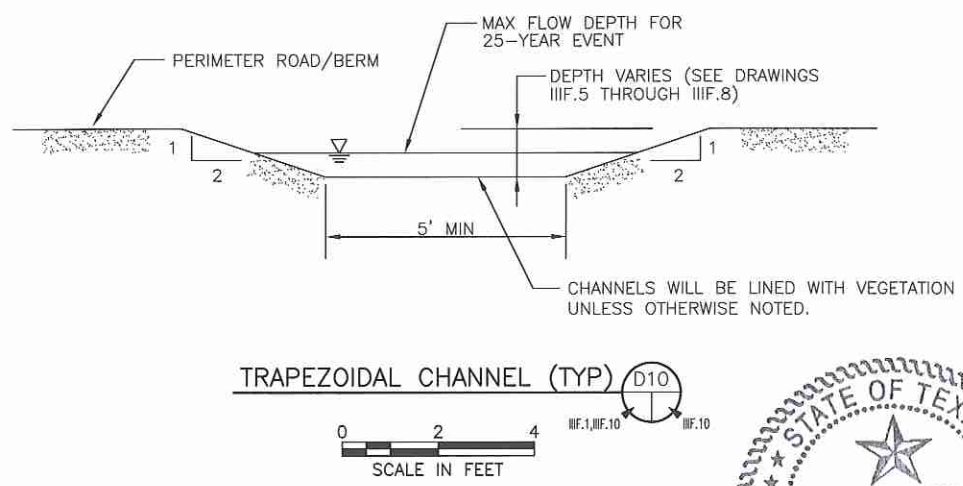
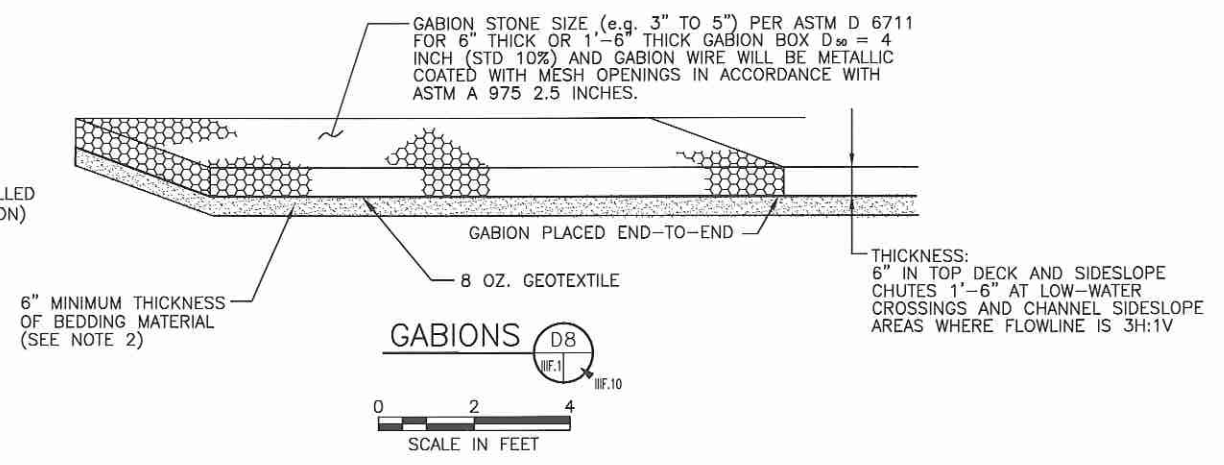
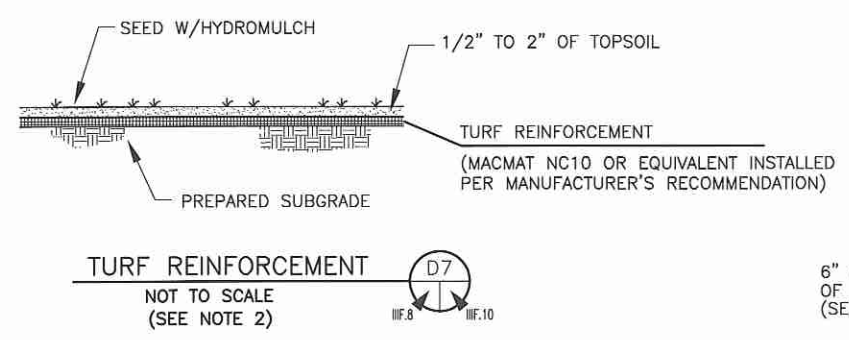
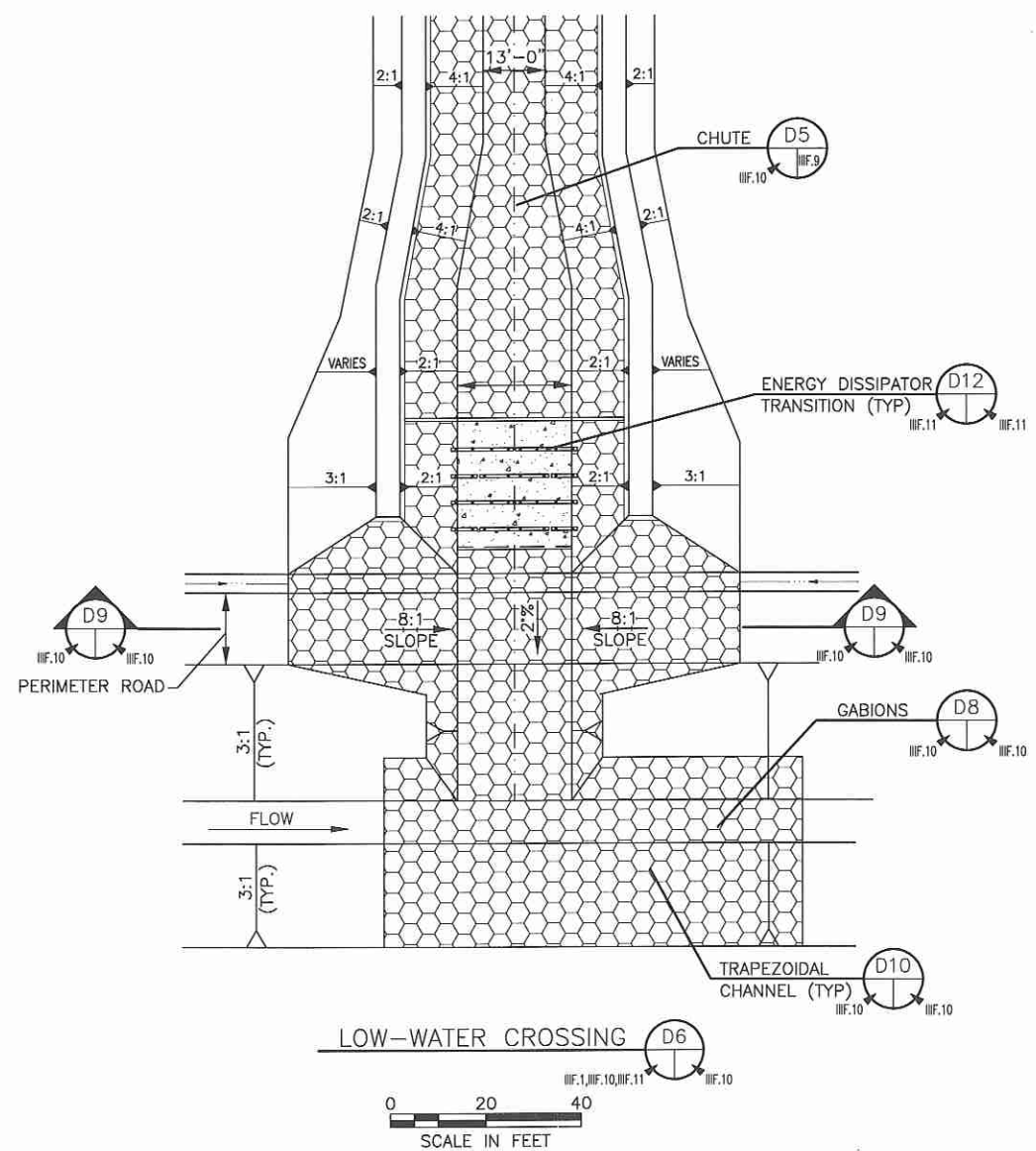
- REFER TO DRAWING IIIIF.1-DRAINAGE STRUCTURE PLAN FOR LOCATION OF DETAILS.
- BEDDING MATERIAL WILL CONSIST OF CLAYEY SOILS COMPACTED TO PROVIDE FIRM BASE THAT WILL BE overlain BY 8 oz/sy GEOTEXTILE PRIOR TO PLACEMENT OF GABIONS.
- CHUTE DETAILS ARE SHOWN WITH 13 FEET OF BOTTOM WIDTH. SEE APPENDIX IIIIF-C AND THE TABLE ON DRAWING IIIIF.11 FOR ACTUAL BOTTOM WIDTHS OF INDIVIDUAL CHUTES.
- EROSION LAYER WILL BE CAPABLE OF SUSTAINING VEGETATIVE GROWTH.
- REFER TO APPENDIX IIIJ-A-A FOR FINAL COVER DRAINAGE PIPE DESIGN AND TO DRAWING IIIJ-A-A-22 FOR FINAL COVER DRAINAGE PIPE LAYOUT. THE PIPE WILL EXTEND A MINIMUM OF 3-INCHES ABOVE THE TOP OF GABIONS.
- THE EDGES OF THE INSTALLED GABIONS TIE EITHER TO THE TOP OF THE EROSION LAYER (i.e., AT UPSTREAM END OF DRAINAGE LETDOWN) OR TO SOIL BERMS THAT ESTABLISH THE TOP OF THE DRAINAGE LETDOWN SIDE SLOPES.

STATE OF TEXAS
 NEVZAT TURAN
 84059
 LICENSED PROFESSIONAL ENGINEER
 2-28-12

<input type="checkbox"/> DRAFT <input checked="" type="checkbox"/> FOR PERMITTING PURPOSES ONLY <input type="checkbox"/> ISSUED FOR CONSTRUCTION <input type="checkbox"/> CLIENT APPROVAL BY:		PREPARED FOR CITY OF FARMERS BRANCH		MAJOR PERMIT AMENDMENT DRAINAGE DETAILS CAMELOT LANDFILL DENTON COUNTY, TEXAS													
DATE: 02/2012 FILE: 1339-351-11 CAD: IIIIF.9-DRAINAGE.DWG		DRAWN BY: SRF DESIGN BY: CRM REVIEWED BY: JPY		REVISIONS <table border="1"> <thead> <tr> <th>NO.</th> <th>DATE</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> </tbody> </table>		NO.	DATE	DESCRIPTION									
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<small>CHICAGO, IL NAPERVILLE, IL COLUMBUS, OH DENVER, CO</small>				<small>FORT WORTH, TX (817) 735-9770</small>													
<small>GRIFITH, IN SOUTH BEND, IN SPRINGFIELD, IL ST. LOUIS, MO</small>				TBPE REGISTRATION NO. F-3727 Weaver Boos Consultants DRAWING IIIIF.9													

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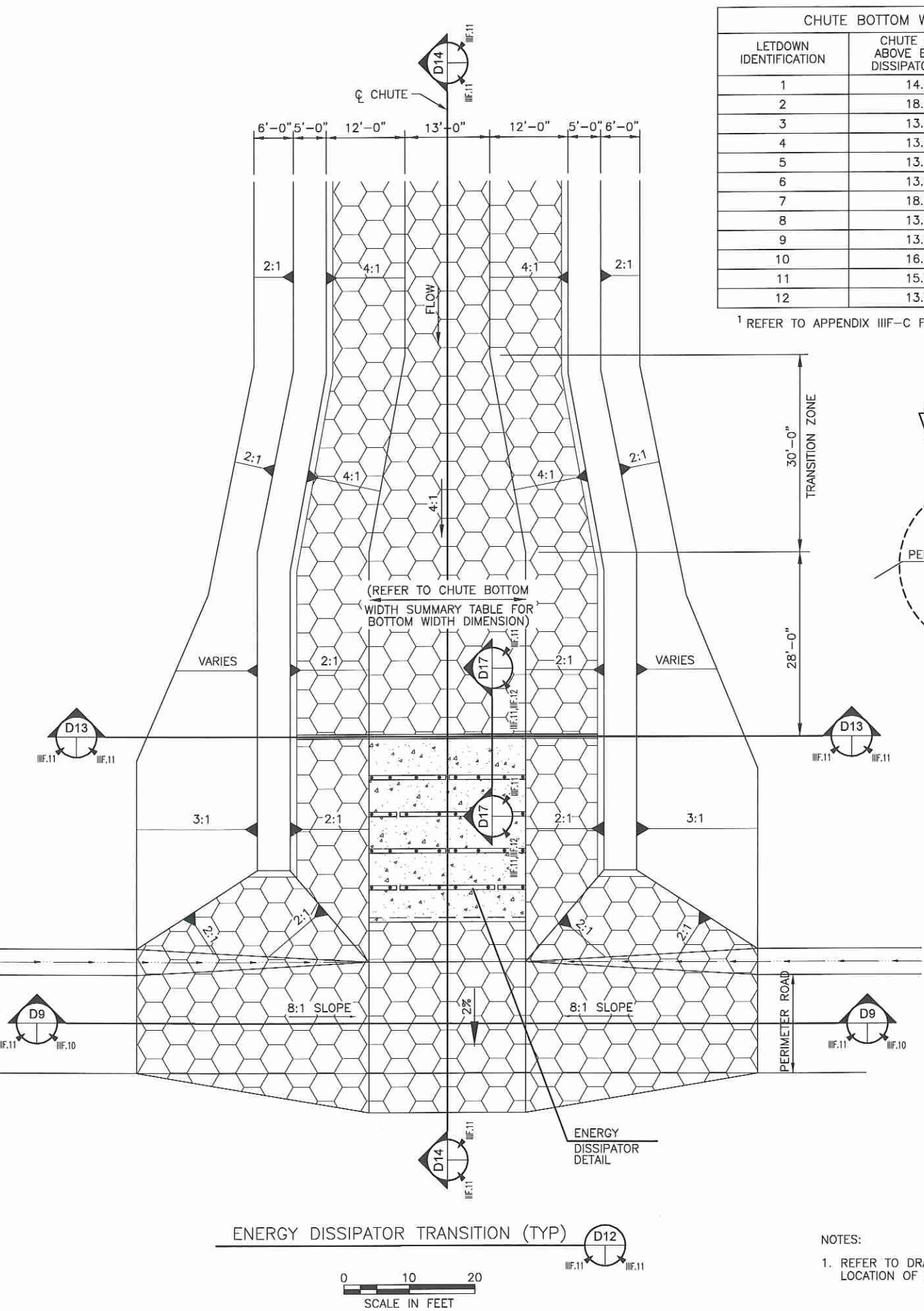
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- NOTES:
- REFER TO DRAWING III.F.1-DRAINAGE STRUCTURE PLAN FOR LOCATION OF DETAILS.
 - BEDDING MATERIAL WILL CONSIST OF CLAYEY SOILS COMPACTED TO PROVIDE A FIRM BASE THAT WILL BE overlain BY 8 oz/sy GEOTEXTILE PRIOR TO PLACEMENT OF GABIONS.

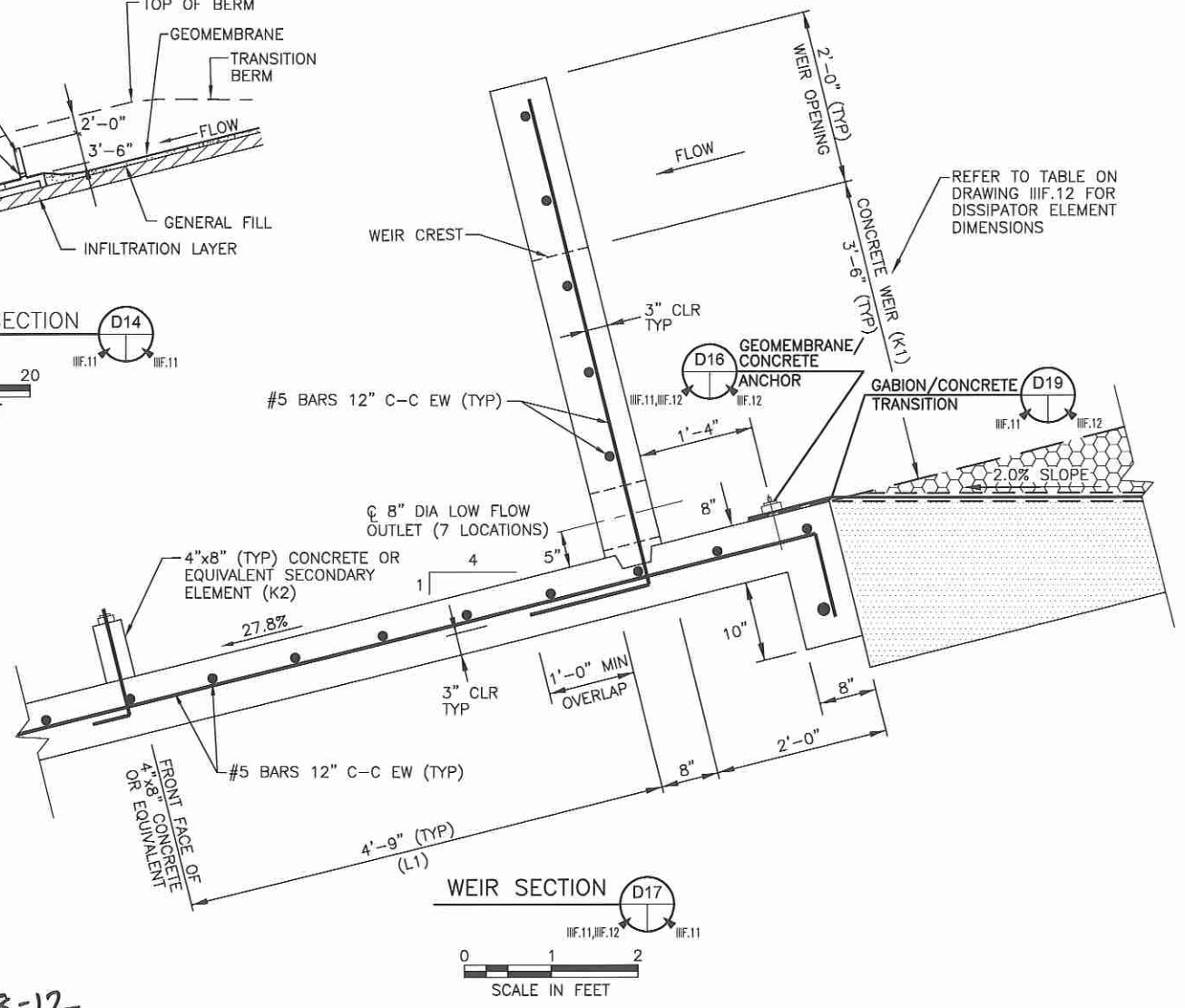
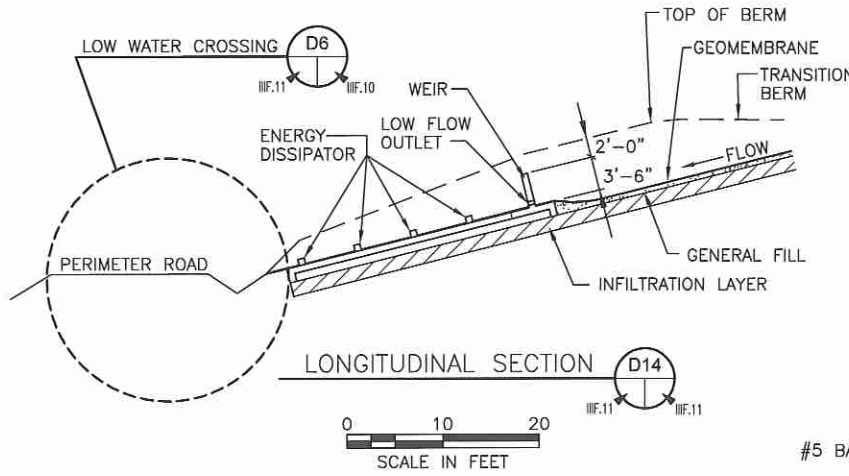
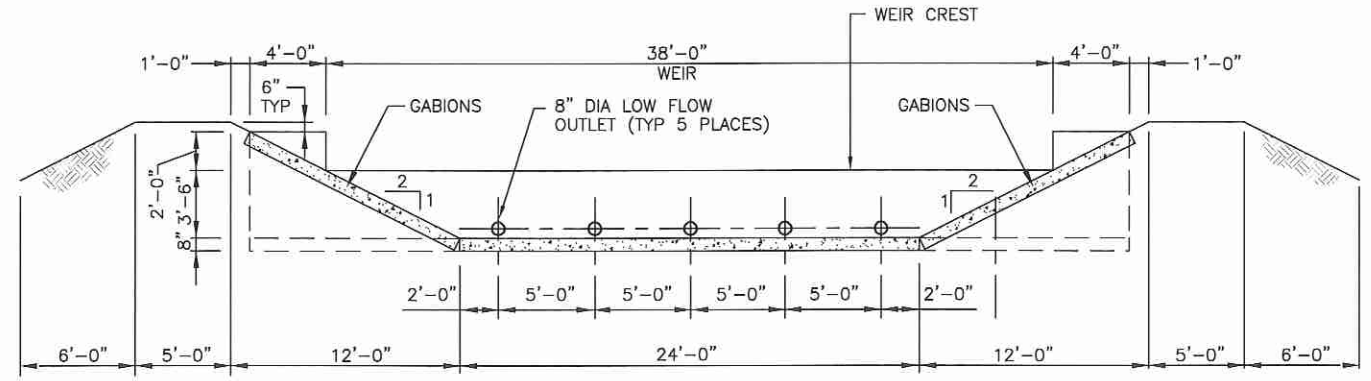
<input type="checkbox"/> DRAFT <input checked="" type="checkbox"/> FOR PERMITTING PURPOSES ONLY <input type="checkbox"/> ISSUED FOR CONSTRUCTION <input type="checkbox"/> CLIENT APPROVAL BY:		PREPARED FOR CITY OF FARMERS BRANCH	MAJOR PERMIT AMENDMENT DRAINAGE DETAILS CAMELOT LANDFILL DENTON COUNTY, TEXAS								
DATE: 02/2012 FILE: 1339-351-11 CAD: III.F.10-DRAINAGE.DWG	DRAWN BY: SRF DESIGN BY: CRM REVIEWED BY: JPY	REVISIONS <table border="1"> <thead> <tr> <th>NO.</th> <th>DATE</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> </tr> </tbody> </table>		NO.	DATE	DESCRIPTION					
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CHUTE BOTTOM WIDTH SUMMARY ¹		
LETDOWN IDENTIFICATION	CHUTE WIDTH ABOVE ENERGY DISSIPATOR (FT)	CHUTE WIDTH ABOVE TRANSITION ZONE (FT)
1	14.0	13.0
2	18.0	13.0
3	13.0	13.0
4	13.0	13.0
5	13.0	13.0
6	13.0	13.0
7	18.0	13.0
8	13.0	13.0
9	13.0	13.0
10	16.0	13.0
11	15.0	13.0
12	13.0	13.0

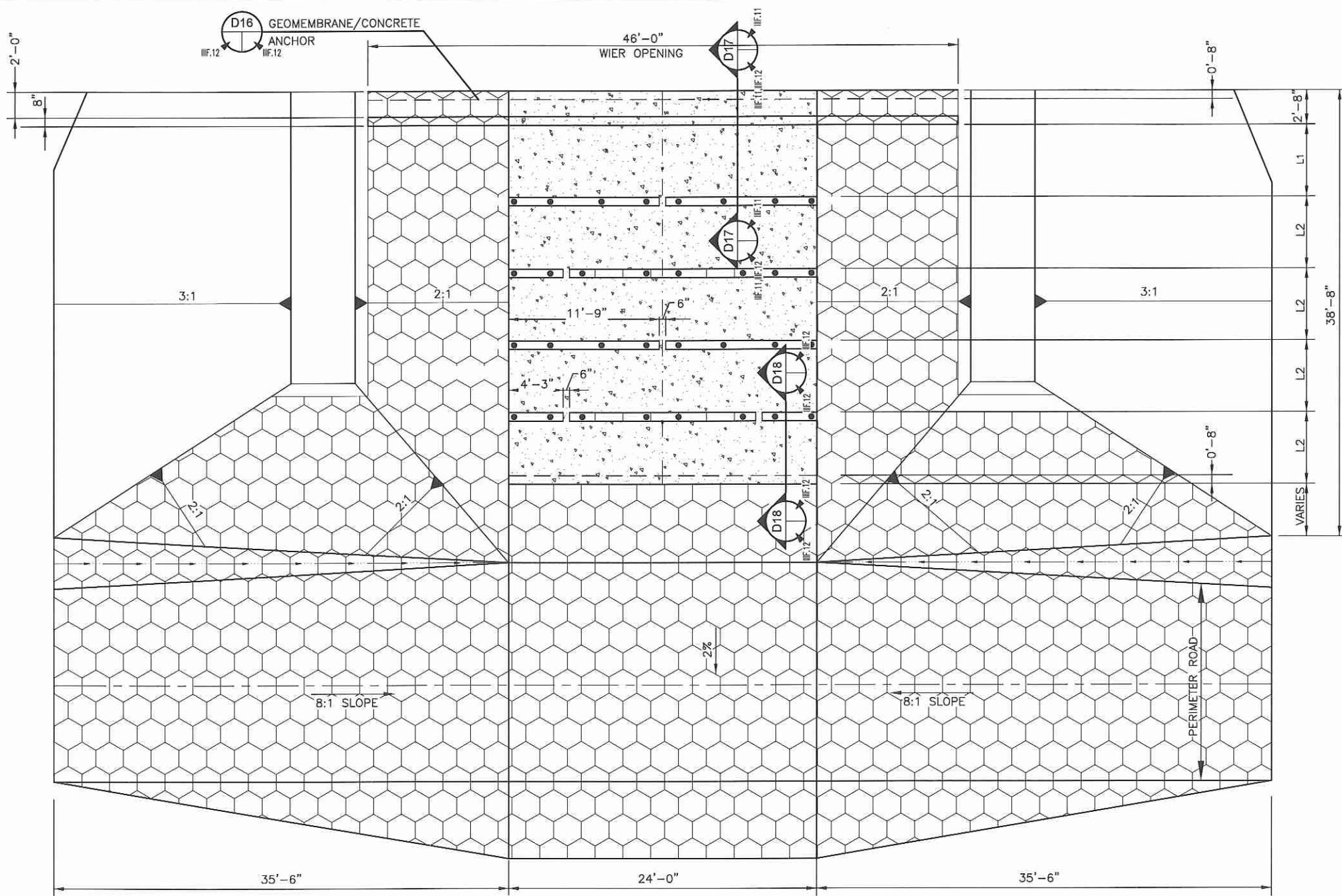
¹ REFER TO APPENDIX IIIF-C FOR SUPPORTING CALCULATIONS



NOTES:

1. REFER TO DRAWING IIIF.1--DRAINAGE STRUCTURE PLAN FOR LOCATION OF DETAILS.

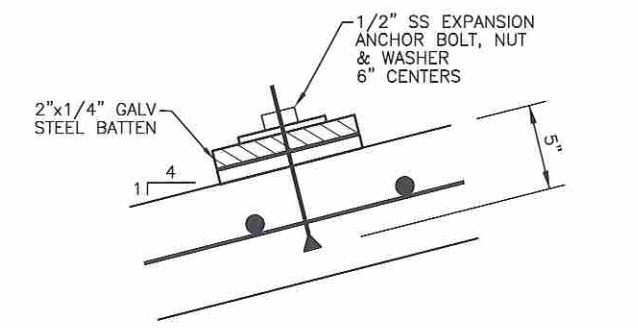
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DATE: 02/2012 FILE: 1339-351-11 CAD: IIIF.11--DRAINAGE.DWG	DRAWN BY: SRF DESIGN BY: CRM REVIEWED BY: JPY	REVISIONS NO. DATE DESCRIPTION	Weaver Boos Consultants TBPE REGISTRATION NO. F-3727
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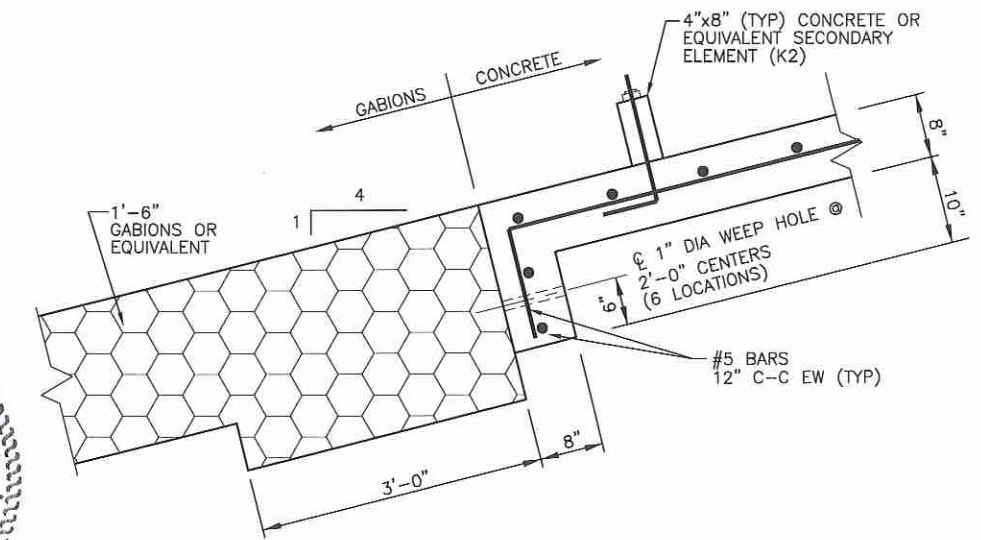
DISSIPATOR DESIGN SUMMARY ¹

LETDOWN IDENTIFICATION	HEIGHT OF		LENGTH BETWEEN	
	CONCRETE WEIR (K1) (FT)	SECONDARY ELEMENT (K2) (FT)	WEIR AND FIRST ELEMENT (L1) (FT)	ELEMENTS (L2) (FT)
1	3.5	0.96	4.83	8.9
2	3.5	0.95	4.73	8.8
3	3.0	0.75	2.55	5.0
4	3.0	0.75	3.67	7.0
5	3.5	0.92	4.56	8.5
6	3.0	0.75	2.91	5.6
7	3.5	0.97	4.84	8.9
8	3.0	0.75	3.11	6.0
9	3.0	0.78	3.80	7.2
10	3.5	0.97	4.86	9.0
11	3.5	0.93	4.63	8.6
12	3.0	0.82	4.04	7.6

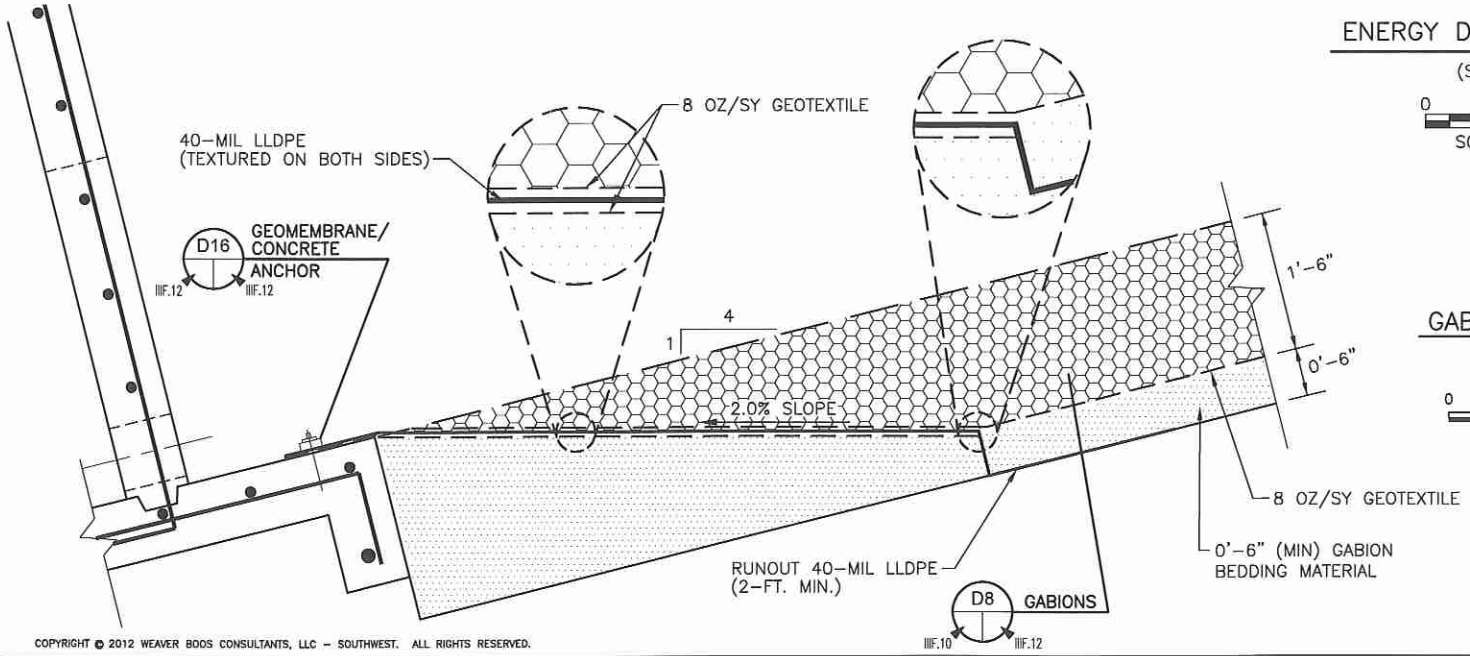
¹ REFER TO APPENDIX III-F-C FOR SUPPORTING CALCULATIONS



GEOMEMBRANE/CONCRETE ANCHOR (D16)
NTS

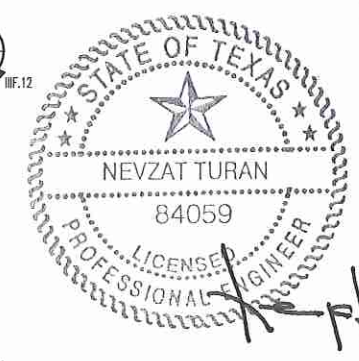


DISSIPATOR SECTION (TYP) (D18)
SCALE IN FEET



ENERGY DISSIPATOR DETAIL (D15)
(SEE NOTE 1)
SCALE IN FEET

GABION/CONCRETE TRANSITION (D19)
SCALE IN FEET

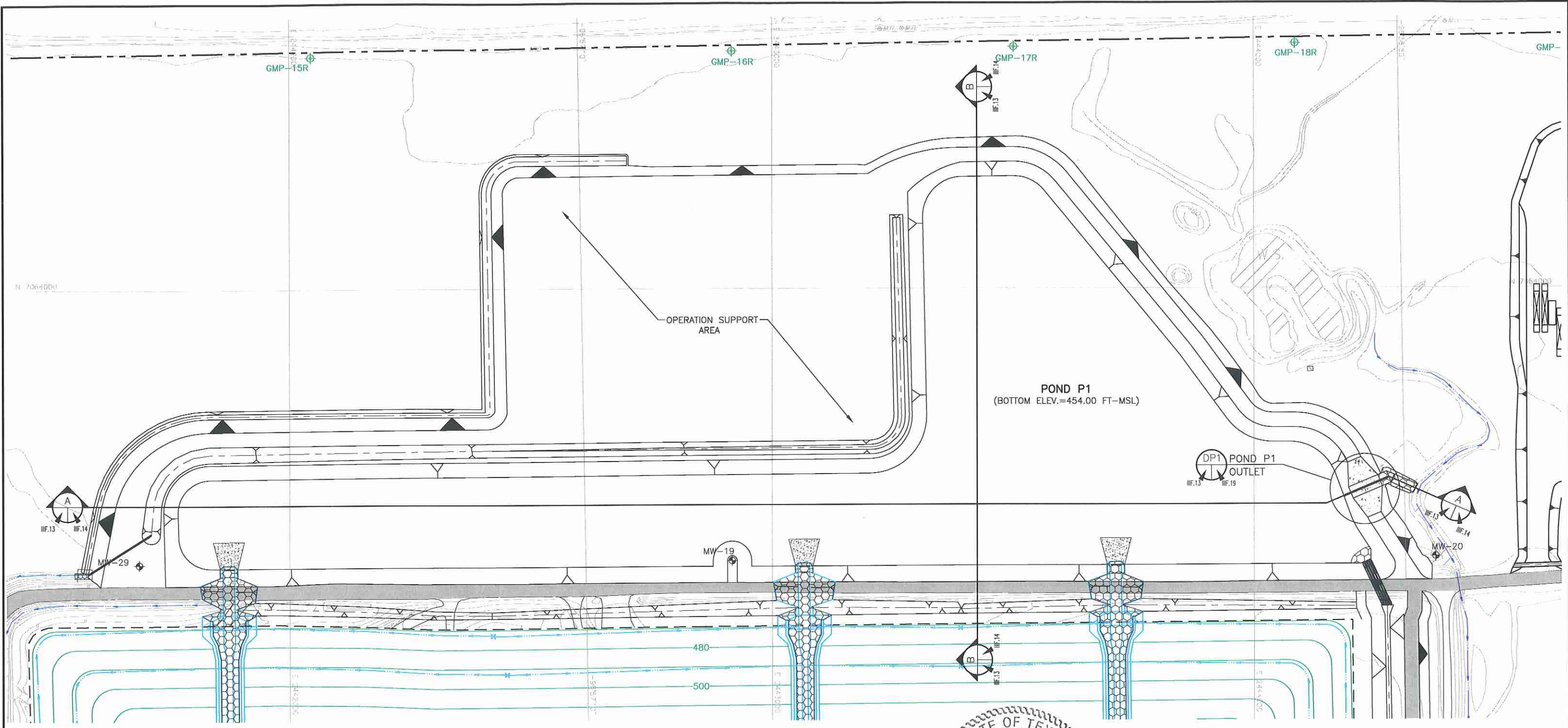


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<input type="checkbox"/> DRAFT <input checked="" type="checkbox"/> FOR PERMITTING PURPOSES ONLY <input type="checkbox"/> ISSUED FOR CONSTRUCTION <input type="checkbox"/> CLIENT APPROVAL BY:	PREPARED FOR CITY OF FARMERS BRANCH	MAJOR PERMIT AMENDMENT DRAINAGE DETAILS CAMELOT LANDFILL DENTON COUNTY, TEXAS												
DATE: 02/2012 FILE: 1339-351-11 CAD: III.12-DRAINAGE.DWG	DRAWN BY: SRF DESIGN BY: CRM REVIEWED BY: JPY	Weaver Boos Consultants TBPE REGISTRATION NO. F-3727												
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NO.	DATE	DESCRIPTION												
FORT WORTH, TX (817) 735-9770	GRIFFITH, IN SOUTH BEND, IN SPRINGFIELD, IL ST. LOUIS, MO	DRAWING III.F.12												

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O:\1339\351\EXPANSION 2009\PART III--SDP\IIF\IIF.13-18_PONDS.dwg, jwilson, 1:2



POND P1	
ELEVATION (FT-MSL)	SURFACE AREA (AC)
454	17.18
455	17.75
456	18.16
457	18.58
458	18.99
459	19.41
460	19.82

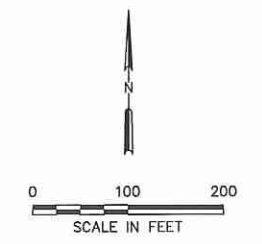
- LEGEND**
- PERMIT BOUNDARY
 - PROPOSED LIMIT OF WASTE
 - STATE PLANE COORDINATE SYSTEM
 - GEODETIC COORDINATE SYSTEM
 - EXISTING CONTOUR (SEE NOTE 1)
 - FINAL COVER CONTOUR
 - DRAINAGE LETDOWN
 - DRAINAGE SWALE
 - MW-29 PERMITTED GROUNDWATER MONITORING WELL
 - GMP-14R PROPOSED GAS MONITORING PROBE

NOTE:

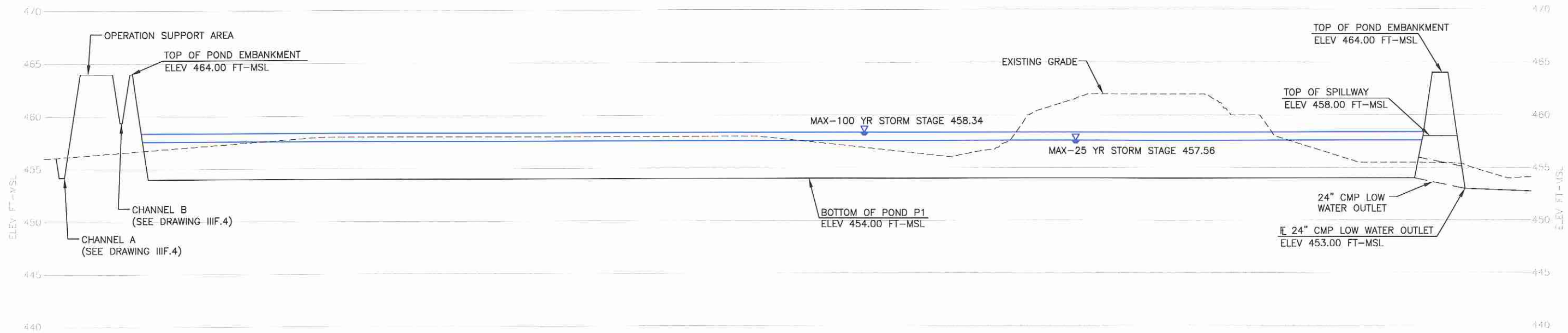
- CONTOURS AND ELEVATIONS PROVIDED BY METROPOLITAN AERIAL SURVEYS COMPILED FROM AERIAL PHOTOGRAPHY FLOWN 8-28-2010. THE GRID SYSTEM IS TIED TO THE TEXAS STATE PLANE COORDINATE SYSTEM NORTH CENTRAL ZONE NAD 1983. ELEVATIONS ARE BASED ON NAVD 1988.
- PERMIT BOUNDARY WAS PREPARED BY PEISER SUREYING CO. IN NOVEMBER 2010.



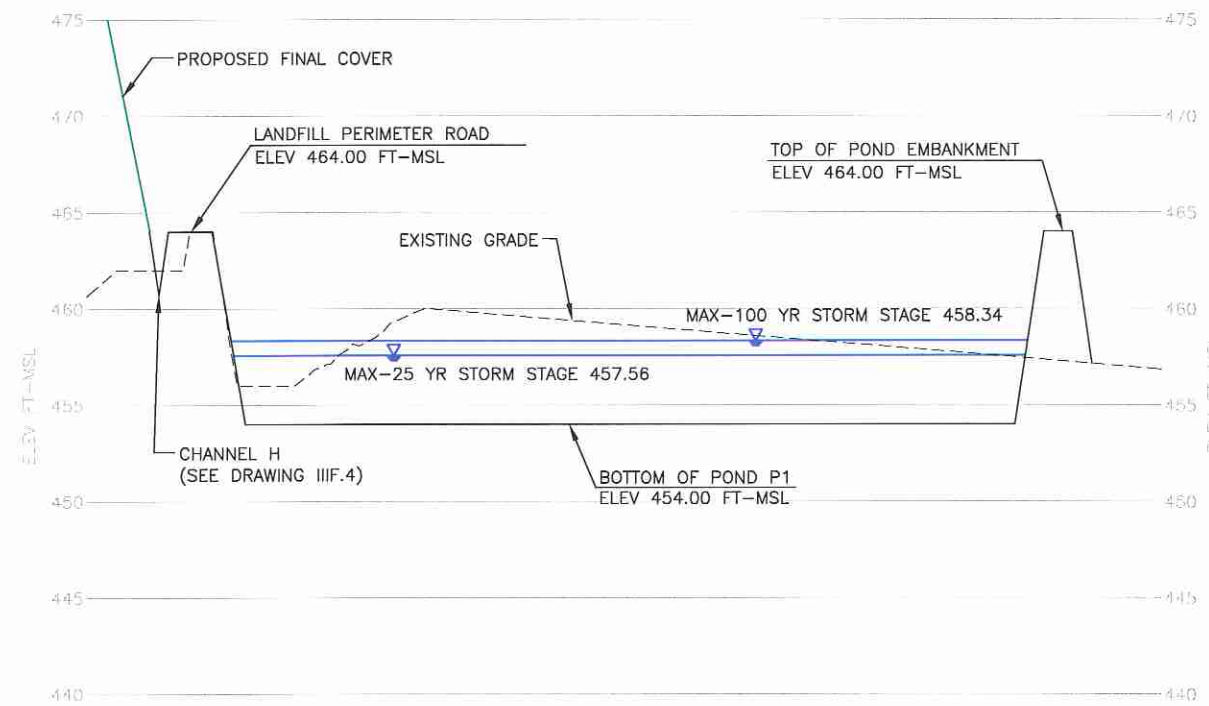
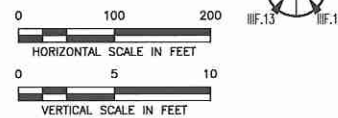
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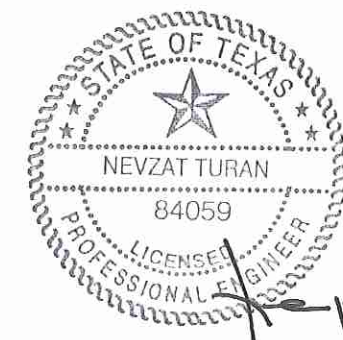
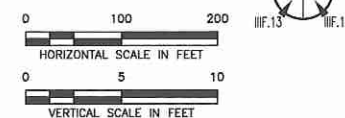
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DATE: 02/2012 FILE: 1339-351-11 CAD: IIF.13-18_PONDS.DWG	DRAWN BY: JOW DESIGN BY: CRM REVIEWED BY: JPY	REVISIONS <table border="1"> <thead> <tr> <th>NO.</th> <th>DATE</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> </tr> </tbody> </table>		NO.	DATE	DESCRIPTION						
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DETENTION POND P1 SECTION A



DETENTION POND P1 SECTION B

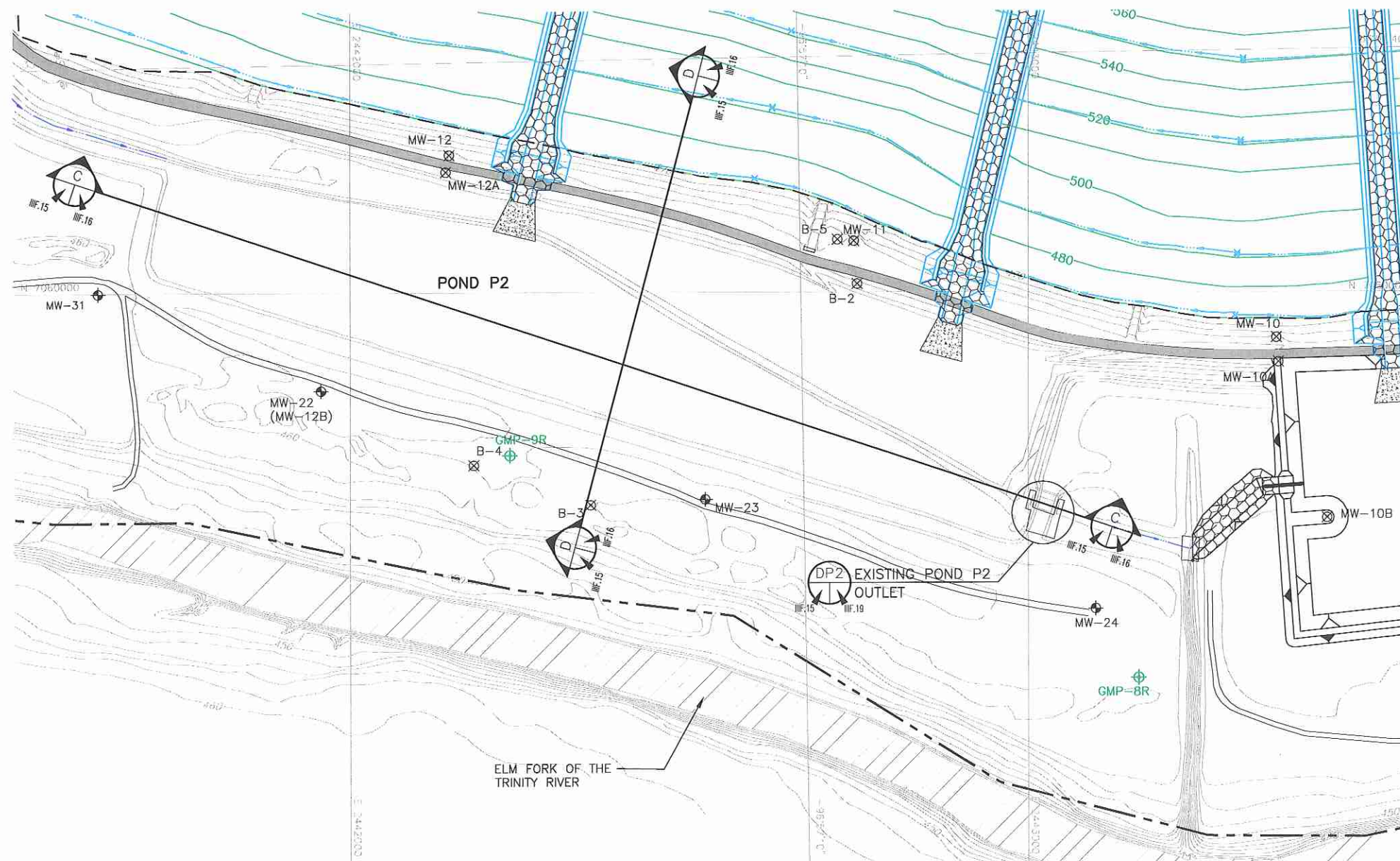


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DATE: 02/2012 FILE: 0120-84-11 CAD: III.F.13-18 POND.DWG	DRAWN BY: JDW DESIGN BY: JAE REVIEWED BY: JPY	REVISIONS <table border="1"> <thead> <tr> <th>NO.</th> <th>DATE</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> </tbody> </table>	NO.	DATE	DESCRIPTION										CAMELOT LANDFILL DENTON COUNTY, TEXAS <i>Weaver Boos Consultants</i> TBPE REGISTRATION NO. F-3727
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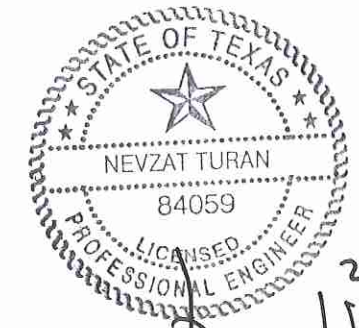


POND P2	
ELEVATION (FT-MSL)	SURFACE AREA (AC)
454	4.08
455	6.79
456	8.38
457	8.62
458	8.87
459	9.12

- LEGEND**
- PERMIT BOUNDARY
 - - - PROPOSED LIMIT OF WASTE
 - N 7060000 STATE PLANE COORDINATE SYSTEM
 - 86°57'10" GEODETIC COORDINATE SYSTEM
 - 450 EXISTING CONTOUR (SEE NOTE 1)
 - 500 FINAL COVER CONTOUR
 - DRAINAGE LETDOWN
 - DRAINAGE SWALE
 - ◆ MW-22 PERMITTED GROUNDWATER MONITORING WELL
 - ⊕ GMP-9 PERMITTED GAS MONITORING PROBE
 - ⊗ MW-12 PERMITTED OBSERVATION WELL

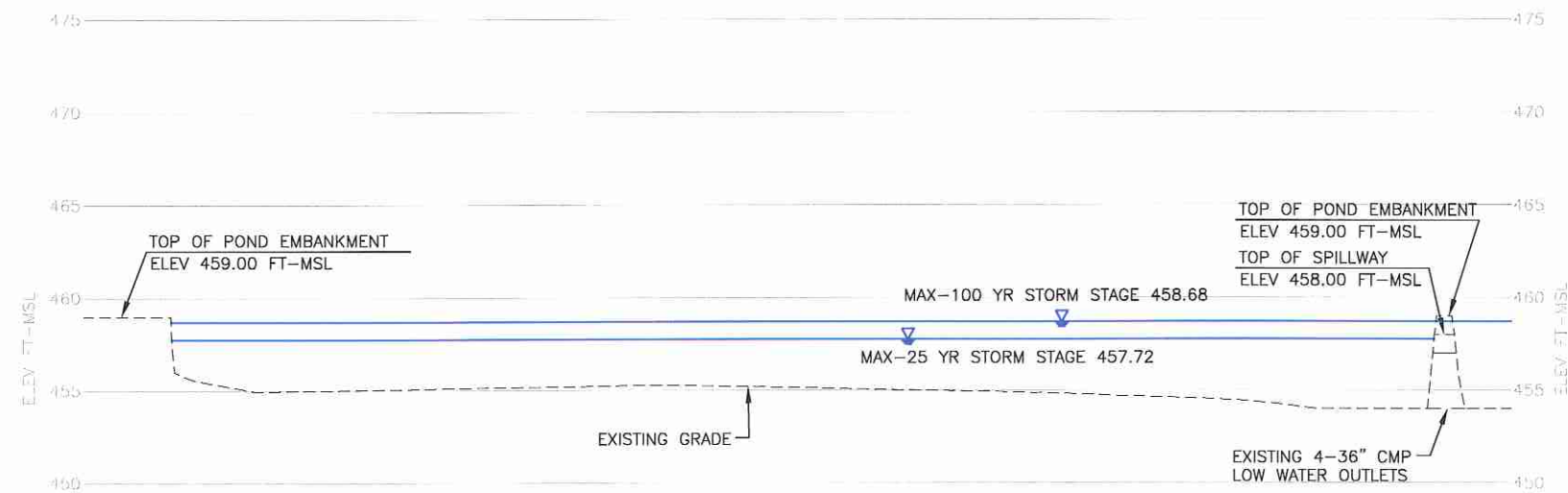
NOTE:

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- PERMIT BOUNDARY WAS PREPARED BY PEISER SUREYING CO. IN NOVEMBER 2010.

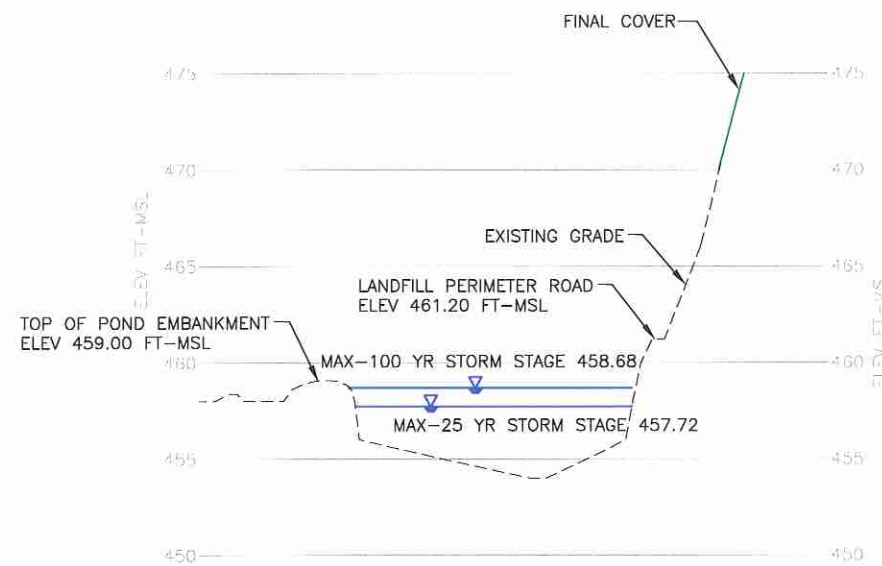
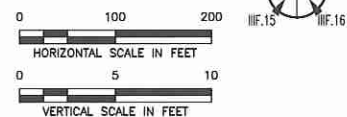


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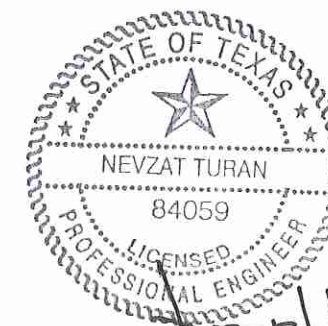
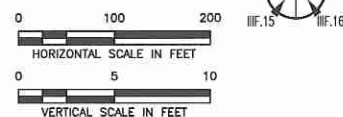
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DATE: 02/2012 FILE: 1339-351-11 CAD: IIF.13-18_PONDS.DWG	DRAWN BY: JOW DESIGN BY: CRM REVIEWED BY: JPY													
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NO.	DATE	DESCRIPTION												



DETENTION POND P2 SECTION C

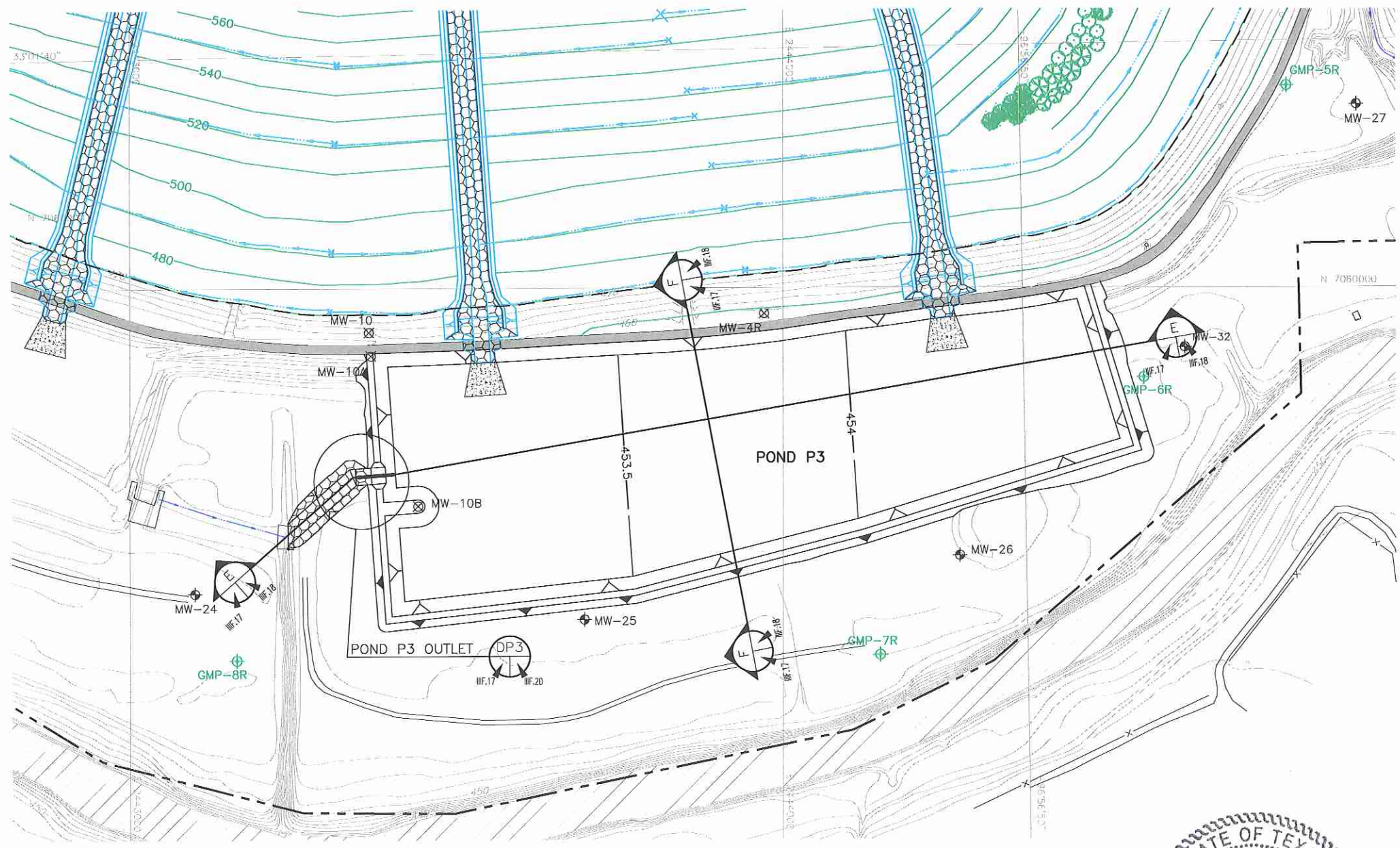


DETENTION POND P2 SECTION D



2-28-12

<input type="checkbox"/> DRAFT <input checked="" type="checkbox"/> FOR PERMITTING PURPOSES ONLY <input type="checkbox"/> ISSUED FOR CONSTRUCTION <input type="checkbox"/> CLIENT APPROVAL BY:	PREPARED FOR CITY OF FARMERS BRANCH	MAJOR PERMIT AMENDMENT POND P2 SECTIONS CAMELOT LANDFILL DENTON COUNTY, TEXAS
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		GRIFFITH, IN SOUTH BEND, IN SPRINGFIELD, IL ST. LOUIS, MO
		DRAWING IIF.16



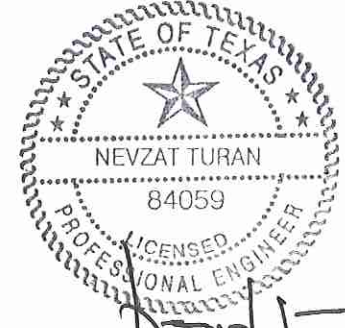
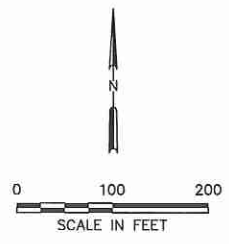
POND P3

ELEVATION (FT-MSL)	SURFACE AREA (AC)
453.5	2.73
454	5.36
455	7.71
456	7.97
457	8.16
458	8.36
459	8.56

- LEGEND**
- PERMIT BOUNDARY
 - PROPOSED LIMIT OF WASTE
 - N 7080000 STATE PLANE COORDINATE SYSTEM
 - 450' 40" GEODETIC COORDINATE SYSTEM
 - 450 EXISTING CONTOUR (SEE NOTE 1)
 - 500 FINAL COVER CONTOUR
 - [Pattern] DRAINAGE LETDOWN
 - [Symbol] DRAINAGE SWALE
 - [Symbol] MW-25 PERMITTED GROUNDWATER MONITORING WELL
 - [Symbol] MW-30 PROPOSED GROUNDWATER MONITORING WELL
 - [Symbol] GMP-14R PROPOSED GAS MONITORING PROBE

NOTE:

- CONTOURS AND ELEVATIONS PROVIDED BY METROPOLITAN AERIAL SURVEYS COMPILED FROM AERIAL PHOTOGRAPHY FLOWN 8-28-2010. THE GRID SYSTEM IS TIED TO THE TEXAS STATE PLANE COORDINATE SYSTEM NORTH CENTRAL ZONE NAD 1983. ELEVATIONS ARE BASED ON NAVD 1988.
- PERMIT BOUNDARY WAS PREPARED BY PEISER SUREYING CO. IN NOVEMBER 2010.

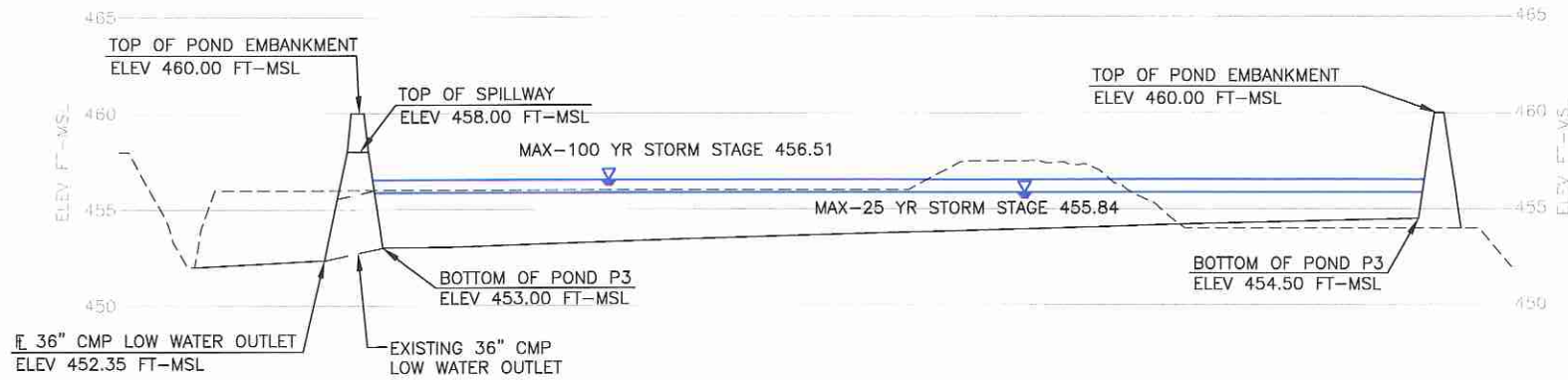


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DATE: 02/2012 FILE: 1339-351-11 CAD: IIF.13-18 POND3.DWG	DRAWN BY: JDW DESIGN BY: CRM REVIEWED BY: JPY	REVISIONS <table border="1"> <thead> <tr> <th>NO.</th> <th>DATE</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> </tbody> </table>		NO.	DATE	DESCRIPTION								
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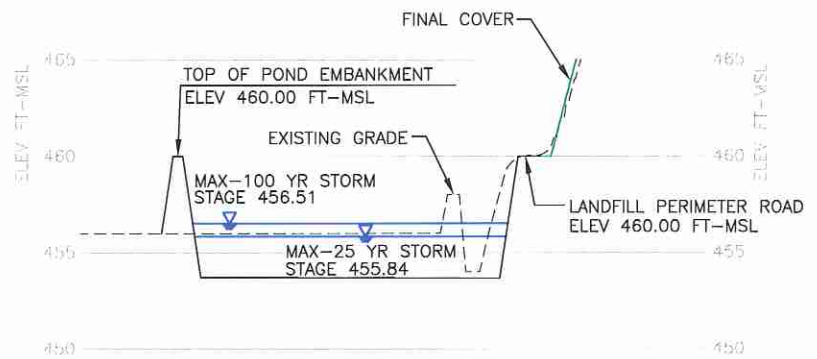
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DETENTION POND P3 SECTION DP3

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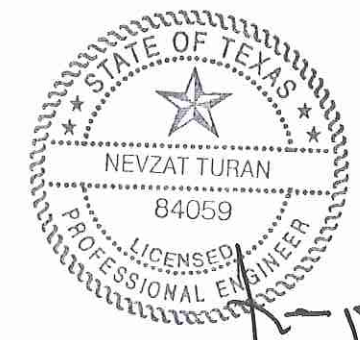
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DETENTION POND P3 SECTION DP3

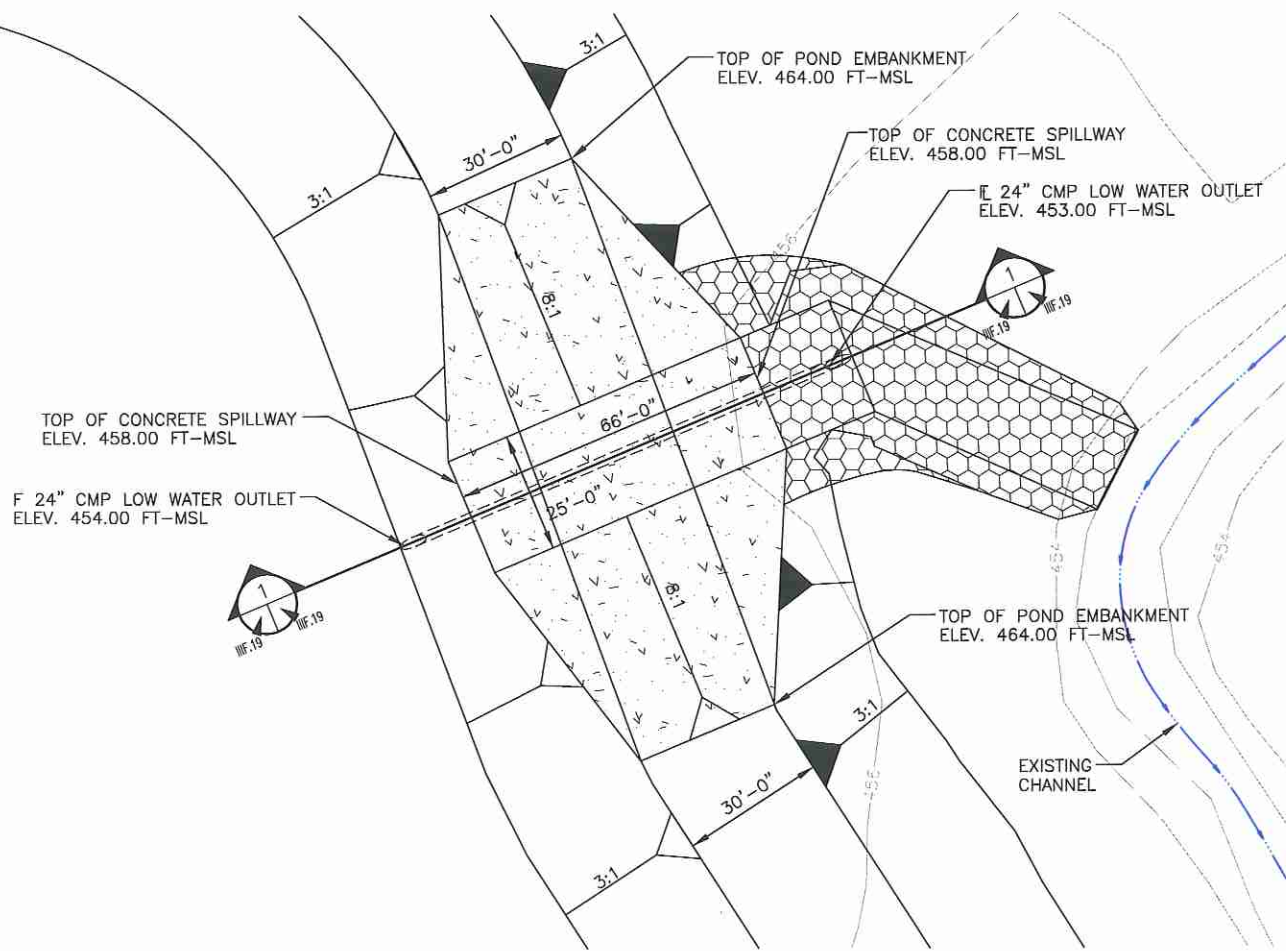
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0 5 10 VERTICAL SCALE IN FEET

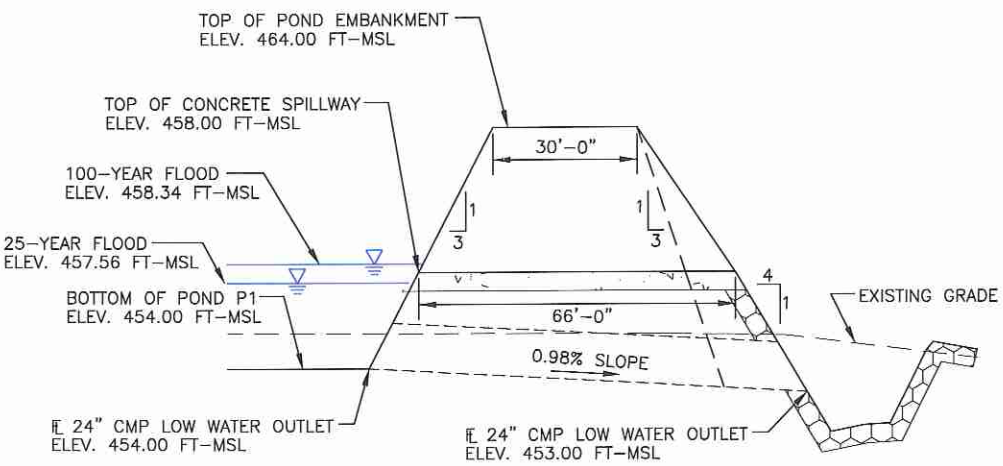


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2-28-12

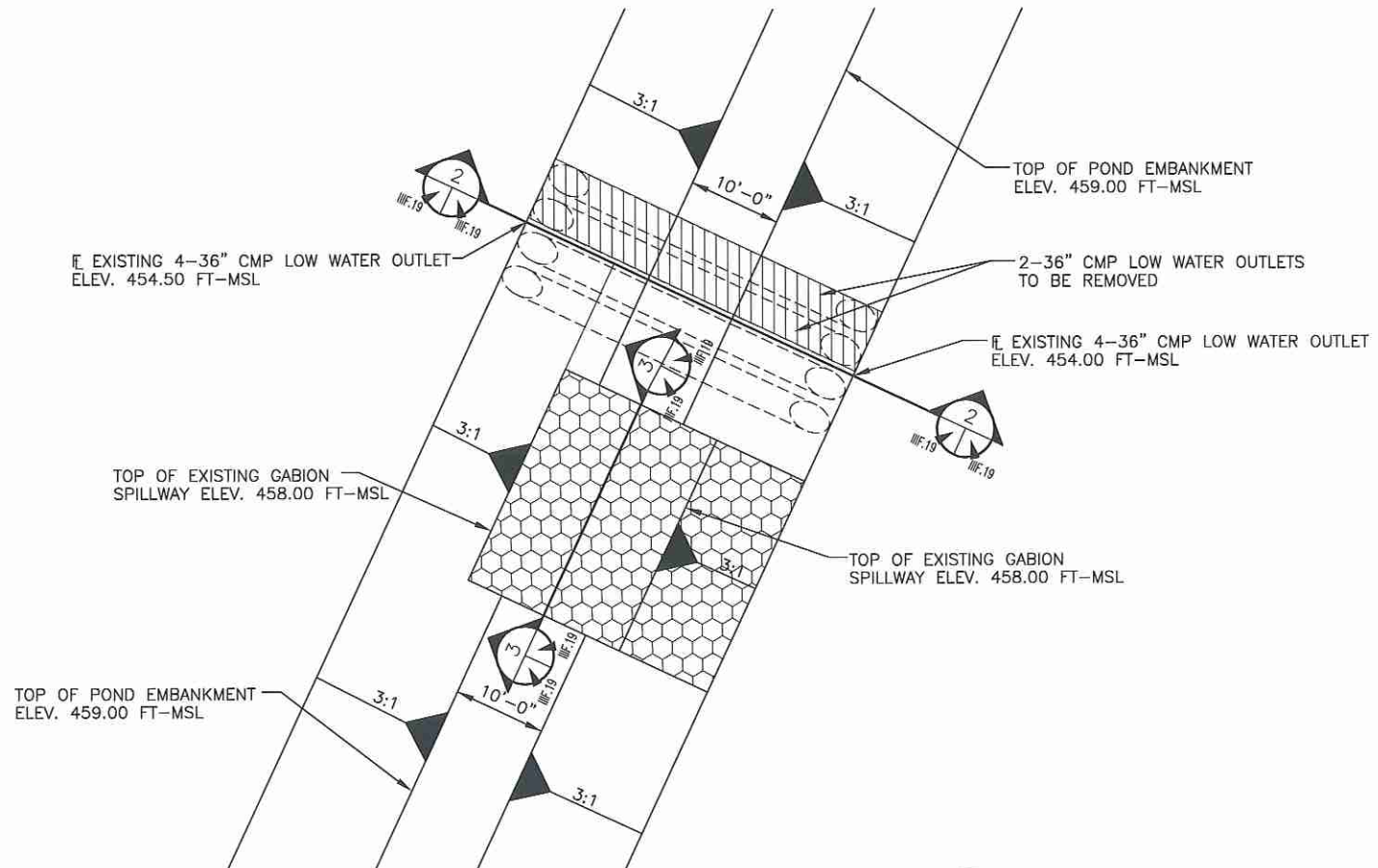
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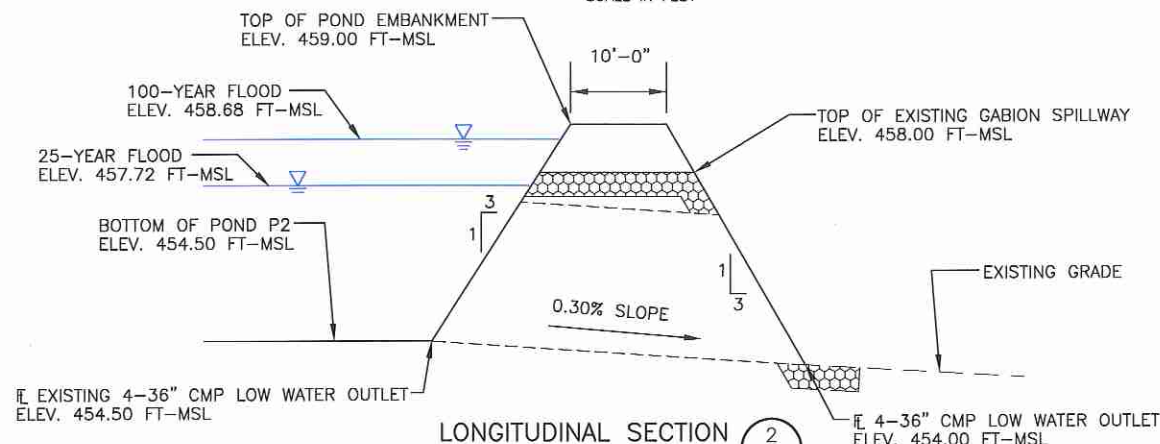
POND P1 OUTLET STRUCTURE DP1
 SCALE IN FEET



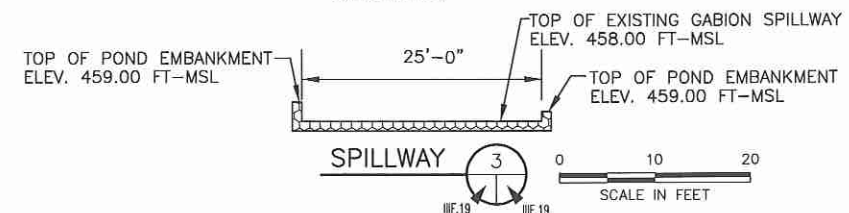
LONGITUDINAL SECTION 1
 SCALE IN FEET



POND P2 EXISTING OUTLET STRUCTURE DP2
 SCALE IN FEET



LONGITUDINAL SECTION 2
 SCALE IN FEET



SPILLWAY 3
 SCALE IN FEET

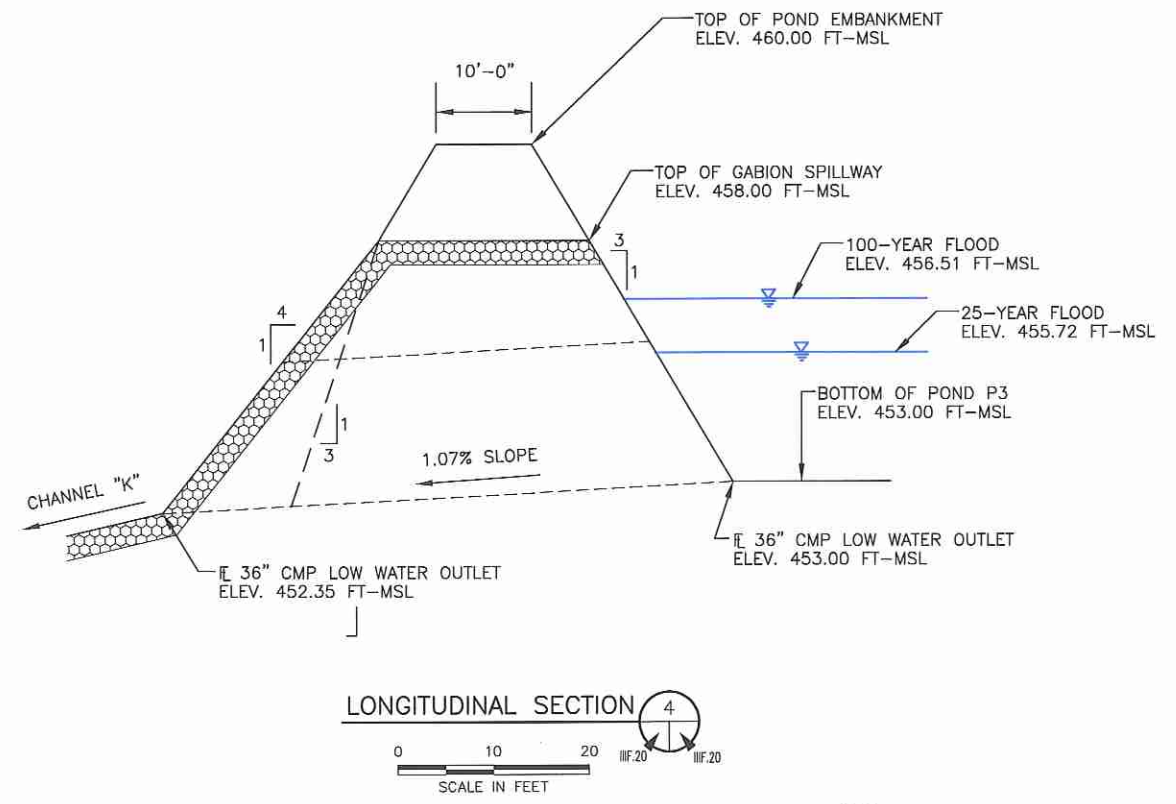
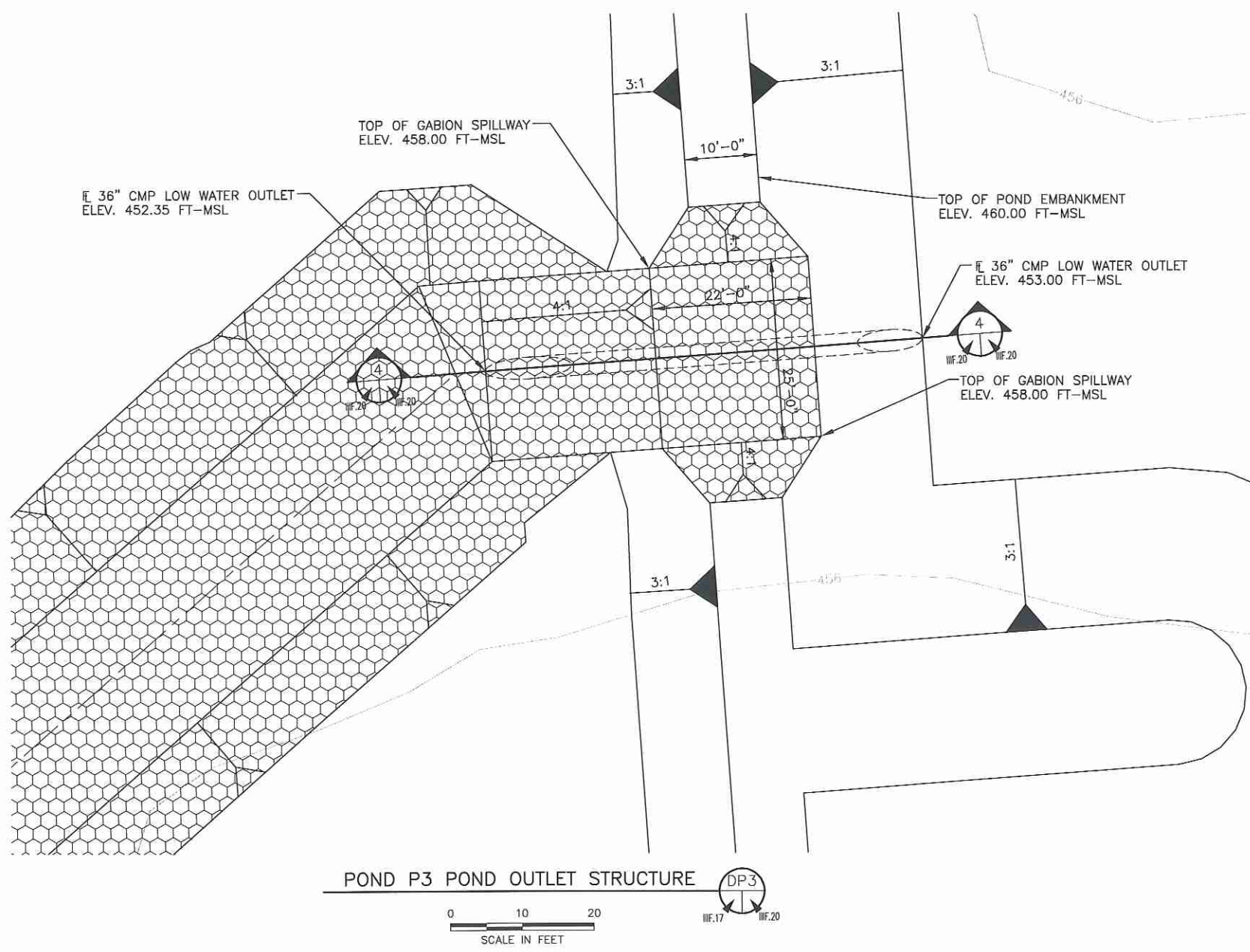


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DATE: 02/2012 FILE: 1339-351-11 CAD: IIF.19-20 OUTLET.DWG	DRAWN BY: JDW DESIGN BY: CRM REVIEWED BY: JPY	REVISIONS NO. DATE DESCRIPTION	
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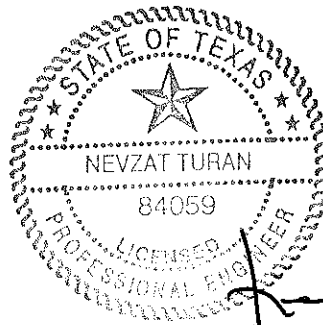
STATE OF TEXAS
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 NEVZAT TURAN
 84059
 LICENSED PROFESSIONAL ENGINEER

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DATE: 02/2012 FILE: 1339-351-11 CAD: IIF.19-20 OUTLET.DWG	DRAWN BY: JOW DESIGN BY: CRM REVIEWED BY: JPY	REVISIONS <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 5%;">NO.</th> <th style="width: 10%;">DATE</th> <th style="width: 85%;">DESCRIPTION</th> </tr> </thead> <tbody> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> </tbody> </table>	NO.	DATE	DESCRIPTION									
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		Weaver Boos Consultants TBPE REGISTRATION NO. F-3727 DRAWING IIF.20												

APPENDIX IIIF-A

**POST-DEVELOPMENT CONDITION
HYDROLOGIC CALCULATIONS**

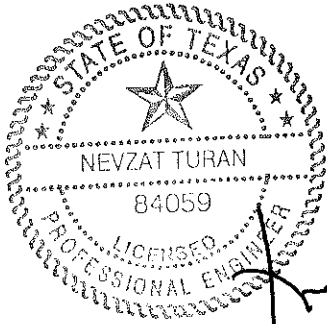


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Includes pages IIIF-A-1 through IIIF-A-116

CONTENTS

Hypothetical Storm Data	IIIF-A-1
Precipitation Loss Data	IIIF-A-3
Hydrograph Development Information	IIIF-A-15
Post-development HEC-1 Analysis Drainage Areas	IIIF-A-27
HEC-1 Output – Post-development 25-Year, 24-Hour Storm Event	IIIF-A-30
Volume Calculations	IIIF-A-105
Velocity Calculations	IIIF-A-111



19/1/1
2-28-12

HYPOTHETICAL STORM DATA

Hypothetical Storm Data

Precipitation data taken from TP-40 and Hydro 35 rainfall data.

Time	5 min	15 min	60 min	2 hr	3 hr	6 hr	12 hr	24 hr
25-Year Event	0.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44
100-Year Event	0.88	1.87	4.30	5.45	5.75	6.80	8.30	9.45

TP-40 (*U.S. Department of Commerce, May 1961*) was used to identify precipitation values for storm durations ranging from 60 minutes to 24 hours.

Hydro 35 (*National Oceanic and Atmospheric Administration, June 1977*) was used to estimate precipitation for the 5 minute and 15 minute duration storm events.

PRECIPITATION LOSS DATA

Required: Determine the SCS curve numbers for both on-site and off-site drainage areas for use in the HEC-1 analysis.

- References:**
1. Dodson's and Associates, Inc., *ProHec-1 Plus Program Documentation*, 1995.
 2. United States Department of Agriculture, National Resource Conservation Service, Web Soil Survey for Hill County, Texas (<http://websoilsurvey.nrcs.usda.gov>).
 3. The Hydrologic Evaluation of Landfill Performance (HELP) Model - Engineering Documentation for version 3. EPA/600/R-94/168b, September 1994.

Note: Approximate non landfill areas within the permit boundary on SCS map (page IIIF-A-5).

Solution: Based on the soil survey information found in Ref. 2, hydrologic group D soils predominate the soils within the permit boundary drainage area (see pages IIIF-A-5 through IIIF-A-7).

All on-site drainage areas and off-site drainage areas near the site (O3, O4, and O5) were considered pasture land in fair conditions. A curve number was selected using the table on page IIIF-A-8.

Use: CN = 84

Curve numbers for offsite areas O1, O1A, and O2 were calculated using an area-weighted average of rural and urban land uses, including pasture or range in fair condition, 1/4 acre average residential lots, and industrial districts. The calculated composite curve numbers are shown below.

Use: CN = 87	for area O1
Use: CN = 85	for area O1A
Use: CN = 85	for area O2

The final cover system was assumed to be in place and the erosion layer will control precipitation loss. A curve number that is corrected for the surface slope of the erosion layer may be computed first using the chart on page IIIF-A-8 to select an un-adjusted curve number. Calculate the adjusted curve number using equation 34 from Ref. 3 (see page IIIF-A-8).

$$CN_{\bar{n}} = 100 - (100 - CN_{II_o}) * (L^* / S^*) ^ (CN_{II_o}^{-0.81})$$

Use: CN _{II_o} = 84, L* = (300/500), S* = (.04/.04)	for top dome surfaces
Use: CN _{II_o} = 84, L* = (120/500), S* = (.25/.04)	for side slopes








































Calculate: CN = 84	for top dome surfaces
Calculate: CN = 86	for side slopes

- Use curve number calculated for side slopes for the entire final cover area, including top dome areas, conservatively.

The pond areas are assumed to collect all precipitation for their areas:

Use: CN = 100

MAP LEGEND

 Area of Interest (AOI)	 Very Stony Spot
 Soils	 Wet Spot
 Area of Interest (AOI)	 Other
 Soil Map Units	Special Line Features
 Blowout	 Gully
 Borrow Pit	 Short Steep Slope
 Clay Spot	 Other
 Closed Depression	Political Features
 Gravel Pit	 Cities
 Gravelly Spot	Water Features
 Landfill	 Oceans
 Lava Flow	 Streams and Canals
 Marsh or swamp	Transportation
 Mine or Quarry	 Rails
 Miscellaneous Water	 Interstate Highways
 Perennial Water	 US Routes
 Rock Outcrop	 Major Roads
 Saline Spot	 Local Roads
 Sandy Spot	
 Severely Eroded Spot	
 Sinkhole	
 Slide or Slip	
 Sodic Spot	
 Spoil Area	
 Stony Spot	

MAP INFORMATION

Map Scale: 1:14,700 if printed on B size (11" x 17") sheet.

The soil surveys that comprise your AOI were mapped at 1:24,000. Please rely on the bar scale on each map sheet for accurate map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL: <http://websoilsurvey.nrcs.usda.gov>
 Coordinate System: UTM Zone 14N NAD83

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Denton County, Texas
 Survey Area Data: Version 7, Jan 14, 2010
 Date(s) aerial images were photographed: 1995

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Denton County, Texas (TX121)			
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
3	Altoga silty clay, 5 to 8 percent slopes	77.8	3.6%
4	Altoga silty clay, 5 to 12 percent slopes, eroded	68.7	3.2%
5	Aquilla loamy fine sand, 2 to 5 percent slopes	37.7	1.7%
6	Arents, gently undulating	36.7	1.7%
7	Arents, hilly	102.5	4.7%
9	Bastil fine sandy loam, 1 to 3 percent slopes	35.8	1.6%
10	Bastil fine sandy loam, 3 to 5 percent slopes	32.7	1.5%
21	Burleson clay, 0 to 1 percent slopes	61.0	2.8%
22	Burleson clay, 1 to 3 percent slopes	80.7	3.7%
27	Crockett fine sandy loam, 1 to 3 percent slopes	79.8	3.7%
32	Ferris-Heiden clay, 5 to 15 percent slopes	66.5	3.1%
33	Frio silty clay, occasionally flooded	391.4	18.0%
44	Houston Black clay, 1 to 3 percent slopes	3.7	0.2%
53	Lewisville clay loam, 3 to 5 percent slopes	23.5	1.1%
63	Ovan clay, occasionally flooded	590.5	27.2%
70	Seagoville clay, occasionally flooded	54.2	2.5%
72	Silstid loamy fine sand, 1 to 5 percent slopes	0.8	0.0%
78	Trinity clay, occasionally flooded	307.4	14.1%
81	Vertel clay, 3 to 5 percent slopes	3.4	0.2%
83	Wilson clay loam, 0 to 1 percent slopes	33.0	1.5%
84	Wilson clay loam, 1 to 3 percent slopes	1.8	0.1%
W	Water	83.8	3.9%
Totals for Area of Interest		2,173.6	100.0%

Report—Water Features

Water Features—Denton County, Texas											
Map unit symbol and soil name	Hydrologic group	Surface runoff	Month	Water table		Surface depth	Ponding		Flooding		
				Upper limit	Lower limit		Duration	Frequency	Duration	Frequency	
				Ft	Ft	Ft					
3—Altoga silty clay, 5 to 8 percent slopes											
Altoga	B	—	Jan-Dec	—	—	—	—	None	—	—	
4—Altoga silty clay, 5 to 12 percent slopes, eroded											
Altoga, eroded	B	—	Jan-Dec	—	—	—	—	None	—	—	
5—Aquilla loamy fine sand, 2 to 5 percent slopes											
Aquilla	A	—	January	4.0-5.0	4.5-6.0	—	—	None	—	None	
	A	—	February	4.0-5.0	4.5-6.0	—	—	None	—	None	
	A	—	March	4.0-5.0	4.5-6.0	—	—	None	—	None	
	A	—	December	4.0-5.0	4.5-6.0	—	—	None	—	None	
6—Arenis, gently undulating											
Arenis	A	—	January	—	—	—	—	None	Long	Occasional	
	A	—	February	—	—	—	—	None	Long	Occasional	
	A	—	March	—	—	—	—	None	Long	Occasional	
	A	—	April	—	—	—	—	None	Long	Occasional	
	A	—	May	—	—	—	—	None	Long	Occasional	
	A	—	September	—	—	—	—	None	Long	Occasional	
	A	—	October	—	—	—	—	None	Long	Occasional	
	A	—	November	—	—	—	—	None	Long	Occasional	
	A	—	December	—	—	—	—	None	Long	Occasional	

Water Features—Denton County, Texas										
Map unit symbol and soil name	Hydrologic group	Surface runoff	Month	Water table		Surface depth	Ponding		Flooding	
				Upper limit	Lower limit		Duration	Frequency	Duration	Frequency
7—Arentis, hilly				Ft	Ft	Ft				
Arentis	A	—	January	—	—	—	—	—	None	Occasional
	A	—	February	—	—	—	—	—	None	Occasional
	A	—	March	—	—	—	—	—	None	Occasional
	A	—	April	—	—	—	—	—	None	Occasional
	A	—	May	—	—	—	—	—	None	Occasional
	A	—	September	—	—	—	—	—	None	Occasional
	A	—	October	—	—	—	—	—	None	Occasional
	A	—	November	—	—	—	—	—	None	Occasional
	A	—	December	—	—	—	—	—	None	Occasional
9—Bastil fine sandy loam, 1 to 3 percent slopes										
Bastil	B	—	Jan-Dec	—	—	—	—	—	None	—
10—Bastil fine sandy loam, 3 to 5 percent slopes										
Bastil	B	—	Jan-Dec	—	—	—	—	—	None	—
21—Burleson clay, 0 to 1 percent slopes										
Burleson	D	—	Jan-Dec	—	—	—	—	—	None	—
22—Burleson clay, 1 to 3 percent slopes										
Burleson	D	—	Jan-Dec	—	—	—	—	—	None	—
27—Crockett fine sandy loam, 1 to 3 percent slopes										
Crockett	D	—	Jan-Dec	—	—	—	—	—	None	—

Water Features—Denton County, Texas										
Map unit symbol and soil name	Hydrologic group	Surface runoff	Month	Water table		Ponding		Flooding		
				Upper limit	Lower limit	Surface depth	Duration	Frequency	Duration	Frequency
32—Ferris-Heiden clay, 5 to 15 percent slopes				Ft	Ft					
Ferris	D	—	Jan-Dec	—	—	—	—	None	—	—
Heiden	D	—	Jan-Dec	—	—	—	—	None	—	—
33—Frio silty clay, occasionally flooded										
Frio	C	—	January	—	—	—	—	None	Brief	Occasional
	C	—	February	—	—	—	—	None	Brief	Occasional
	C	—	March	—	—	—	—	None	Brief	Occasional
	C	—	April	—	—	—	—	None	Brief	Occasional
	C	—	May	—	—	—	—	None	Brief	Occasional
	C	—	October	—	—	—	—	None	Brief	Occasional
	C	—	November	—	—	—	—	None	Brief	Occasional
	C	—	December	—	—	—	—	None	Brief	Occasional
44—Houston Black clay, 1 to 3 percent slopes										
Houston black	D	—	Jan-Dec	—	—	—	—	None	—	—
53—Lewisville clay loam, 3 to 5 percent slopes										
Lewisville	B	—	Jan-Dec	—	—	—	—	None	—	—
63—Ovan clay, occasionally flooded										
Ovan	D	—	March	—	—	—	—	None	Brief	Occasional
	D	—	April	—	—	—	—	None	Brief	Occasional
	D	—	May	—	—	—	—	None	Brief	Occasional
	D	—	June	—	—	—	—	None	Brief	Occasional

Water Features—Denton County, Texas										
Map unit symbol and soil name	Hydrologic group	Surface runoff	Month	Water table		Ponding		Flooding		
				Upper limit	Lower limit	Surface depth	Duration	Frequency	Duration	Frequency
70—Seagoville clay, occasionally flooded				Ft	Ft					
Seagoville	D	---	January	---	---	---	---	None	Very brief	Occasional
	D	---	February	---	---	---	---	None	Very brief	Occasional
	D	---	March	---	---	---	---	None	Very brief	Occasional
	D	---	April	---	---	---	---	None	Very brief	Occasional
	D	---	May	---	---	---	---	None	Very brief	Occasional
	D	---	June	---	---	---	---	None	Very brief	Occasional
	D	---	October	---	---	---	---	None	Very brief	Occasional
	D	---	November	---	---	---	---	None	Very brief	Occasional
	D	---	December	---	---	---	---	None	Very brief	Occasional
72—Siltstid loamy fine sand, 1 to 5 percent slopes										
Siltstid	A	---	Jan-Dec	---	---	---	---	None	---	---
78—Trinity clay, occasionally flooded										
Trinity	D	---	February	---	---	---	---	None	Brief	Occasional
	D	---	March	---	---	---	---	None	Brief	Occasional
	D	---	April	---	---	---	---	None	Brief	Occasional
	D	---	May	---	---	---	---	None	Brief	Occasional
81—Vertel clay, 3 to 5 percent slopes										
Vertel	D	---	Jan-Dec	---	---	---	---	None	---	---
83—Wilson clay loam, 0 to 1 percent slopes										
Wilson	D	---	Jan-Dec	---	---	---	---	None	---	---

Water Features—Denton County, Texas										
Map unit symbol and soil name	Hydrologic group	Surface runoff	Month	Water table		Ponding		Flooding		
				Upper limit	Lower limit	Surface depth	Duration	Frequency	Duration	Frequency
84—Wilson clay loam, 1 to 3 percent slopes				Ft	Ft	Ft				
Wilson	D	—	Jan-Dec	—	—	—	—	None	—	—
W—Water										
Water	—	—	Jan-Dec	—	—	—	—	None	—	—

Data Source Information

Soil Survey Area: Denton County, Texas
 Survey Area Data: Version 7, Jan 14, 2010

where

- CN_{II_0} = AMC-II curve number for mild slope (unadjusted for slope)
- C_0 = regression constant for a given level of vegetation
- C_1 = regression constant for a given level of vegetation
- C_2 = regression constant for a given level of vegetation
- IR = infiltration correlation parameter for given soil type

The relationship between CN_{II_0} , the vegetative cover and default soil texture is shown graphically in Figure 8. Table 7 gives values of C_0 , C_1 and C_2 for the five types of vegetative cover built into the HELP program.

4.2.3 Adjustment of Curve Number for Surface Slope

A regression equation was developed to adjust the AMC-II curve number for surface slope conditions. The regression was developed based on kinematic wave theory where

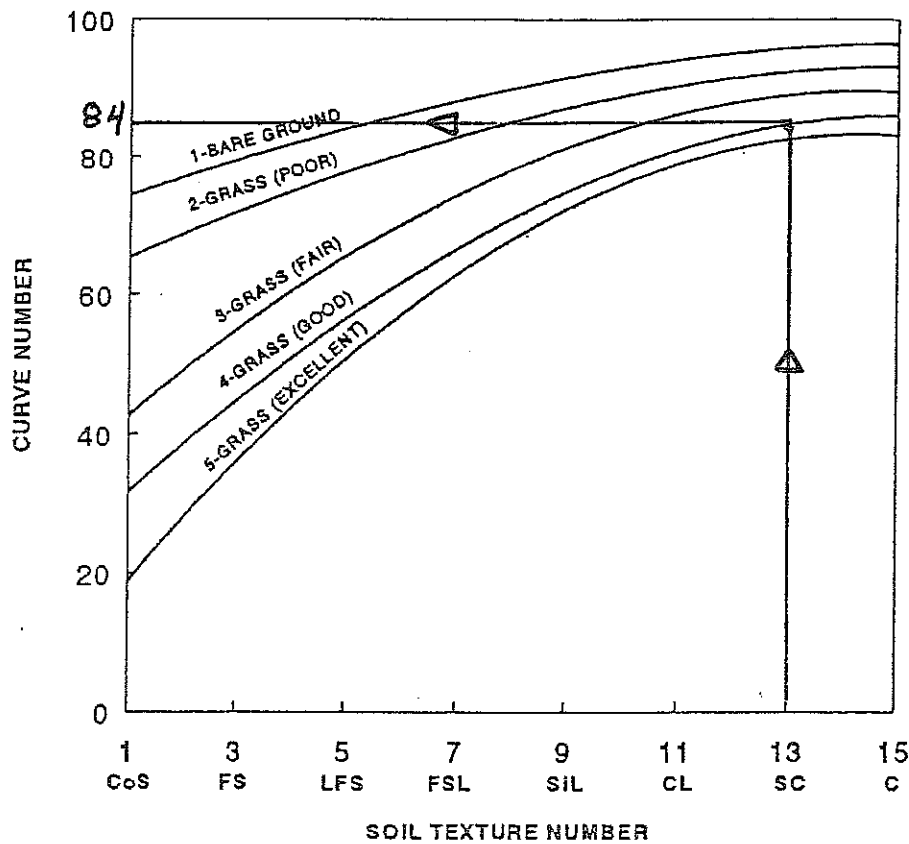


Figure 8. Relation between SCS Curve Number and Default Soil Texture Number for Various Levels of Vegetation

**TABLE 5.3 Values of SCS
Curve Number for Rural Areas**

Source: [McCuen, 1982]

Land Use Description	Hydrologic Soil Group			
	A	B	C	D
Fallow:				
Straight Row	77	86	91	94
Row Crops:				
Straight Row, Poor Condition	72	81	88	91
Straight Row, Good Condition	67	78	85	89
Contoured, Poor Condition	70	79	84	88
Contoured, Good Condition	65	75	82	86
Contoured and Terraced, Poor Condition	66	74	80	82
Contoured and Terraced, Good Condition	62	71	78	81
Small Grain:				
Straight Row, Poor Condition	65	76	84	88
Straight Row, Good Condition	63	75	83	87
Contoured, Poor Condition	63	74	82	85
Contoured, Good Condition	61	73	81	84
Contoured and Terraced, Poor Condition	61	72	79	82
Contoured and Terraced, Good Condition	59	70	78	81
Close-Seeded Legumes or Rotation Meadow				
Straight Row, Poor Condition	66	77	85	89
Straight Row, Good Condition	58	72	81	85
Contoured, Poor Condition	64	75	83	85
Contoured, Good Condition	55	69	78	83
Contoured and Terraced, Poor Condition	63	73	80	83
Contoured and Terraced, Good Condition	51	67	76	80
Pasture or Range:				
Poor Condition	68	79	86	89
Fair Condition	49	69	79	84
Good Condition	39	61	74	80
Contoured, Poor Condition	47	67	81	88
Contoured, Fair Condition	25	59	75	83
Contoured, Good Condition	6	35	70	79
Meadow, Good Condition	30	58	71	78
Woods or Forest Land:				
Poor Condition	45	66	77	83
Fair Condition	36	60	73	79
Good Condition	25	55	70	77
Farmsteads:	59	74	82	86

Initial and Uniform Loss Rate

An initial loss in inches (*STRTL*) and a constant loss rate (*CNSTL*) in inches per hour are specified for this method. All rainfall is lost until the volume of initial loss is satisfied. After the initial loss is satisfied, rainfall is lost at the constant rate.

This section provides guidance in selecting the values used for the initial loss and uniform loss rate in two ways:

1. By consulting previous studies of actual rainfall events for a particular watershed or region.
2. By relating the parameters to the SCS Curve Number, which can be estimated using the information presented earlier in this chapter.

Previous studies by the U.S. Army Corps of Engineers or other public agencies may provide guidance on selecting appropriate values for the initial loss and uniform loss rate for a particular location. Tables 5.4 through 5.6 list the values of initial and

HYDROGRAPH DEVELOPMENT INFORMATION

HYDROGRAPH DEVELOPMENT INFORMATION

Landfill Areas

Direct runoff methods, (i.e., kinematic wave) have been used for the majority of the landfill final cover areas. The kinematic wave method has been used to model the 4 percent topslope areas and 25 percent side slope areas before the flow is intercepted by the drainage swales. The kinematic wave method is a physically based method using slope, surface roughness, catchment lengths and areas. This method does not consider attenuation for flood wave; as a consequence, this method provides for a conservative analysis. The following typical parameters for the kinematic wave method have been developed for landfill areas.

Kinematic wave parameters for overland flow:

- Slope: Varies from 0.04 to 0.25 ft/ft landfill slopes
- N: 0.35 Manning's friction coefficient (based on using a value between dense grass (N = 0.24) and Bermuda grass (N = 0.41) listed in Soil Conservation Services TR-55)
- L: Represents a typical distance between swales for overland flow for each drainage area. For example, as shown on Sheet IIIF-A-24, the swale spacing on 4H:1V sideslopes is 120 feet.

Percentage of drainage area represented by this element is 100 percent.

Kinematic Wave routing for channels:

- Channel length (ft): The length of the channel section.
- Channel slope (ft/ft): Varies from 0.0010 to 0.0574 (0.005 for swales).
- Channel roughness coefficient: 0.03 for grass lined channels and swales.
- Channel type: A trapezoidal channel was used with varying width and 3:1 side slopes ("V" ditch with varying side slopes for swales).

Non-Landfill Final Cover Areas

Hydrographs for the majority of non-landfill final cover areas within and near the permit boundary (e.g., pond areas) were developed using the Snyder unit hydrograph method.

Espey “10-Minute” method has been used to estimate Snyder parameters. Snyder parameter estimations are provided on pages IIF-A-21 through IIF-A-26.

As discussed in Section 2 of Appendix IIF, hydrographs for the areas outside of the permit boundary (O1, O1A, O2, O3, O4, O5, O6, O7, O8, O9, OSB, and OSC), and larger areas inside the permit boundary (S7, S9, and S11) were developed using the Snyder unit hydrograph method. The percent imperviousness ranges from 2 percent to 12 percent, for the majority of the non-landfill no-site and off-site areas, which represents the majority of the watershed as undeveloped. Pond areas are assumed to be 100 percent impervious, and areas with significant channel surface or paved surfaces were assigned higher percentages of impervious area, as shown on IIF-A-22.

Drainage Areas

The drainage areas used for this analysis are shown on Sheets IIF-A-28 and IIF-A-29. The routing scheme for the post-development condition is shown in the HEC-1 output file presented on pages IIF-A-30 through IIF-A-104.

**DISTRIBUTED RUNOFF METHOD
KINEMATIC WAVE EXAMPLE**

Drainage area "A7T" is used in this example (refer to Sheet IIF-A-19 for location of drainage area).

Watershed Specific Parameters:

A = 13.58	acres	Watershed Area (acres)
A = 0.0212	sq-miles	Watershed Area (sq-miles)
CN = 84		SCS Curve Number (see sheet IIF-A-4 for more information)

Kinematic Wave parameter for overland flow:

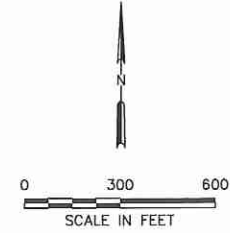
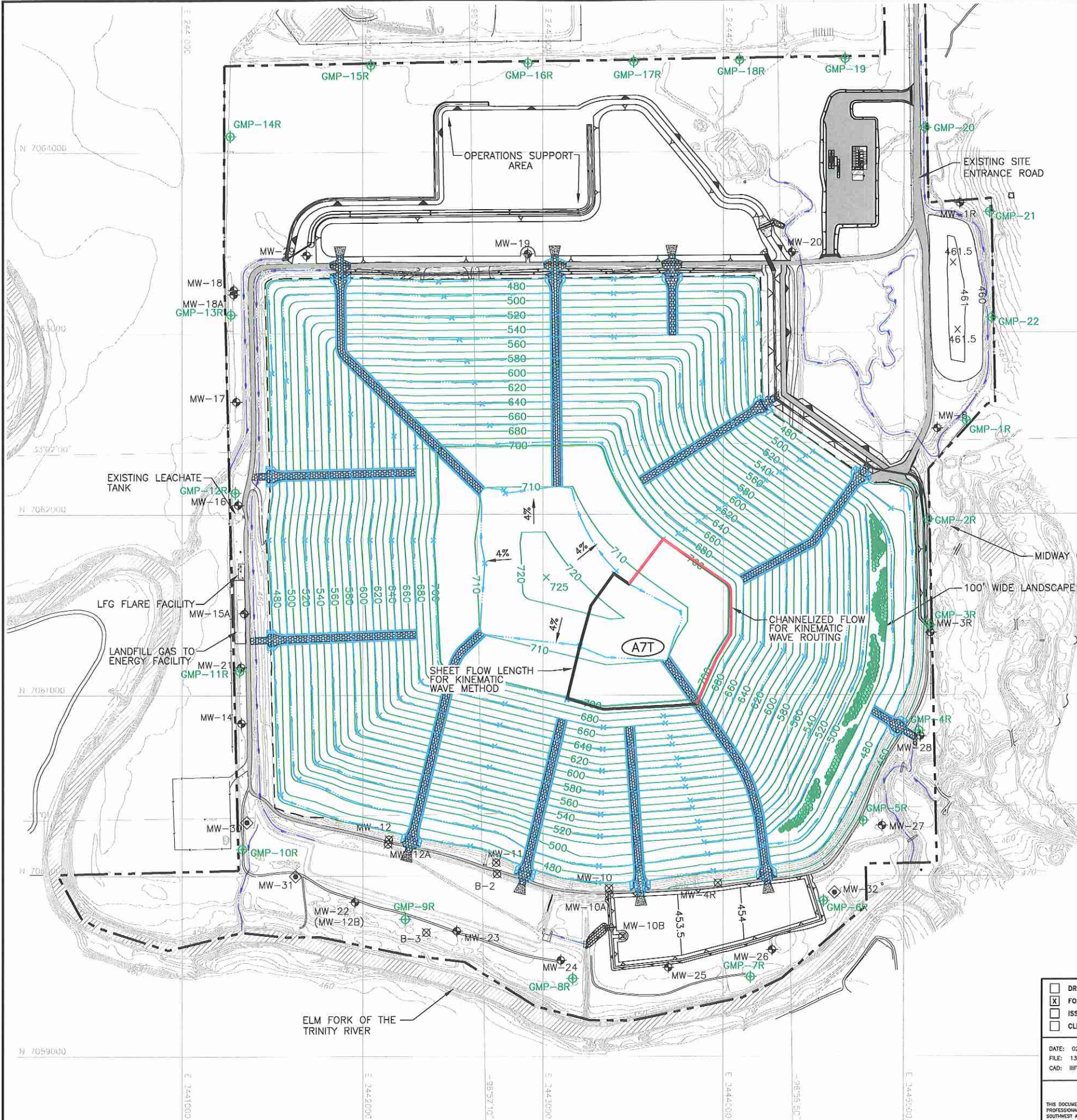
L = 312	ft	Typical overland flow (ft)
S = 0.04	ft/ft	Landfill slope (ft/ft)
N = 0.35		Manning's Coefficient

Percentage of the drainage area represented by this element is 100 percent

Kinematic Wave routing data for the swale:

L = 1133	ft	Typical swale length (ft)
S = 0.005	ft/ft	Swale bottom slope (ft/ft)
N = 0.03		Manning's Coefficient
Channel = TRAP		Swale Type*

* A trapezoidal channel with no bottom width was used to simulate a triangular channel.



- LEGEND**
- PERMIT BOUNDARY
 - - - PROPOSED LIMIT OF WASTE
 - N 7064000 STATE PLANE COORDINATE SYSTEM
 - 33°02'00" GEODETIC COORDINATE SYSTEM
 - 500 EXISTING CONTOUR (SEE NOTE 1)
 - 600 FINAL COVER CONTOUR
 - DRAINAGE LETDOWN
 - DRAINAGE SWALE
 - ⊙ MW-8 EXISTING GROUNDWATER MONITORING WELL
 - ⊙ MW-30 PROPOSED GROUNDWATER MONITORING WELL
 - ⊙ GMP-20 PROPOSED LANDFILL GAS MONITORING PROBE
 - ⊙ MW-12 OBSERVATION WELL
 - DRAINAGE AREA BOUNDARY
 - (A7T) DRAINAGE AREA DESIGNATION

NOTE:

- CONTOURS AND ELEVATIONS PROVIDED BY METROPOLITAN AERIAL SURVEYS COMPILED FROM AERIAL PHOTOGRAPHY FLOWN 8-28-2010. THE GRID SYSTEM IS TIED TO THE TEXAS STATE PLANE COORDINATE SYSTEM NORTH CENTRAL ZONE NAD 1983. ELEVATIONS ARE BASED ON NAVD 1988.
- PERMIT BOUNDARY WAS PREPARED BY PEISER SUREYING CO. IN NOVEMBER 2010.



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REVISIONS		
NO.	DATE	DESCRIPTION

**MAJOR PERMIT AMENDMENT
KINEMATIC WAVE PARAMETERS**

CAMELOT LANDFILL
DENTON COUNTY, TEXAS

Weaver Boos Consultants
TBPE REGISTRATION NO. F-3727

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SHEET IIF-A-20

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ESPEY 10-MINUTE METHOD PARAMETERS

CAMELOT LANDFILL
1339-351-11-02-6B.6
UNIT HYDROGRAPH DATA
PROPOSED EXPANSION CONDITION

Snyder's Hydrograph Coefficients (Espey's 10 Minute Method)

Proposed Expansion Conditions

Area No.	Area (acres)	Max. Flow Length (L) (ft)	S (ft/ft)	I (%)	Manning "n"	Φ^1	T_r^2 (min)	T_{lag}^3 (min)	T_{lag} (hr)	Area ⁴ (sq mi)	q_p^5 (cfs/sq mi)	C_p^6
O1	87.47	3,580	0.0101	23	0.04	0.80	25.7	23.2	0.39	0.1367	1059.5	0.64
O1A	23.42	2,285	0.0132	4	0.04	0.85	32.7	30.2	0.50	0.0366	864.1	0.68
O2	1008.38	14,770	0.0050	18	0.04	0.81	45.3	42.8	0.71	1.5756	524.7	0.58
O3	16.18	835	0.0611	2	0.04	0.86	20.4	17.9	0.30	0.0253	1452.4	0.68
O4	86.04	3,840	0.0180	10	0.04	0.84	28.4	25.9	0.43	0.1344	954.5	0.64
O5	116.47	2,140	0.0121	2	0.04	0.86	38.0	35.5	0.59	0.1820	690.4	0.64
S1	10.26	875	0.0020	2	0.04	0.86	48.5	46.0	0.77	0.0160	585.8	0.70
S2	30.64	2,676	0.0009	2	0.04	0.86	76.6	74.1	1.23	0.0479	344.0	0.66
S3	4.55	250	0.0120	2	0.04	0.86	23.2	20.7	0.35	0.0071	1330.2	0.72
S4	43.34	3,950	0.0058	2	0.04	0.86	52.6	50.1	0.83	0.0677	507.4	0.66
S5	7.34	1,405	0.0085	2	0.04	0.86	37.7	35.2	0.59	0.0115	778.1	0.71
S6	13.92	3,910	0.0063	2	0.04	0.86	51.4	48.9	0.81	0.0218	544.2	0.69
S7	5.39	1,015	0.0148	2	0.04	0.86	30.4	27.9	0.47	0.0084	989.9	0.72
S8	10.12	785	0.0522	2	0.04	0.86	20.9	18.4	0.31	0.0158	1440.6	0.69
S9	22.75	802	0.0279	2	0.04	0.86	24.6	22.1	0.37	0.0355	1173.3	0.68
S10	10.76	282	0.0317	2	0.04	0.86	18.7	16.2	0.27	0.0168	1617.9	0.68

¹ Conveyance efficiency coefficient from Dodson & Associates Inc., *ProHec-1 Program Documentation*, 1995, pages 6-19 and 6-20.

² $T_r = 3.1(\Delta L^{0.23})(S^{0.25})(\Phi^{0.18})(\Phi^{1.57})$

³ $T_{lag} = T_r - \Delta H/2$

⁴ From area summary sheet

⁵ $q_p = 31600(A^{-0.04})(T_r^{-1.07})$

⁶ $C_p = 49.375(A^{-0.04})(T_r^{-1.07})(T_{lag})$

T_r = surface runoff to unit hydrograph peak (min)

L = distance along main channel from study point to watershed boundary (ft)

S = main channel slope (ft/ft)

I = impervious cover within the watershed (%)

T_{lag} = watershed lag time (min)

Δt = computation interval (minutes)

q_p = unit hydrograph peak discharge (cfs/sq mi)

C_p = Snyder's peaking coefficient

Snyder Unit Hydrograph uses lag time (T_{lag}) and peaking coefficient accounting for flood wave and watershed storage conditions.

Drainage area "O1" is used in this example.

Estimated Watershed specific parameters

A =	87.47	acres	watershed area
L =	3580	feet	maximun flow length with this watershed
S =	0.0101	feet/feet	watershed slope
I =	23	percent (%)	watershed imperviousness
n =	0.04		Manning's coefficient

Calculate T_r : time beginning of surface runoff to the unit hydrograph peak in minutes

$$T_r = 3.1(L^{0.23})(S^{-0.25})(I^{-0.18})(\Phi^{1.57})$$

Estimate : conveyance efficiency coefficient

See figure 6.12 on page IIIF-A-19 for estimating

Φ = for 6 percent impervious cover and $n = 0.04$

$$\Phi = 0.80$$

$$T_r = 3.1(3580^{0.23})(.0101^{-0.25})(23^{-0.18})(0.8^{1.57})$$

$$T_r = 25.7 \quad \text{min}$$

Calculate T_{lag} : watershed lag time

$$T_{lag} = T_r - (\Delta t/2)$$

$$T_{lag} = 23.2 \quad \text{minutes}$$

$$T_{lag} = 0.39 \quad \text{hours}$$

Δt is calculation interval, and 5 minutes is used
in the HEC - 1 modeling in this project

$$A = A/640$$

$$A = 0.1367 \quad \text{square miles}$$

Calculate q_p : peak discharge of unit hydrograph per unit area (cfs/sq. mi).

$$q_p = 31600(A^{-0.04})(T_r^{-1.07})$$

$$q_p = 31600(0.1367^{-0.04})(25.7^{-1.07})$$

$$q_p = 1059.5 \quad \text{cfs/sq. mi}$$

Calculate Peaking coefficient C_p :

$$C_p = 49.375(A^{-0.04})(T_r^{-1.07})(T_{lag})$$

$$C_p = 49.375(0.1367^{-0.04})(25.7^{-1.07})(0.39)$$

$$C_p = 0.64$$

compute the value of Snyder's peaking coefficient C_p for use in HEC-1 analyses. First, the watershed lag time T_L is determined by subtracting one-half of the computation interval from the time to rise ($T_L = T_r - \Delta t/2$). Then, C_p may be computed by substituting the known values of T_L and q_p into Snyder's equation for peak unit hydrograph flow rate and solving for C_p .

$$C_p = \frac{q_p \times T_L}{640} \quad 6.30$$

In another study, Espey [1977] derived the following equation for computing the time from the beginning of surface runoff to the unit hydrograph peak:

$$T_r = 3.10 L^{0.23} S^{-0.25} I^{-0.18} \Phi^{1.57}$$

Espey "10-Minute" Method for Estimating Snyder Parameters

6.31

in which:

T_r = time from beginning of surface runoff to unit hydrograph peak (minutes)

L = total distance along main channel from study point to watershed boundary (feet)

S = main channel slope between the reference point and a point 0.2L downstream from the upstream watershed boundary (feet per foot)

I = impervious cover within the watershed (percent)

Φ = description of conveyance efficiency of the watershed drainage system.

The conveyance efficiency coefficient Φ is determined using the relationships illustrated on Figure 6.12.

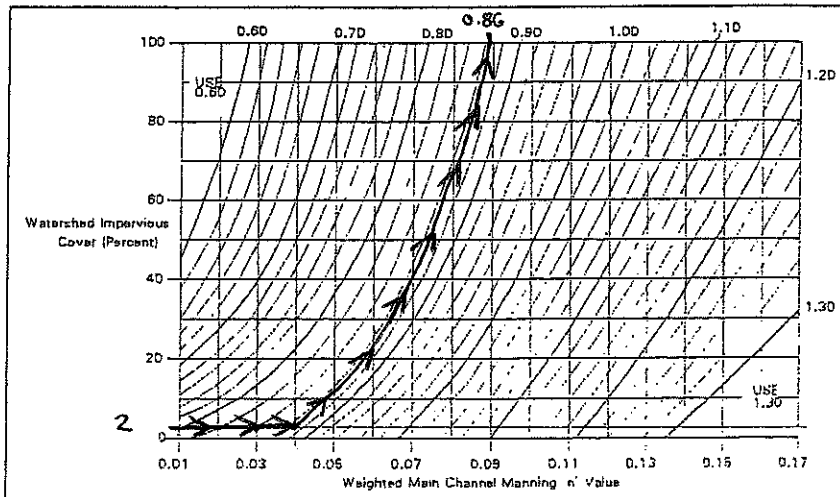


FIGURE 6.12 Determination of Conveyance Efficiency Coefficient Φ

This equation was derived from records for 41 watersheds in Texas, Tennessee, Mississippi, Pennsylvania, North Carolina, Colorado, Kentucky, and Indiana. The range in the watershed characteristics used to develop the equations for urban areas were:

Area : From 0.0128 square miles to 15.00 square miles

L : From 555 feet to 35,600 feet

S : From 0.0005 ft. per ft. to 0.0295 ft. per ft.

I : From 2% to 100%

Φ : From 0.60 to 1.30

Again, note that the time to rise T_r is not the same as the watershed lag time T_L . The difference between the two is that T_r is defined as the time from the beginning of effective rainfall to the peak of the unit hydrograph, while T_L is the time from the centroid of the effective rainfall to the peak of the unit hydrograph. For the purposes of HEC-1 analyses, however, T_L may be determined simply by subtracting one-half the computation time interval from the computed value of T_r ($T_r - \Delta t/2$).

The relationship developed by Espey to compute the peak flow rate of the unit hydrograph is as follows:

$$6.32 \quad Q_u = 31600 A^{0.96} T_r^{-1.07}$$

in which:

Q_u = unit hydrograph peak discharge (cfs)

A = drainage area (square miles)

T_r = time of rise from beginning of surface runoff to unit hydrograph peak (minutes)

Riverside County Method for Estimating Snyder Parameters

Three watershed lag equations have been derived for use in rural areas of Riverside County, California by the Riverside County Flood Control and Water Conservation District [Anonymous, 1963]. These equations differ slightly from those developed at the Tulsa District of the U.S. Army Corps of Engineers in that lag is defined as the time from the beginning of rainfall to the point on the unit hydrograph corresponding to one-half of the total runoff volume.

Each equation is applicable to a different topographic region:

$$6.33 \quad T_L = 120 \left(\frac{L \times L_{cc}}{\sqrt{S}} \right)^{0.38} \quad (\text{Mountain Areas})$$

$$6.34 \quad T_L = 0.72 \left(\frac{L \times L_{cc}}{\sqrt{S}} \right)^{0.38} \quad (\text{Foothill Areas})$$

$$6.35 \quad T_L = 0.58 \left(\frac{L \times L_{cc}}{\sqrt{S}} \right)^{0.38} \quad (\text{Valley Areas})$$

in which:

T_L = watershed lag in hours

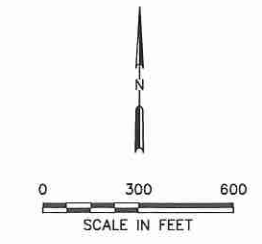
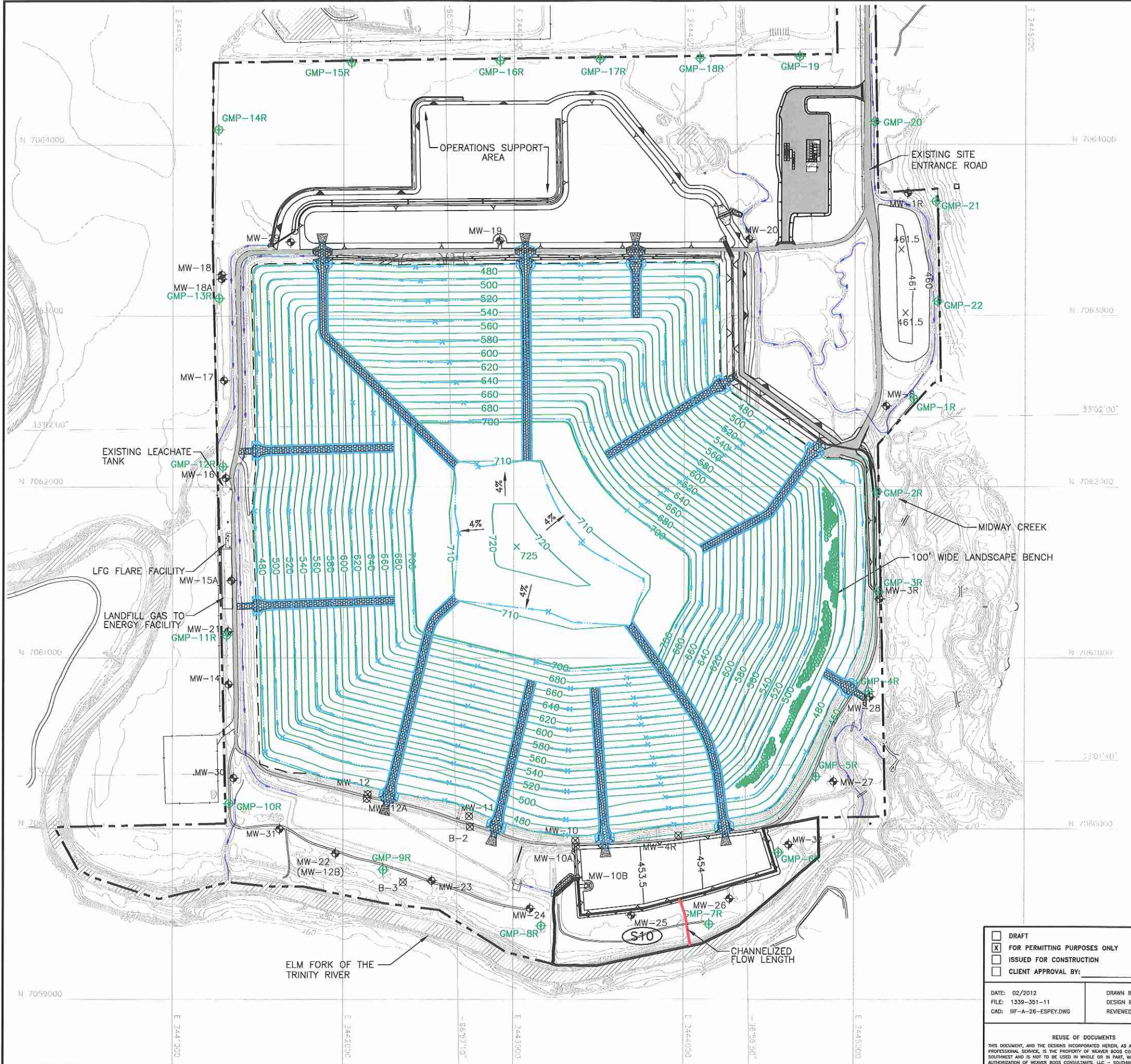
L = watershed length in miles

L_{cc} = length to centroid in miles

S = watershed slope in feet per mile.

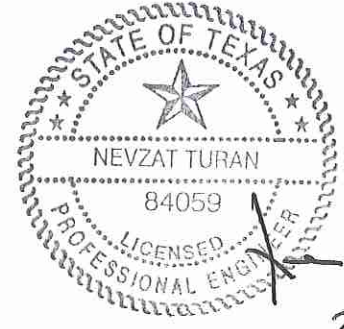
The sizes of the watersheds studied in developing these equations ranged from 2.3 square miles to 645 square miles.

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- LEGEND**
- PERMIT BOUNDARY
 - PROPOSED LIMIT OF WASTE
 - N 7064000 STATE PLANE COORDINATE SYSTEM
 - 1:202'00" GEODETIC COORDINATE SYSTEM
 - 500 EXISTING CONTOUR (SEE NOTE 1)
 - 600 FINAL COVER CONTOUR
 - DRAINAGE LETDOWN
 - DRAINAGE SWALE
 - ⊕ MW-8 PERMITTED GROUNDWATER MONITORING WELL
 - ⊗ MW-12 PERMITTED GROUNDWATER OBSERVATION WELL
 - ⊕ GMP-14R PROPOSED GAS MONITORING PROBE
 - DRAINAGE AREA BOUNDARY
 - (S10) DRAINAGE AREA DESIGNATION

- NOTE:**
1. CONTOURS AND ELEVATIONS PROVIDED BY METROPOLITAN AERIAL SURVEYS COMPILED FROM AERIAL PHOTOGRAPHY FLOWN 8-28-2010. THE GRID SYSTEM IS TIED TO THE TEXAS STATE PLANE COORDINATE SYSTEM NORTH CENTRAL ZONE NAD 1983. ELEVATIONS ARE BASED ON NAVD 1988.
 2. PERMIT BOUNDARY WAS PREPARED BY PEISER SUREYING CO. IN NOVEMBER 2010.



2-28-12

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PREPARED FOR		CITY OF FARMERS BRANCH
REVISIONS		
NO.	DATE	DESCRIPTION

MAJOR PERMIT AMENDMENT
ESPEY "10-MINUTE" METHOD
PARAMETERS
 CAMELOT LANDFILL
 DENTON COUNTY, TEXAS

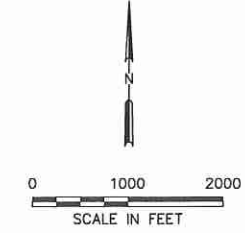
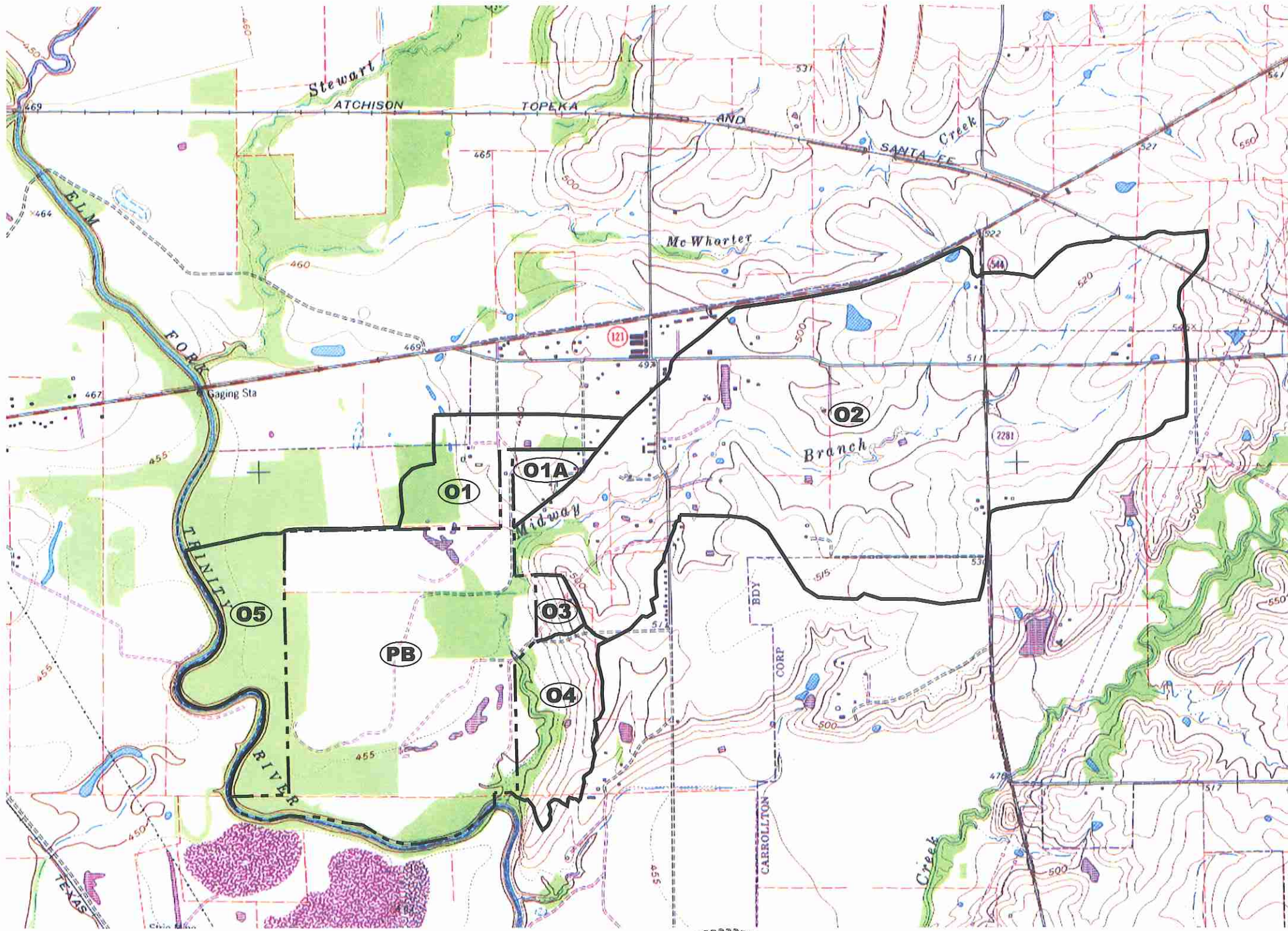
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SHEET IIIF-A-26

**POST-DEVELOPMENT HEC-1 ANALYSIS
DRAINAGE AREAS**

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LEGEND

--- PERMIT BOUNDARY

— DRAINAGE AREA BOUNDARY

○02○ DRAINAGE AREA LABEL

DRAINAGE AREA NO.	AREA (ACRES)
O1	87.5
O1A	23.4
O2	1,008.4
O3	16.2
O4	86.0
O5	116.5
PB	462.6
TOTAL	1,807.6

ROAD CLASSIFICATION

Heavy-duty ——— Light-duty ———

Medium-duty ——— Unimproved dirt ———

○ Interstate Route ○ U.S. Route ○ State Route

LEWISVILLE EAST, TEX.
 SW/4 FRISCO 15' QUADRANGLE
 N3300-W9652.5/7.5
 1960
 PHOTOREVISED 1968
 AMS 6650 111 SW-SERIES V882

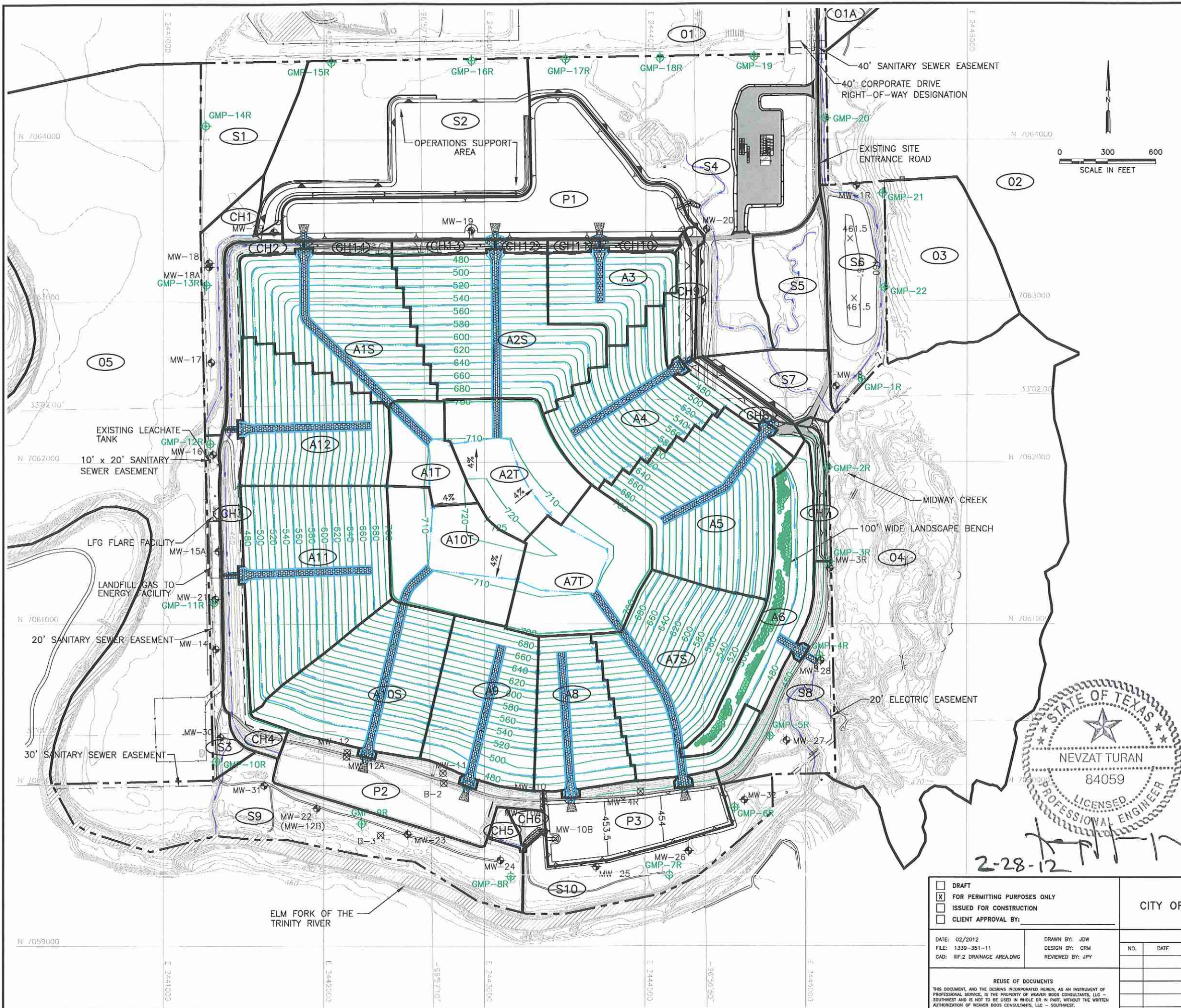
- NOTES:**
1. DRAINAGE AREA DELINEATION WITHIN THE PERMIT BOUNDARY IS INCLUDED ON SHEET IIF-A-29.
 2. TOPOGRAPHY REPRODUCED FROM USGS 7.5 MINUTE QUADRANGLE TOPOGRAPHIC MAP (LEWISVILLE EAST, TX, PHOTO REVISED 1981).

NEVZAT TURAN
 84059
 LICENSED PROFESSIONAL ENGINEER
 2-28-12

<input type="checkbox"/> DRAFT	PREPARED FOR
<input checked="" type="checkbox"/> FOR PERMITTING PURPOSES ONLY	CITY OF FARMERS BRANCH
<input type="checkbox"/> ISSUED FOR CONSTRUCTION	
<input type="checkbox"/> CLIENT APPROVAL BY:	
DATE: 02/2012	DRAWN BY: SRF
FILE: 1339-351-11	DESIGN BY: CRM
CAD: IIF-A-28-DRAINAGE.DWG	REVIEWED BY: JPY
REUSE OF DOCUMENTS	
THIS DOCUMENT, AND THE DESIGNS INCORPORATED HEREIN, AS AN INSTRUMENT OF PROFESSIONAL SERVICE, IS THE PROPERTY OF WEAVER BOOS CONSULTANTS, LLC - SOUTHWEST AND IS NOT TO BE USED IN WHOLE OR IN PART, WITHOUT THE WRITTEN AUTHORIZATION OF WEAVER BOOS CONSULTANTS, LLC - SOUTHWEST.	

REVISIONS		
NO.	DATE	DESCRIPTION

**MAJOR PERMIT AMENDMENT
 OFFSITE DRAINAGE AREA MAP**
 CAMELOT LANDFILL
 DENTON COUNTY, TEXAS
Weaver Boos Consultants
 TBPE REGISTRATION NO. F-3727
 CHICAGO, IL FORT WORTH, TX GRIFFITH, IN
 NAPERVILLE, IL COLUMBUS, OH SOUTH BEND, IN
 DENVER, CO (817) 735-9770 SPRINGFIELD, IL
 ST. LOUIS, MO

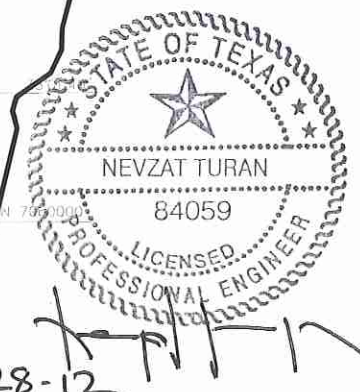


LEGEND

- PERMIT BOUNDARY
- PROPOSED LIMIT OF WASTE
- N 7064000 STATE PLANE COORDINATE SYSTEM
- 33°02'00" GEODETIC COORDINATE SYSTEM
- 500 EXISTING CONTOUR (SEE NOTE 1)
- 600 FINAL COVER CONTOUR
- DRAINAGE LETDOWN
- DRAINAGE SWALE
- EASEMENT BOUNDARY
- MW-8 PERMITTED GROUNDWATER MONITORING WELL
- MW-12 PERMITTED GROUNDWATER OBSERVATION WELL
- GMP-14R PROPOSED GAS MONITORING PROBE
- DRAINAGE AREA BOUNDARY
- (A7T) DRAINAGE AREA DESIGNATION

- NOTE:**
- CONTOURS AND ELEVATIONS PROVIDED BY METROPOLITAN AERIAL SURVEYS COMPILED FROM AERIAL PHOTOGRAPHY FLOWN 8-28-2010. THE GRID SYSTEM IS TIED TO THE TEXAS STATE PLANE COORDINATE SYSTEM NORTH CENTRAL ZONE NAD 1983. ELEVATIONS ARE BASED ON NAVD 1988.
 - PERMIT BOUNDARY WAS PREPARED BY PEISER SUREYING CO. IN NOVEMBER 2010.
 - MAXIMUM FINAL COVER ELEVATION IS 725 FT-MSL. MAXIMUM TOP OF WASTE ELEVATION IS 721.5 FT-MSL.
 - REFER TO DRAWING IIIIF-A-28 FOR COMPLETE OFFSITE DRAINAGE AREA DELINEATIONS.

DRAINAGE AREA NO.	AREA (ACRES)	DRAINAGE AREA NO.	AREA (ACRES)
S1	10.26	A10T	12.37
S2	30.86	A10S	16.60
S3	4.55	A11	22.08
S4	43.34	A12	15.17
S5	7.34	CH1	5.94
S6	13.92	CH2	3.29
S7	5.39	CH3	2.71
S8	10.12	CH4	4.45
S9	22.75	CH5	0.76
S10	10.76	CH6	0.83
A1T	5.47	CH7	2.33
A1S	18.48	CH8	3.37
A2T	11.83	CH9	3.09
A2S	20.59	CH10	0.85
A3	8.07	CH11	0.56
A4	13.51	CH12	0.59
A5	19.01	CH13	1.29
A6	11.00	CH14	1.02
A7T	13.58	P1	23.10
A7S	20.36	P2	12.55
A8	10.75	P3	10.74
A9	13.99		



<input type="checkbox"/> DRAFT <input checked="" type="checkbox"/> FOR PERMITTING PURPOSES ONLY <input type="checkbox"/> ISSUED FOR CONSTRUCTION <input type="checkbox"/> CLIENT APPROVAL BY:	PREPARED FOR CITY OF FARMERS BRANCH	MAJOR PERMIT AMENDMENT POST DEVELOPMENT DRAINAGE CAMELOT LANDFILL DENTON COUNTY, TEXAS
DATE: 02/2012 FILE: 1339-351-11 CAD: IIIIF-2 DRAINAGE AREA.DWG	DRAWN BY: JDW DESIGN BY: CRM REVIEWED BY: JPY	
REUSE OF DOCUMENTS <small>THIS DOCUMENT, AND THE DESIGNS INCORPORATED HEREIN, AS AN INSTRUMENT OF PROFESSIONAL SERVICE, IS THE PROPERTY OF WEAVER BOOS CONSULTANTS, LLC. SOUTHWEST AND IS NOT TO BE USED IN WHOLE OR IN PART, WITHOUT THE WRITTEN AUTHORIZATION OF WEAVER BOOS CONSULTANTS, LLC - SOUTHWEST.</small>		CHICAGO, IL FORT WORTH, TX GRIFFITH, IN NAPERVILLE, IL COLUMBUS, OH SOUTH BEND, IN DENVER, CO ST. LOUIS, MO
		SHEET IIIIF-A-29

O:\1339\351\EXPANSION 2009\PART III-SUB\IIIIF-A-29-DRAINAGE AREAS.dwg, jwilson, 1:2

**HEC-1 OUTPUT – POST-DEVELOPMENT
25-YEAR, 24-HOUR STORM EVENT**

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 13MAY11 TIME 13:24:13
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DIAGRAM
1 ID CAMELOT LANDFILL
2 ID PROPOSED EXPANSION CONDITION
3 ID 25-YEAR, 24-HOUR STORM EVENT
4 ID FILE:\SOLID WASTE\CITY OF FARMERS BRANCH\EXPANSION\
5 ID PARTIII-SDP\APPENDIX IIIF\IIIF\HEC-1\PROP25.IH1
6 IT 5 0 2400 720 0 0
7 IO 3 0 0
*
8 KK O1
9 KM OFFSITE AREA O1
10 KO 0 0 0 7 21
11 BA .1367
12 PH 4 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44
13 LS 87
14 US .39 .64
*
15 KK S4
16 KM SUBAREA S4
17 KO 0 0 0 7 21
18 BA .0677
19 LS 0 84
20 US .83 .66
*
21 KK CS4
22 KM COMBINE AREAS PRIOR TO POND P1 OUTLET
23 KO 0 0 0 7 21
24 HC 2
*
25 KK A1T
26 KM SUBAREA A1T
27 KO 0 0 0 7 21
28 BA .0085
29 LS 0 84
30 UK 265 .04 .35 100
31 RD 507 .005 .03 TRAP 0 2 NO
*
32 KK A1S
33 KM SUBAREA A1S
34 KO 0 0 0 7 21
35 BA .0289
36 LS 0 86
37 UK 120 .25 .35 100
38 RD 881 .005 .03 TRAP 0 2 NO
*

```

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
39 KK CA1
40 KM COMBINE A1 SUBAREAS
41 KO 0 0 0 7 21
42 HC 2

```

```

*
43 KK CH14
44 KM SUBAREA CH14
45 KO 0 0 0 7 21
46 BA .0016
47 LS 0 84
48 UK 52 .1 .35 100
49 RD 524 .005 .03 TRAP 0 3 NO
*
50 KK CCH14
51 KM COMBINE CH14 WITH A1 AREAS
52 KO 0 0 0 7 21
53 HC 2
*
54 KK A2T
55 KM SUBAREA A27
56 KO 0 0 0 7 21
57 BA .0185
58 LS 0 84
59 UK 312 .04 .35 100
60 RD 879 .005 .03 TRAP 0 2 NO
*
61 KK A2S
62 KM SUBAREA A2S
63 KO 0 0 0 7 21
64 BA .0322
65 LS 0 86
66 UK 120 .25 .35 100
67 RD 925 .005 .03 TRAP 0 2 NO
*
68 KK CA2
69 KM COMBINE A2 SUBAREAS
70 KO 0 0 0 7 21
71 HC 2
*
72 KK CH12
73 KM SUBAREA CH12
74 KO 0 0 0 7 21
75 BA .0009
76 LS 0 84
77 UK 52 .1 .35 100
78 RD 313 .005 .03 TRAP 0 3 NO
*
79 KK CH13
80 KM SUBAREA CH13
81 KO 0 0 0 7 21
82 BA .0020
83 LS 0 84
84 UK 52 .1 .35 100
85 RD 634 .005 .03 TRAP 0 3 NO
*
86 KK CCH13
87 KM COMBINE CH12 AND CH13 WITH A2 AREAS
88 KO 0 0 0 7 21
89 HC 3
*
90 KK A3
91 KM SUBAREA A3
92 KO 0 0 0 7 21
93 BA .0126
94 LS 0 86
95 UK 120 .25 .35 100
96 RD 630 .005 .03 TRAP 0 2 NO
*
97 KK CH10
98 KM SUBAREA CH10
99 KO 0 0 0 7 21
100 BA .0013
101 LS 0 84
102 UK 52 .1 .35 100
103 RD 483 .005 .03 TRAP 0 3 NO
*
104 KK CH11
105 KM SUBAREA CH11
106 KO 0 0 0 7 21
107 BA .0009
108 LS 0 84
109 UK 52 .1 .35 100
110 RD 313 .005 .03 TRAP 0 3 NO
*
111 KK CCH11

```

1

HEC-1 INPUT

PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

112 KM COMBINE CH10 AND CH11 WITH AREA A3
 113 KO 0 0 0 7 21
 114 HC 3
 *
 115 KK CA3
 116 KM COMBINE AREAS FLOWING DIRECTLY INTO P1
 117 KO 0 0 0 7 21
 118 HC 3
 *

1

HEC-1 INPUT

PAGE 4

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

119 KK CH7
 120 KM CHANNEL CH7
 121 KO 0 0 0 7 21
 122 BA .0036
 123 LS 0 84
 124 UK 82 .25 .35 100
 125 RD 830 .003 .03 TRAP 5 2 NO
 *

126 KK A5
 127 KM SUBAREA A5
 128 KO 0 0 0 7 21
 129 BA .0297
 130 LS 0 86
 131 UK 120 .25 .35 100
 132 RD 1007 .005 .03 TRAP 0 2 NO
 *

133 KK CA5
 134 KM COMBINE CH7 AND A5 BEFORE ROUTING THROUGH CH8
 135 KO 0 0 0 7 21
 136 HC 2
 *

137 KK CH8
 138 KM CHANNEL CH8
 139 KO 0 0 0 7 21
 140 BA .0053
 141 LS 0 84
 142 UK 46 .0652 .35 100
 143 RD 707 .03 .03 TRAP 5 2 YES
 *

144 KK A4
 145 KM SUBAREA A4
 146 KO 0 0 0 7 21
 147 BA .0211
 148 LS 0 86
 149 UK 120 .25 .35 100
 150 RD 403 .005 .03 TRAP 0 2 NO
 *

151 KK CA4
 152 KM COMBINE WITH A4 BEFORE ROUTING THROUGH CH9
 153 KO 0 0 0 7 21
 154 HC 2
 *

155 KK CH9
 156 KM CHANNEL CH9
 157 KO 0 0 0 7 21
 158 BA .0048
 159 LS 0 84
 160 UK 75 .1 .35 100

1

HEC-1 INPUT

PAGE 5

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

161 RD 670 .03 .03 TRAP 5 2 YES
 *

162 KK P1
 163 KM DETENTION POND P1
 164 KO 0 0 0 7 21
 165 BA .0361
 166 LS 0 100
 167 UD 0
 *

168 KK P1-IN
 169 KM COMBINE AREAS DISCHARGING TO POND P1
 170 KO 0 0 0 7 21
 171 HC 3
 *

172 KK RP1
 173 KM ROUTE THROUGH POND P1
 174 KO 0 0 0 7 21
 175 RS 1 ELEV 454.5
 176 SA 0 17.7532 18.1645 18.5771 18.9910 19.4062 19.8227 20.2405
 177 SE 454.5 455 456 457 458 459 460 461
 178 SS 458 25 2.6 1.5

179	SL	455.5	3.1416	.8	.5				
	*								
180	KK	CP1							
181	KM	COMBINE DOWNSTREAM OF POND P1	OUTLET						
182	KO	0	0	0	7	21			
183	HC	2							
	*								
184	KK	S5							
185	KM	SUBAREA S5							
186	KO	0	0	0	7	21			
187	BA	.0115							
188	LS	0	84						
189	US	.59	.71						
	*								
190	KK	CS5							
191	KM	COMBINE AREAS UPSTREAM OF S7							
192	KO	0	0	0	7	21			
193	HC	2							
	*								
194	KK	S7							
195	KM	SUBAREA S7							
196	KO	0	0	0	7	21			
197	BA	.0084							
198	LS	0	84						
199	US	.47	.72						
	*								

1

HEC-1 INPUT

PAGE 6

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

200	KK	CS7							
201	KM	COMBINE WITH AREA S7							
202	KO	0	0	0	7	21			
203	HC	2							
	*								
204	KK	O1A							
205	KM	OFFSITE AREA O1A							
206	KO	0	0	0	7	21			
207	BA	.0366							
208	LS	0	85						
209	US	.5	.68						
	*								
210	KK	O2							
211	KM	OFFSITE AREA O2							
212	KO	0	0	0	7	21			
213	BA	1.5756							
214	LS	0	85						
215	US	.71	.58						
	*								
216	KK	O3							
217	KM	OFFSITE AREA O3							
218	KO	0	0	0	7	21			
219	BA	.0253							
220	LS	0	84						
221	US	.30	.68						
	*								
222	KK	S6							
223	KM	SUBAREA S6							
224	KO	0	0	0	7	21			
225	BA	.0218							
226	LS	0	84						
227	US	.81	.69						
	*								
228	KK	CS6							
229	KM	COMBINE AREAS DISCHARGING OFF OF P.B.							
230	KO	0	0	0	7	21			
231	HC	5							
	*								
232	KK	O4							
233	KM	OFFSITE AREA O4							
234	KO	0	0	0	7	21			
235	BA	.1344							
236	LS	0	84						
237	US	.43	.64						
	*								

1

HEC-1 INPUT

PAGE 7

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

238	KK	CO4							
239	KM	MIDWAY BRANCH DISCHARGING BACK ONTO P.B.							
240	KO	0	0	0	7	21			
241	HC	2							
	*								

242 KK A6
 243 KM SUBAREA A6
 244 KO 0 0 0 7 21
 245 BA .0172
 246 LS 0 86
 247 UK 120 .25 .35 100
 248 RD 1314 .002 .03 TRAP 0 2 NO
 *

249 KK S8
 250 KM SUBAREA S8
 251 KO 0 0 0 7 21
 252 BA .0158
 253 LS 0 84
 254 US .31 .69
 *

255 KK CS8
 256 KM MIDWAY BRANCH DISCHARGING OFF OF P.B.
 257 KO 0 0 0 7 21
 258 HC 3
 *

259 KK S1
 260 KM SUBAREA S1
 261 KO 0 0 0 7 21
 262 BA .0160
 263 LS 0 84
 264 US .77 .70
 *

265 KK S2
 266 KM SUBAREA S2
 267 KO 0 0 0 7 21
 268 BA .0479
 269 LS 0 84
 270 US 1.23 .66
 *

271 KK CH1
 272 KM CHANNEL CH1
 273 KO 0 0 0 7 21
 274 BA .0093
 275 LS 0 84
 276 UK 411 .005 .35 100
 277 RD 1283 .0016 .03 TRAP 15 4 YES
 *

1

HEC-1 INPUT

PAGE 8

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

278 KK S3
 279 KM SUBAREA S3
 280 KO 0 0 0 7 21
 281 BA .0071
 282 LS 0 84
 283 US .35 .72
 *

284 KK O5
 285 KM OFFSITE AREA O5
 286 KO 0 0 0 7 21
 287 BA .1820
 288 LS 0 84
 289 US .59 .64
 *

290 KK C05
 291 KM COMBINE WEST AREAS DISCHARGING TO ELM FORK
 292 KO 0 0 0 7 21
 293 HC 4
 *

294 KK CH2
 295 KM CHANNEL CH2
 296 KO 0 0 0 7 21
 297 BA .0051
 298 LS 0 84
 299 UK 82 .0122 .35 100
 300 RD 1539 .0016 .03 TRAP 8 2 NO
 *

301 KK A12
 302 KM SUBAREA A12
 303 KO 0 0 0 7 21
 304 BA .0237
 305 LS 0 86
 306 UK 120 .25 .35 100
 307 RD 559 .005 .03 TRAP 0 2 NO
 *

308 KK CR12
 309 KM COMBINE CH2 AND A12
 310 KO 0 0 0 7 21
 311 HC 2
 *

312	KK	CH3																	
313	KM	CHANNEL CH3																	
314	KO	0	0	0	7	21													
315	BA	.0042																	
316	LS	0	84																
317	UK	92	.0435	.35	100														
318	RD	840	.0012	.03			TRAP	10	2	YES									
	*																		

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

319	KK	A11																	
320	KM	SUBAREA A11																	
321	KO	0	0	0	7	21													
322	BA	.0345																	
323	LS	0	86																
324	UK	120	.25	.35	100														
325	RD	842	.005	.03			TRAP	0	2	NO									
	*																		

326	KK	CA11																	
327	KM	COMBINE WITH CH3 AND A11																	
328	KO	0	0	0	7	21													
329	HC	2																	
	*																		

330	KK	CH4																	
331	KM	CHANNEL CH4																	
332	KO	0	0	0	7	21													
333	BA	.0070																	
334	LS	0	84																
335	UK	101	.0792	.35	100														
336	RD	1180	.0025	.03			TRAP	10	2	YES									
	*																		

337	KK	A10T																	
338	KM	SUBAREA A10T																	
339	KO	0	0	0	7	21													
340	BA	.0193																	
341	LS	0	84																
342	UK	265	.04	.35	100														
343	RD	772	.005	.03			TRAP	0	2	NO									
	*																		

344	KK	A10S																	
345	KM	SUBAREA A10S																	
346	KO	0	0	0	7	21													
347	BA	.0259																	
348	LS	0	86																
349	UK	120	.25	.35	100														
350	RD	764	.005	.03			TRAP	0	2	NO									
	*																		

351	KK	CA10																	
352	KM	COMBINE A10 SUBAREAS																	
353	KO	0	0	0	7	21													
354	HC	2																	
	*																		

355	KK	A9																	
356	KM	SUBAREA A9																	
357	KO	0	0	0	7	21													
358	BA	.0219																	
359	LS	0	86																
360	UK	120	.25	.35	100														
	*																		

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

361	RD	399	.005	.03			TRAP	0	2	NO										
	*																			

362	KK	P2																	
363	KM	DETENTION POND P2																	
364	KO	0	0	0	7	21													
365	BA	.0196																	
366	LS		100																
367	UD	0																	
	*																		

368	KK	P2-IN																	
369	KM	COMBINE AREAS DISCHARGING TO POND P2																	
370	KO	0	0	0	7	21													
371	HC	4																	
	*																		

372	KK	RP2																	
373	KM	ROUTE THROUGH POND P2																	
374	KO	0	0	0	7	21													
375	RS	1	ELEV	454															
376	SA	0	4.4466	6.7860	8.2567	8.3782	8.5005	8.6236	8.8721	9.1240									
377	SE	454	454.5	455	455.5	456	456.5	457	458	459									
378	SS	458	25	2.6	1.5														
379	SL	456	14.137	.8	.5														

```

*
380 KK CH5
381 KM CHANNEL CH5
382 KO 0 0 7 21
383 BA .0012
384 LS 0 84
385 UK 197 .0051 .35 100
386 RD 155 .005 .03 TRAP 20 2 YES
*
387 KK A7T
388 KM SUBAREA A7T
389 KO 0 0 7 21
390 BA .0212
391 LS 0 84
392 UK 312 .04 .35 100
393 RD 1133 .005 .03 TRAP 0 2 NO
*
394 KK A7S
395 KM SUBAREA A7S
396 KO 0 0 7 21
397 BA .0318
398 LS 0 86
399 UK 120 .25 .35 100
400 RD 1094 .005 .03 TRAP 0 2 NO
*

```

1

HEC-1 INPUT

PAGE 11

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

401 KK CA7
402 KM COMBINE A7 SUBAREAS
403 KO 0 0 7 21
404 HC 2
*
405 KK A8
406 KM SUBAREA A8
407 KO 0 0 7 21
408 BA .0168
409 LS 0 86
410 UK 120 .25 .35 100
411 RD 399 .005 .03 TRAP 0 2 NO
*
412 KK P3
413 KM DETENTION POND P3
414 KO 0 0 7 21
415 BA .0168
416 LS 100
417 UD 0
*
418 KK P3-IN
419 KM COMBINE AREAS DISCHARGING TO POND P3
420 KO 0 0 7 21
421 HC 3
*
422 KK RP3
423 KM ROUTE THROUGH POND P3
424 KO 0 0 7 21
425 RS 1 ELEV 453
426 SA 0 5.356 7.771 7.965 8.160 8.357 8.555
427 SE 453 454 455 456 457 458 459
428 SS 458 25 2.6 1.5
429 SL 454.5 7.069 .8 .5
*
430 KK CH6
431 KM CHANNEL CH6
432 KO 0 0 7 21
433 BA .0013
434 LS 0 84
435 UK 50 .1 .35 100
436 RD 155 .005 .03 TRAP 20 2 YES
*
437 KK CCH6
438 KM COMBINE AREAS UPSTREAM OF S8
439 KO 0 0 7 21
440 HC 2
*

```

1

HEC-1 INPUT

PAGE 12

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

441 KK S9
442 KM SUBAREA S9
443 KO 0 0 7 21
444 BA .0355
445 LS 0 84
446 US .37 .68

```

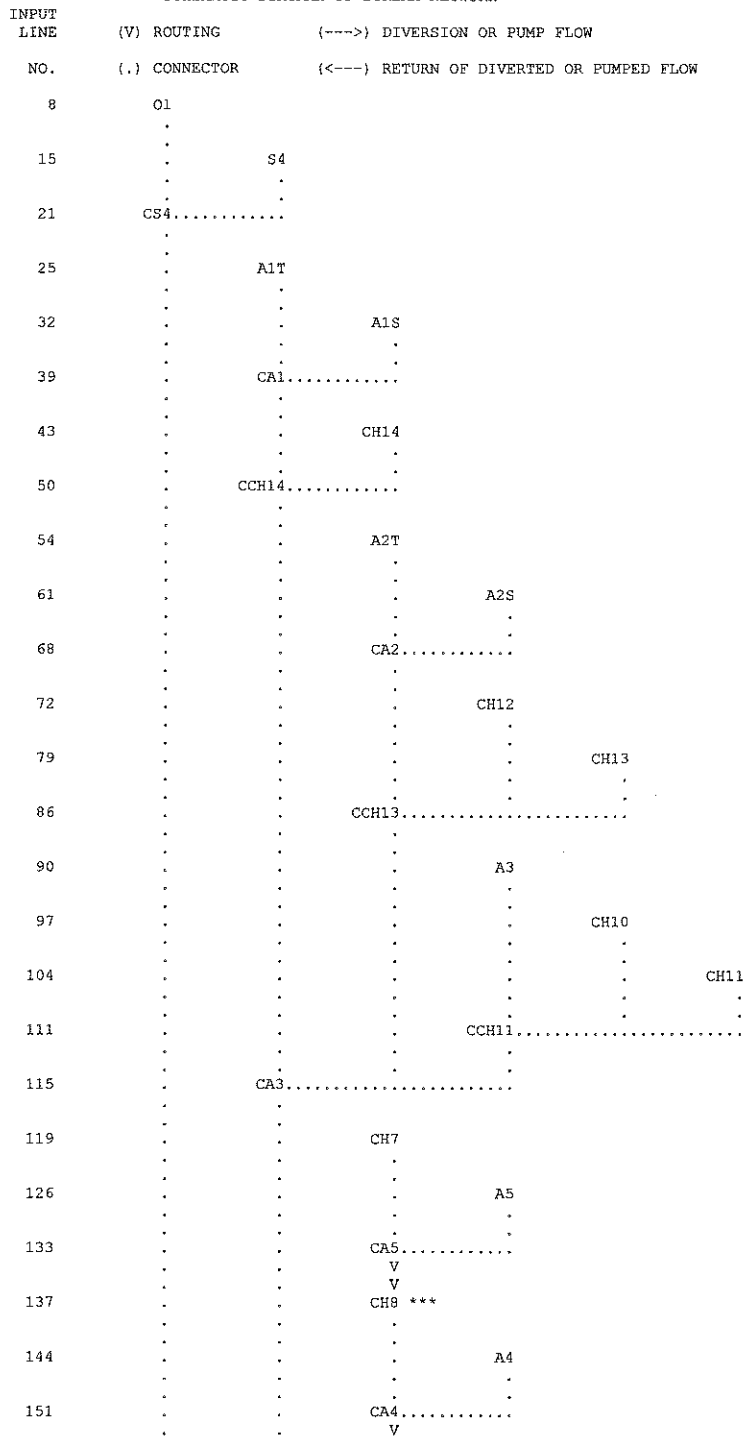
```

*
447      KK      S10
448      KM      SUBAREA S10
449      KO      0      0      7      21
450      BA      .0168
451      LS      0      84
452      US      .27      .68
*
453      KK      CS9
454      KM      COMBINE AREAS DISCHARGING SOUTH OFF OF P.B.
455      KO      0      0      0      7      21
456      HC      3
*
457      ZZ

```

1

SCHEMATIC DIAGRAM OF STREAM NETWORK



```

155      .      .      V
      .      .      CH9 ***
162      .      .      .      P1
      .      .      .      .
168      .      P1-IN.....
      .      V
172      .      RP1
      .      .
180      .      CP1.....
      .      .
184      .      S5
      .      .
190      .      CS5.....
      .      .
194      .      S7
      .      .
200      .      CS7.....
      .      .
204      .      O1A
      .      .
210      .      .      O2
      .      .      .
216      .      .      .      O3
      .      .      .      .
222      .      .      .      .      S6
      .      .      .      .      .
228      .      .      .      .      .
      .      .      .      .      .
      .      .      .      .      .
232      .      .      O4
      .      .      .
238      .      .      CO4.....
      .      .      .
242      .      .      A6
      .      .      .
249      .      .      .      S8
      .      .      .      .
255      .      .      .      .      .
      .      .      .      .      .
      .      .      .      .      .
259      .      .      S1
      .      .      .
265      .      .      .      S2
      .      .      .      V
      .      .      .      V
271      .      .      .      CH1 ***
      .      .      .      .
278      .      .      .      .      S3
      .      .      .      .      .
284      .      .      .      .      .      O5
      .      .      .      .      .      .
290      .      .      .      .      .      .
      .      .      .      .      .      .
      .      .      .      .      .      .
294      .      .      .      CH2
      .      .      .      .
301      .      .      .      .      A12
      .      .      .      .      .
308      .      .      .      .      .      CA12.....
      .      .      .      .      .      V
      .      .      .      .      .      V
312      .      .      .      .      .      CH3 ***
      .      .      .      .      .      .
319      .      .      .      .      .      .      A11
      .      .      .      .      .      .      .
326      .      .      .      .      .      .      CA11.....
      .      .      .      .      .      .      V
      .      .      .      .      .      .      V
330      .      .      .      .      .      .      CH4 ***
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337 . . . . . A10T
. . . . .
344 . . . . . A10S
. . . . .
351 . . . . . CA10.....
. . . . .
355 . . . . . A9
. . . . .
362 . . . . . P2
. . . . .
368 . . . . . P2-IN.....
. . . . . V
. . . . . V
372 . . . . . RP2
. . . . . V
. . . . . V
380 . . . . . CH5 ***
. . . . .
387 . . . . . A7T
. . . . .
394 . . . . . A7S
. . . . .
401 . . . . . CA7.....
. . . . .
405 . . . . . A8
. . . . .
412 . . . . . P3
. . . . .
418 . . . . . P3-IN.....
. . . . . V
. . . . . V
422 . . . . . RP3
. . . . . V
. . . . . V
430 . . . . . CH6 ***
. . . . .
437 . . . . . CCH6.....
. . . . .
441 . . . . . S9
. . . . .
447 . . . . . S10
. . . . .
453 . . . . . CS9.....

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(***) RUNOFF ALSO COMPUTED AT THIS LOCATION
*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 13MAY11 TIME 13:24:13 *
*****

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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

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CAMELOT LANDFILL
PROPOSED EXPANSION CONDITION
25-YEAR, 24-HOUR STORM EVENT
FILE:\SOLID WASTE\CITY OF FARMERS BRANCH\EXPANSION\
PARTIII-SDP\APPENDIX IIIF\IIIFA\HEC-1\PROP25.IH1

```

```

7 IO OUTPUT CONTROL VARIABLES
      IPRNT 3 PRINT CONTROL
      IPLOT 0 PLOT CONTROL
      QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
      NMIN 5 MINUTES IN COMPUTATION INTERVAL
      IDATE 1 0 STARTING DATE
      ITIME 0000 STARTING TIME
      NQ 720 NUMBER OF HYDROGRAPH ORDINATES
      NDDATE 4 0 ENDING DATE
      NDTIME 1155 ENDING TIME
      ICENT 19 CENTURY MARK

      COMPUTATION INTERVAL .08 HOURS
      TOTAL TIME BASE 59.92 HOURS

```

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRES- FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

 * *
 8 KK * O1 *
 * *

OFFSITE AREA O1

10 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

11 BA SUBBASIN CHARACTERISTICS
 TAREA .14 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .14

13 LS SCS LOSS RATE
 STRTL .30 INITIAL ABSTRACTION
 CRVNBR 87.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

14 US SNYDER UNITGRAPH
 TP .39 LAG
 CP .64 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS
 CLARK TC= .45 HR, R= .34 HR
 SNYDER TP= .39 HR, CP= .65

UNIT HYDROGRAPH
 25 END-OF-PERIOD ORDINATES
 13. 46. 89. 127. 144. 135. 110. 86. 67. 53.
 41. 32. 25. 20. 15. 12. 9. 7. 6. 5.
 4. 3. 2. 2. 1.

*** **

HYDROGRAPH AT STATION O1

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.53, TOTAL EXCESS = 5.90

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
298.	12.42	70.	22.	9.	9.
		(INCHES) 4.730	5.877	5.877	5.877
		(AC-FT) 34.	43.	43.	43.

CUMULATIVE AREA = .14 SQ MI

 * *
 15 KK * S4 *
 * *

SUBAREA S4

17 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

18 BA SUBBASIN CHARACTERISTICS
 TAREA .07 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
 STORM AREA = .07

19 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

20 US SNYDER UNITGRAPH
 TP .83 LAG
 CP .66 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS

CLARK TC= .94 HR, R= .69 HR
 SNYDER TP= .84 HR, CP= .67

UNIT HYDROGRAPH
 50 END-OF-PERIOD ORDINATES

1.	4.	8.	13.	18.	24.	28.	32.	34.	36.
35.	33.	29.	26.	23.	20.	18.	16.	14.	13.
11.	10.	9.	8.	7.	6.	5.	5.	4.	4.
3.	3.	3.	2.	2.	2.	2.	1.	1.	1.
1.	1.	1.	1.	1.	1.	0.	0.	0.	0.

*** *** *** *** ***

HYDROGRAPH AT STATION S4

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
94.	12.92	33.	10.	4.	4.
		(INCHES) 4.467	5.531	5.531	5.531
		(AC-FT) 16.	20.	20.	20.

CUMULATIVE AREA = .07 SQ MI

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 * *
 21 KK * CS4 *
 * *

COMBINE AREAS PRIOR TO POND P1 OUTLET

23 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

24 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** *** *** *** ***

HYDROGRAPH AT STATION CS4

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	59.92-HR	
364.	12.50	102.	32.	13.	13.	
		(INCHES)	4.633	5.763	5.763	5.763
		(AC-FT)	51.	63.	63.	63.

CUMULATIVE AREA = .20 SQ MI

 * *
 25 KK * ALT *
 * *

SUBAREA AIT

27 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

28 BA SUBBASIN CHARACTERISTICS

TAREA	.01	SUBBASIN AREA
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PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .01

29 LS SCS LOSS RATE

STRTL	.38	INITIAL ABSTRACTION
CRVNER	84.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

30 UK OVERLAND-FLOW ELEMENT NO. 1

L	265.	OVERLAND FLOW LENGTH
S	.0400	SLOPE
N	.350	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

MUSKINGUM-CUNGE

31 RD MAIN CHANNEL

L	507.	CHANNEL LENGTH
S	.0050	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.01	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	.00	BOTTOM WIDTH OR DIAMETER
Z	2.00	SIDE SLOPE
RUPSTQ	NO	ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)	DX (FT)				
PLANE1	.85	1.67	2.24	53.00	28.38	727.52	.40	
MAIN	1.63	1.33	2.26	253.50	27.96	728.16	3.74	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2520E+01 OUTFLOW= .2491E+01 BASIN STORAGE= .4099E-03 PERCENT ERROR= 1.1

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	1.63	1.33	5.00	27.39	730.00	5.49
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HYDROGRAPH AT STATION AIT

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	59.92-HR	
27.	12.17	4.	1.	1.	1.	
		(INCHES)	4.488	5.487	5.492	5.492
		(AC-FT)	2.	2.	2.	2.

CUMULATIVE AREA = .01 SQ MI

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* *
32 KK * ALS *
* *

SUBAREA A1S

34 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLDT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

35 BA SUBBASIN CHARACTERISTICS

TAREA	.03	SUBBASIN AREA
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PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .03

36 LS SCS LOSS RATE

STRTL	.33	INITIAL ABSTRACTION
CRVNBR	86.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

37 UK OVERLAND-FLOW ELEMENT NO. 1

L	120.	OVERLAND FLOW LENGTH
S	.2500	SLOPE
N	.350	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

38 RD MUSKINGUM-CUNGE MAIN CHANNEL

L	881.	CHANNEL LENGTH
S	.0050	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.03	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	.00	BOTTOM WIDTH OR DIAMETER
Z	2.00	SIDE SLOPE
RUPSTQ	NO	ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)				
PLANE1	2.13	1.67	.70	24.00	145.61	725.02	.61
MAIN	1.63	1.33	2.61	440.50	137.15	724.04	5.62

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .8923E+01 OUTFLOW= .8693E+01 BASIN STORAGE= .4875E-03 PERCENT ERROR= 2.6

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	1.63	1.33	5.00	131.18	725.00	5.64
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HYDROGRAPH AT STATION ALS

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
131.	12.08	14.	4.	2.	2.
		4.649 (INCHES)	5.640	5.641	5.641
		7. (AC-FT)	9.	9.	9.

CUMULATIVE AREA = .03 SQ MI

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* *
39 KK * CA1 *
* *

COMBINE A1 SUBAREAS

41 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

42 HC HYDROGRAPH COMBINATION

ICOMP	2	NUMBER OF HYDROGRAPHS TO COMBINE
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HYDROGRAPH AT STATION CA1

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
156.	12.08	19.	6.	2.	2.
		4.610 (INCHES)	5.605	5.607	5.607
		9. (AC-FT)	11.	11.	11.

CUMULATIVE AREA = .04 SQ MI

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* *
43 KK * CH14 *
* *

SUBAREA CH14

45 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

46 BA SUBBASIN CHARACTERISTICS

TAREA	.00	SUBBASIN AREA
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PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .00

47 LS SCS LOSS RATE

STRTL	.38	INITIAL ABSTRACTION
CRVNR	84.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

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KINEMATIC WAVE
48 UK OVERLAND-FLOW ELEMENT NO. 1
      L 52. OVERLAND FLOW LENGTH
      S .1000 SLOPE
      N .350 ROUGHNESS COEFFICIENT
      PA 100.0 PERCENT OF SUBBASIN
      DXMIN 5 MINIMUM NUMBER OF DX INTERVALS
MUSKINGUM-CUNGE
49 RD MAIN CHANNEL
      L 524. CHANNEL LENGTH
      S .0050 SLOPE
      N .030 CHANNEL ROUGHNESS COEFFICIENT
      CA .00 CONTRIBUTING AREA
      SHAPE TRAP CHANNEL SHAPE
      WD .00 BOTTOM WIDTH OR DIAMETER
      Z 3.00 SIDE SLOPE
      RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

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COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)				
PLANE1	1.35	1.67	.67	10.40	7.93	724.45	.33
MAIN	1.48	1.33	3.46	262.00	7.12	725.83	2.53

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .4743E+00 OUTFLOW= .4688E+00 BASIN STORAGE= .3115E-03 PERCENT ERROR= 1.1

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

ELEMENT	ALPHA	M	DT	DX	PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELERITY
			(MIN)	(FT)	(CFS)	(MIN)	(IN)	(FPS)
MAIN	1.48	1.33	5.00		7.05	725.00	5.48	

HYDROGRAPH AT STATION CH14

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR (CFS)	24-HR (INCHES)	72-HR (AC-FT)	59.92-HR (CFS)
7.	12.08	1.	0.	0.	0.
		4.503	5.483	5.483	5.483
		0.	0.	0.	0.

CUMULATIVE AREA = .00 SQ MI

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*****
* CCH14 *
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COMBINE CH14 WITH A1 AREAS

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52 KO OUTPUT CONTROL VARIABLES
      IPRNT 3 PRINT CONTROL
      IPLOT 0 PLOT CONTROL
      QSCAL 0. HYDROGRAPH PLOT SCALE
      IPNCH 7 PUNCH COMPUTED HYDROGRAPH
      IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
      ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
      ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
      TIMINT .083 TIME INTERVAL IN HOURS

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53 HC HYDROGRAPH COMBINATION
      ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION CCH14

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR (CFS)	24-HR (INCHES)	72-HR (AC-FT)	59.92-HR (CFS)
163.	12.08	19.	6.	2.	2.
		4.605	5.600	5.602	5.602
		10.	12.	12.	12.

CUMULATIVE AREA = .04 SQ MI

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 54 KK * A2T *
 * *

SUBAREA A27

56 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

57 BA SUBBASIN CHARACTERISTICS
 TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
 STORM AREA = .02

58 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

59 UK OVERLAND-FLOW ELEMENT NO. 1
 L 312. OVERLAND FLOW LENGTH
 S .0400 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

MUSKINGUM-CUNGE

60 RD MAIN CHANNEL
 L 879. CHANNEL LENGTH
 S .0050 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .02 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER
 Z 2.00 SIDE SLOPE
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS
 COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	.85	1.67	2.54	62.40	58.76	728.32	5.55	.42
MAIN	1.63	1.33	3.28	439.50	57.59	730.43	5.45	4.47

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .5484E+01 OUTFLOW= .5382E+01 BASIN STORAGE= .9579E-03 PERCENT ERROR= 1.9

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1.63 1.33 5.00 57.39 730.00 5.45

*** **

HYDROGRAPH AT STATION A2T

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (INCHES)	72-HR (AC-FT)	59.92-HR (FPS)
57.	12.17	9.	4.484	4.	1.
		3.	5.446	5.	1.
		1.	5.452	5.	1.

CUMULATIVE AREA = .02 SQ MI

*** **

 * *
 61 KK * A2S *
 * *

SUBAREA A2S

63 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

64 BA SUBBASIN CHARACTERISTICS
 TAREA .03 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .03

65 LS SCS LOSS RATE
 STRTL .33 INITIAL ABSTRACTION
 CRVNBR 86.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

66 UK OVERLAND-FLOW ELEMENT NO. 1
 L 120. OVERLAND FLOW LENGTH
 S .2500 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

MUSKINGUM-CUNGE

67 RD MAIN CHANNEL
 L 925. CHANNEL LENGTH
 S .0050 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .03 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER
 Z 2.00 SIDE SLOPE
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELERITY
		M	DT				
PLANE1	2.13	1.67	.70	24.00	162.24	725.02	.61
MAIN	1.63	1.33	2.67	462.50	150.43	723.85	5.77

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .9942E+01 OUTFLOW= .9680E+01 BASIN STORAGE= .5134E-03 PERCENT ERROR= 2.6

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1.63 1.33 5.00 144.46 725.00 5.63

*** **

HYDROGRAPH AT STATION A2S

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
+ 144.	12.08	16.	5.	2.	2.
		(INCHES) 4.641	5.632	5.632	5.632
		(AC-FT) 8.	10.	10.	10.

CUMULATIVE AREA = .03 SQ MI

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* *
68 KK * CA2 *
* *

COMBINE A2 SUBAREAS

70 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

71 HC HYDROGRAPH COMBINATION
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION CA2

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	59.92-HR	
		(CFS)				
+ 195.	12.08	25.	8.	3.	3.	
		(INCHES)	4.580	5.564	5.567	5.567
		(AC-FT)	12.	15.	15.	15.
CUMULATIVE AREA =		.05 SQ MI				

*** **

* *
72 KK * CH12 *
* *

SUBAREA CH12

74 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

75 BA SUBBASIN CHARACTERISTICS
TAREA .00 SUBBASIN AREA

PRECIPITATION DATA

HYDRO-35	DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM						TP-49				
	5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00
STORM AREA =								.00			

76 LS SCS LOSS RATE
STRTL .38 INITIAL ABSTRACTION
CRVNR 84.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

77 UK OVERLAND-FLOW ELEMENT NO. 1
L 52. OVERLAND FLOW LENGTH
S .1000 SLOPE
N .350 ROUGHNESS COEFFICIENT
PA 100.0 PERCENT OF SUBBASIN
DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

MUSKINGUM-CUNGE

78 RD MAIN CHANNEL
L 313. CHANNEL LENGTH
S .0050 SLOPE
N .030 CHANNEL ROUGHNESS COEFFICIENT
CA .00 CONTRIBUTING AREA
SHAPE TRAP CHANNEL SHAPE

WD .00 BOTTOM WIDTH OR DIAMETER
 Z 3.00 SIDE SLOPE
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)				
PLANE1	1.35	1.67	.67	10.40	4.46	724.45	5.56
MAIN	1.48	1.33	2.38	156.50	4.44	724.72	5.50

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2668E+00 OUTFLOW= .2641E+00 BASIN STORAGE= .1752E-03 PERCENT ERROR= .9

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1.48 1.33 5.00 4.31 725.00 5.51

*** **

HYDROGRAPH AT STATION CH12

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR (CFS)	24-HR	72-HR	59.92-HR
4.	12.08	0.	0.	0.	0.
		(INCHES) 4.524	5.512	5.512	5.512
		(AC-FT) 0.	0.	0.	0.

CUMULATIVE AREA = .00 SQ MI

*** **

 * *
 79 KK * CH13 *
 * *

SUBAREA CH13

81 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

82 BA SUBBASIN CHARACTERISTICS
 TAREA .00 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .00

83 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

84 UK OVERLAND-FLOW ELEMENT NO. 1
 L 52. OVERLAND FLOW LENGTH
 S .1000 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

MUSKINGUM-CUNGE

85 RD MAIN CHANNEL
 L 634. CHANNEL LENGTH
 S .0050 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER

Z 3.00 SIDE SLOPE
RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS
COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DK (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	1.35	1.67	.67	10.40	9.91	724.45	5.56	.33
MAIN	1.48	1.33	3.96	317.00	9.58	723.77	5.48	2.67

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .5929E+00 OUTFLOW= .5848E+00 BASIN STORAGE= .3570E-03 PERCENT ERROR= 1.3

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1.48 1.33 5.00 8.74 725.00 5.47

*** **

HYDROGRAPH AT STATION CH13

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
9.	12.08	1.	0.	0.	0.
		(INCHES) 4.495	5.473	5.473	5.473
		(AC-FT) 0.	1.	1.	1.

CUMULATIVE AREA = .00 SQ MI

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* *
86 KK * CCH13 *
* *

COMBINE CH12 AND CH13 WITH A2 AREAS

88 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

89 HC HYDROGRAPH COMBINATION
ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION CCH13

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
208.	12.08	26.	8.	3.	3.
		(INCHES) 4.576	5.560	5.562	5.562
		(AC-FT) 13.	16.	16.	16.

CUMULATIVE AREA = .05 SQ MI

*** **

* *
90 KK * A3 *
* *

SUBAREA A3

92 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL

QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

93 BA SUBBASIN CHARACTERISTICS
 TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
 STORM AREA = .01

94 LS SCS LOSS RATE
 STRTL .33 INITIAL ABSTRACTION
 CRVNER 86.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

95 UK OVERLAND-FLOW ELEMENT NO. 1
 L 120. OVERLAND FLOW LENGTH
 S .2500 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

96 RD MUSKINGUM-CUNGE
 MAIN CHANNEL
 L 630. CHANNEL LENGTH
 S .0050 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .01 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER
 Z 2.00 SIDE SLOPE
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FFS)
		M	DT (MIN)	DX (FT)				
PLANE1	2.13	1.67	.70	24.00	63.48	725.03	.61	
MAIN	1.63	1.33	2.30	315.00	61.93	724.85	4.56	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .3890E+01 OUTFLOW= .3800E+01 BASIN STORAGE= .3366E-03 PERCENT ERROR= 2.3

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1.63 1.33 5.00 61.14 725.00 5.68

*** **

HYDROGRAPH AT STATION A3

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	59.92-HR	
61.	12.08	6.	2.	1.	1.	
		(INCHES)	4.675	5.676	5.676	5.676
		(AC-FT)	3.	4.	4.	4.

CUMULATIVE AREA = .01 SQ MI

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 * *
 97 KK * CH10 *
 * *

SUBAREA CH10

99 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

100 BA SUBBASIN CHARACTERISTICS
 TAREA .00 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .00

101 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNER 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

102 UK OVERLAND-FLOW ELEMENT NO. 1
 L 52. OVERLAND FLOW LENGTH
 S .1000 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

MUSKINGUM-CUNGE

103 RD MAIN CHANNEL
 L 483. CHANNEL LENGTH
 S .0050 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER
 Z 3.00 SIDE SLOPE
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)	DX (FT)				
PLANE1	1.35	1.67	.67	10.40	6.44	724.45	.33	
MAIN	1.48	1.33	3.36	241.50	6.35	724.81	2.40	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .3854E+00 OUTFLOW= .3819E+00 BASIN STORAGE= .2777E-03 PERCENT ERROR= .8

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1.48 1.33 5.00 6.23 725.00 5.55

*** **

HYDROGRAPH AT STATION CH10

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR (CFS)	24-HR	72-HR	59.92-HR
+ 6.	12.08	1.	0.	0.	0.
		(INCHES) 4.568	5.548	5.549	5.549
		(AC-FT) 0.	0.	0.	0.

CUMULATIVE AREA = .00 SQ MI

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 104 KK * CH11 *
 * *

SUBAREA CH11

106 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH

IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

107 BA SUBBASIN CHARACTERISTICS
 TAREA .00 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
 STORM AREA = .00

108 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

109 UK OVERLAND-FLOW ELEMENT NO. 1
 L 52. OVERLAND FLOW LENGTH
 S .1000 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

MUSKINGUM-CUNGE

110 RD MAIN CHANNEL
 L 313. CHANNEL LENGTH
 S .0050 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER
 Z 3.00 SIDE SLOPE
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELERITY
		M	DT				
PLANE1	1.35	1.67	.67	10.40	4.46	724.45	5.56
MAIN	1.48	1.33	2.38	156.50	4.44	724.72	5.50

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2668E+00 OUTFLOW= .2641E+00 BASIN STORAGE= .1752E-03 PERCENT ERROR= .9

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1.48 1.33 5.00 4.31 725.00 5.51

*** **

HYDROGRAPH AT STATION CH11

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
+ (CFS)	(HR)	(CFS)			
+ 4.	12.08	0.	0.	0.	0.
		(INCHES)	4.524	5.512	5.512
		(AC-FT)	0.	0.	0.

CUMULATIVE AREA = .00 SQ MI

*** **

111 KK

 * *
 * CCH11 *
 * *

COMBINE CH10 AND CH11 WITH AREA A3

113 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT

ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

114 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

*** *** *** *** ***

HYDROGRAPH AT STATION CCH11

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
72.	12.08	7.	2.	1.	1.
		(INCHES) 4.656	5.655	5.655	5.655
		(AC-FT) 4.	4.	4.	4.

CUMULATIVE AREA = .01 SQ MI

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 * *
 115 KK * CA3 *
 * *

COMBINE AREAS FLOWING DIRECTLY INTO P1

117 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

118 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

*** *** *** *** ***

HYDROGRAPH AT STATION CA3

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
443.	12.08	53.	16.	6.	6.
		(INCHES) 4.597	5.587	5.589	5.589
		(AC-FT) 26.	32.	32.	32.

CUMULATIVE AREA = .11 SQ MI

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 * *
 119 KK * CH7 *
 * *

CHANNEL CH7

121 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

122 BA SUBBASIN CHARACTERISTICS
 TAREA .00 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .00

123 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNER 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

124 UK KINEMATIC WAVE
 OVERLAND-FLOW ELEMENT NO. 1
 L 82. OVERLAND FLOW LENGTH
 S .2500 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

125 RD MUSKINGUM-CUNGE
 MAIN CHANNEL
 L 830. CHANNEL LENGTH
 S .0030 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 5.00 BOTTOM WIDTH OR DIAMETER
 Z 2.00 SIDE SLOPE
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)	DX (FT)				
PLANE1	2.13	1.67	.69	16.40	17.84	724.42	.53	
MAIN	.98	1.39	5.00	415.00	16.54	725.00	2.54	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .1067E+01 OUTFLOW= .1026E+01 BASIN STORAGE= .7822E-03 PERCENT ERROR= 3.7

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN .98 1.39 5.00 16.54 725.00 5.35

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HYDROGRAPH AT STATION CH7

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
17.	12.08	2.	1.	0.	0.
		(INCHES) 4.438	5.346	5.347	5.347
		(AC-FT) 1.	1.	1.	1.

CUMULATIVE AREA = .00 SQ MI

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 126 KK * A5 *
 * *

SUBAREA A5

128 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

129 BA SUBBASIN CHARACTERISTICS
 TAREA .03 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .03

130 LS SCS LOSS RATE
 STRTL .33 INITIAL ABSTRACTION
 CRVNR 86.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

131 UK KINEMATIC WAVE
 OVERLAND-FLOW ELEMENT NO. 1
 L 120. OVERLAND FLOW LENGTH
 S .2500 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

132 RD MUSKINGUM-CUNGE
 MAIN CHANNEL
 L 1007. CHANNEL LENGTH
 S .0050 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .03 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER
 Z 2.00 SIDE SLOPE
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS
 COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	2.13	1.67	.70	24.00	149.64	725.02	5.79	.61
MAIN	1.63	1.33	2.97	503.50	140.34	724.03	5.63	5.66

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .9170E+01 OUTFLOW= .8918E+01 BASIN STORAGE= .5553E-03 PERCENT ERROR= 2.7

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1.63 1.33 5.00 133.57 725.00 5.62

*** **

HYDROGRAPH AT STATION A5

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (INCHES)	72-HR (INCHES)	59.92-HR (AC-FT)
134.	12.08	15.	4.629	4.	5.617
			7.	5.617	9.
				9.	9.

CUMULATIVE AREA = .03 SQ MI

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 133 KK * CA5 *
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COMBINE CH7 AND A5 BEFORE ROUTING THROUGH CH8

135 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

136 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION CA5

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
150.	12.08	17.	5.	2.	2.
		(CFS)	(CFS)	(CFS)	(CFS)
		(INCHES)	(INCHES)	(INCHES)	(INCHES)
		4.609	5.587	5.588	5.588
		8.	10.	10.	10.

CUMULATIVE AREA = .03 SQ MI

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 137 KK * CH8 *
 * *

 CHANNEL CH8

139 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLST	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

140 BA SUBBASIN CHARACTERISTICS
 TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .01

141 LS SCS LOSS RATE

STRFL	.38	INITIAL ABSTRACTION
CRVNBR	84.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

142 UK KINEMATIC WAVE
 OVERLAND-FLOW ELEMENT NO. 1

L	46.	OVERLAND FLOW LENGTH
S	.0652	SLOPE
N	.350	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

143 RD MUSKINGUM-CUNGE
 MAIN CHANNEL

L	707.	CHANNEL LENGTH
S	.0300	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.01	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	5.00	BOTTOM WIDTH OR DIAMETER
Z	2.00	SIDE SLOPE
RUPSTQ	YES	ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	M	COMPUTATION TIME STEP		PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
			DT (MIN)	DX (FT)				
PLANE1	1.09	1.67	.57	9.20	26.40	724.95	5.56	.28
MAIN	3.11	1.39	1.07	353.50	168.61	725.84	5.57	11.06

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9924E+01 EXCESS= .1571E+01 OUTFLOW= .1146E+02 BASIN STORAGE= .2671E-03 PERCENT ERROR= .3

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	3.11	1.39	5.00	166.32	725.00	5.57
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HYDROGRAPH AT STATION CH8

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	59.92-HR	
166.	12.08	19.	6.	2.	2.	
		(INCHES)	4.601	5.574	5.575	5.575
		(AC-FT)	9.	11.	11.	11.

CUMULATIVE AREA = .04 SQ MI

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 * *
 144 KK * A4 *
 * *

SUBAREA A4

146 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLST	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

147 BA SUBBASIN CHARACTERISTICS

TAREA	.02	SUBBASIN AREA
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PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .02

148 LS SCS LOSS RATE

STRTL	.33	INITIAL ABSTRACTION
CRVNR	86.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

149 UK OVERLAND-FLOW ELEMENT NO. 1

L	120.	OVERLAND FLOW LENGTH
S	.2500	SLOPE
N	.350	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

MUSKINGUM-CUNGE

150 RD MAIN CHANNEL

L	403.	CHANNEL LENGTH
S	.0050	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.02	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	.00	BOTTOM WIDTH OR DIAMETER
Z	2.00	SIDE SLOPE
RUPSTQ	NO	ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)				
PLANE1	2.13	1.67	.70	24.00	106.31	725.02	5.79
MAIN	1.63	1.33	1.29	403.00	102.51	724.49	5.08

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .6515E+01 OUTFLOW= .5714E+01 BASIN STORAGE= .2350E-03 PERCENT ERROR= 12.3

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	1.63	1.33	5.00	100.30	725.00	5.09
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HYDROGRAPH AT STATION A4

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79

PEAK FLOW TIME MAXIMUM AVERAGE FLOW

		6-HR	24-HR	72-HR	59.92-HR
+ (CFS)	(HR)				
+ 100.	12.08	10.	3.	1.	1.
		(INCHES) 4.353	5.087	5.088	5.088
		(AC-FT) 5.	6.	6.	6.

CUMULATIVE AREA = .02 SQ MI

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 151 KK * CA4 *
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COMBINE WITH A4 BEFORE ROUTING THROUGH CH9

153 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

154 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION CA4

			MAXIMUM AVERAGE FLOW			
PEAK FLOW	TIME		6-HR	24-HR	72-HR	59.92-HR
+ (CFS)	(HR)	(CFS)				
+ 267.	12.08	29.	9.	3.	3.	
		(INCHES) 4.513	5.402	5.403	5.403	5.403
		(AC-FT) 14.	17.	17.	17.	17.

CUMULATIVE AREA = .06 SQ MI

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 155 KK * CH9 *
 * *

CHANNEL CH9

157 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

158 BA SUBBASIN CHARACTERISTICS
 TAREA .00 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .00

159 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

160 UK KINEMATIC WAVE
 OVERLAND-FLOW ELEMENT NO. 1

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      L      75. OVERLAND FLOW LENGTH
      S      .1000 SLOPE
      N      .350 ROUGHNESS COEFFICIENT
      PA     100.0 PERCENT OF SUBBASIN
      DXMIN   5   MINIMUM NUMBER OF DX INTERVALS
161 RD  MUSKINGUM-CUNGE
      MAIN CHANNEL
      L      670. CHANNEL LENGTH
      S      .0300 SLOPE
      N      .030 CHANNEL ROUGHNESS COEFFICIENT
      CA      .00 CONTRIBUTING AREA
      SHAPE   TRAP CHANNEL SHAPE
      WD      5.00 BOTTOM WIDTH OR DIAMETER
      Z      2.00 SIDE SLOPE
      RUPSTQ  YES ROUTE UPSTREAM HYDROGRAPH

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COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)					
PLANE1	1.35	1.67	.74	15.00	23.33	724.59	5.56	.38
MAIN	3.11	1.39	.88	335.00	280.65	725.43	5.41	12.67

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1720E+02 EXCESS= .1423E+01 OUTFLOW= .1860E+02 BASIN STORAGE= .2560E-03 PERCENT ERROR= .2

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

	MAIN	3.11	1.39	5.00	274.91	725.00	5.41
***	***	***	***	***	***	***	***
HYDROGRAPH AT STATION CH9							
TOTAL RAINFALL =	7.44,	TOTAL LOSS =	1.88,	TOTAL EXCESS =	5.56		
PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW					
(CFS)	(HR)	6-HR	24-HR	72-HR	59.92-HR		
+ 275.	12.08	31.	9.	4.	4.		
		(INCHES)	4.518	5.411	5.411	5.411	
		(AC-FT)	16.	19.	19.	19.	
CUMULATIVE AREA =		.06 SQ MI					

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162 KK * P1 *
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DETENTION POND P1

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164 KO OUTPUT CONTROL VARIABLES
      IPRNT  3 PRINT CONTROL
      IPLOT  0 PLOT CONTROL
      QSCAL  0. HYDROGRAPH PLOT SCALE
      IPNCH  7 PUNCH COMPUTED HYDROGRAPH
      IOUT   21 SAVE HYDROGRAPH ON THIS UNIT
      ISAV1  1 FIRST ORDINATE PUNCHED OR SAVED
      ISAV2  720 LAST ORDINATE PUNCHED OR SAVED
      TIMINT .083 TIME INTERVAL IN HOURS

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SUBBASIN RUNOFF DATA

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165 BA SUBBASIN CHARACTERISTICS
      TAREA .04 SUBBASIN AREA

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PRECIPITATION DATA

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12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
..... HYDRO-35 ..... TP-40 ..... TP-49 .....
5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
.74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
      STORM AREA = .04

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166 LS SCS LOSS RATE
      STRTL .00 INITIAL ABSTRACTION
      CRVNBR 100.00 CURVE NUMBER
      RTIMP .00 PERCENT IMPERVIOUS AREA

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167 UD SCS DIMENSIONLESS UNITGRAPH
      TLAG .00 LAG

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UNIT HYDROGRAPH
5 END-OF-PERIOD ORDINATES
0.

208. 58. 11. 2.

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HYDROGRAPH AT STATION P1

TOTAL RAINFALL = 7.44, TOTAL LOSS = .00, TOTAL EXCESS = 7.44

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	59.92-HR
186.	12.08	(CFS)	21.	7.	3.	3.
		(INCHES)	5.468	7.437	7.440	7.440
		(AC-FT)	11.	14.	14.	14.

CUMULATIVE AREA = .04 SQ MI

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168 KK * P1-IN *
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COMBINE AREAS DISCHARGING TO POND P1

170 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

171 HC HYDROGRAPH COMBINATION

ICOMP	3	NUMBER OF HYDROGRAPHS TO COMBINE
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HYDROGRAPH AT STATION P1-IN

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	59.92-HR
904.	12.08	(CFS)	105.	33.	13.	13.
		(INCHES)	4.711	5.839	5.855	5.855
		(AC-FT)	52.	65.	65.	65.

CUMULATIVE AREA = .21 SQ MI

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172 KK * RP1 *
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ROUTE THROUGH POND P1

174 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

HYDROGRAPH ROUTING DATA

175 RS STORAGE ROUTING

NSTPS	1	NUMBER OF SUBREACHES
ITYP	ELEV	TYPE OF INITIAL CONDITION
RSVRIC	454.50	INITIAL CONDITION
X	.00	WORKING R AND D COEFFICIENT

176 SA	AREA	.0	17.8	18.2	18.6	19.0	19.4	19.8	20.2
177 SE	ELEVATION	454.50	455.00	456.00	457.00	458.00	459.00	460.00	461.00
179 SL	LOW-LEVEL OUTLET								
	ELEVL	455.50	ELEVATION AT CENTER OF OUTLET						
	CAREA	3.14	CROSS-SECTIONAL AREA						
	COQL	.80	COEFFICIENT						
	EXPL	.50	EXPONENT OF HEAD						
178 SS	SPILLWAY								
	CREL	458.00	SPILLWAY CREST ELEVATION						
	SPWID	25.00	SPILLWAY WIDTH						
	COQW	2.60	WEIR COEFFICIENT						
	EXPW	1.50	EXPONENT OF HEAD						

COMPUTED STORAGE-ELEVATION DATA

STORAGE	.00	2.96	20.92	39.29	58.07	77.27	96.88	116.91
ELEVATION	454.50	455.00	456.00	457.00	458.00	459.00	460.00	461.00

COMPUTED OUTFLOW-ELEVATION DATA

OUTFLOW	.00	.00	19.56	20.70	21.98	23.44	25.10	27.01	29.24	31.87
ELEVATION	454.50	455.50	456.44	456.55	456.69	456.85	457.05	457.30	457.60	458.00
OUTFLOW	33.02	36.99	45.59	60.62	83.84	117.03	161.97	220.42	294.18	385.02
ELEVATION	458.05	458.16	458.32	458.54	458.81	459.14	459.52	459.96	460.45	461.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	2.96	11.89	20.92	28.97	31.05	33.54	36.54	39.29	40.22
OUTFLOW	.00	.00	.00	14.25	19.56	20.70	21.98	23.44	24.69	25.10
ELEVATION	454.50	455.00	455.50	456.00	456.44	456.55	456.69	456.85	457.00	457.05
STORAGE	44.80	50.59	58.07	59.09	61.10	64.16	68.31	73.55	77.27	79.89
OUTFLOW	27.01	29.24	31.87	33.02	36.99	45.59	60.62	83.84	102.71	117.03
ELEVATION	457.30	457.60	458.00	458.05	458.16	458.32	458.54	458.81	459.00	459.14
STORAGE	87.38	96.02	96.88	105.85	116.91					
OUTFLOW	161.97	220.42	226.61	294.18	385.02					
ELEVATION	459.52	459.96	460.00	460.45	461.00					

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HYDROGRAPH AT STATION RP1

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	59.92-HR	
+	(CFS)	(HR)					
+	28.	15.17	28.	23.	11.	11.	
			(INCHES)	1.242	4.051	4.752	4.752
			(AC-FT)	14.	45.	53.	53.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE				
			6-HR	24-HR	72-HR	59.92-HR	
+	(AC-FT)	(HR)					
+	48.	15.17	47.	36.	21.	21.	
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE				
			6-HR	24-HR	72-HR	59.92-HR	
+	(FEET)	(HR)					
+	457.46	15.17	457.40	456.82	455.94	455.94	

CUMULATIVE AREA = .21 SQ MI

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 180 KK * *
 * CP1 *
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COMBINE DOWNSTREAM OF POND P1 OUTLET

182 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPL0T	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOU7	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

183 HC HYDROGRAPH COMBINATION

ICOMP	2	NUMBER OF HYDROGRAPHS TO COMBINE
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HYDROGRAPH AT STATION CP1

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
+ (CFS)	(HR)	(CFS)			
+ 389.	12.50	125.	52.	23.	23.
		(INCHES)	2.826	4.684	5.253
		(AC-FT)	62.	103.	116.

CUMULATIVE AREA = .41 SQ MI

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 * *
 184 KK * S5 *
 * *

SUBAREA S5

186 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

187 BA SUBBASIN CHARACTERISTICS

TAREA	.01	SUBBASIN AREA
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PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .01

188 LS SCS LOSS RATE

STRTL	.38	INITIAL ABSTRACTION
CRVNBR	84.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

189 US SNYDER UNITGRAPH

TP	.59	LAG
CP	.71	PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS

CLARK	TC= .69 HR,	R= .42 HR
SNYDER	TP= .58 HR,	CP= .70

UNIT HYDROGRAPH
 32 END-OF-PERIOD ORDINATES

0.	2.	3.	5.	7.	8.	9.	9.	8.	7.
5.	4.	4.	3.	2.	2.	2.	1.	1.	1.
1.	1.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.								

*** *** *** *** ***

HYDROGRAPH AT STATION S5

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
+ (CFS)	(HR)	(CFS)			
+ 21.	12.58	6.	2.	1.	1.
		(INCHES)	4.489	5.535	5.535
		(AC-FT)	3.	3.	3.

CUMULATIVE AREA = .01 SQ MI

*** **

190 KK * CS5 *

COMBINE AREAS UPSTREAM OF S7

192 KO OUTPUT CONTROL VARIABLES IPRNT 3 PRINT CONTROL I PLOT 0 PLOT CONTROL QSCAL 0. HYDROGRAPH PLOT SCALE IPNCH 7 PUNCH COMPUTED HYDROGRAPH IOU 21 SAVE HYDROGRAPH ON THIS UNIT ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED ISAV2 720 LAST ORDINATE PUNCHED OR SAVED TIMINT .083 TIME INTERVAL IN HOURS

193 HC HYDROGRAPH COMBINATION ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION CS5

Table with columns: PEAK FLOW (CFS), TIME (HR), 6-HR, 24-HR, 72-HR, 59.92-HR. Includes cumulative area = .42 SQ MI.

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194 KK * S7 *

SUBAREA S7

196 KO OUTPUT CONTROL VARIABLES IPRNT 3 PRINT CONTROL I PLOT 0 PLOT CONTROL QSCAL 0. HYDROGRAPH PLOT SCALE IPNCH 7 PUNCH COMPUTED HYDROGRAPH IOU 21 SAVE HYDROGRAPH ON THIS UNIT ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED ISAV2 720 LAST ORDINATE PUNCHED OR SAVED TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

197 BA SUBBASIN CHARACTERISTICS TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

Table with columns: HYDRO-35 (5-MIN, 15-MIN, 60-MIN), DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM (2-HR, 3-HR, 6-HR, 12-HR, 24-HR), TP-40, TP-49 (2-DAY, 4-DAY, 7-DAY, 10-DAY). Includes storm area = .01.

198 LS SCS LOSS RATE STRTL .38 INITIAL ABSTRACTION CRVNBR 84.00 CURVE NUMBER RTIMP .00 PERCENT IMPERVIOUS AREA

199 US SNYDER UNITGRAPH TP .47 LAG CP .72 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS CLARK TC= .57 HR, R= .32 HR SNYDER TP= .47 HR, CP= .71

UNIT HYDROGRAPH 25 END-OF-PERIOD ORDINATES

1. 2. 4. 6. 8. 8. 8. 6. 5. 4.
 3. 2. 2. 1. 1. 1. 1. 0. 0. 0.
 0. 0. 0. 0. 0.

*** **

HYDROGRAPH AT STATION S7

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
17.	12.50	4.	1.	1.	1.
		(INCHES) 4.494	5.536	5.536	5.536
		(AC-FT) 2.	2.	2.	2.

CUMULATIVE AREA = .01 SQ MI

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 * *
 200 KK * CS7 *
 * *

COMBINE WITH AREA S7

202 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

203 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION CS7

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
426.	12.50	135.	55.	25.	25.
		(INCHES) 2.900	4.717	5.266	5.266
		(AC-FT) 67.	109.	121.	121.

CUMULATIVE AREA = .43 SQ MI

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 204 KK * O1A *
 * *

OFFSITE AREA O1A

206 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

207 BA SUBBASIN CHARACTERISTICS
 TAREA .04 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

.....	HYDRO-35	TP-40	TP-49					
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY

.74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .04

208 LS SCS LOSS RATE
STRTL .35 INITIAL ABSTRACTION
CRVNR 85.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

209 US SNYDER UNITGRAPH
TP .50 LAG
CP .68 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS

CLARK TC= .58 HR, R= .39 HR
SNYDER TP= .50 HR, CP= .67

UNIT HYDROGRAPH

29 END-OF-PERIOD ORDINATES

2. 8. 15. 23. 29. 32. 32. 28. 22. 18.
15. 12. 9. 8. 6. 5. 4. 3. 3. 2.
2. 1. 1. 1. 1. 1. 0. 0. 0.

*** *** *** *** ***

HYDROGRAPH AT STATION O1A

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.77, TOTAL EXCESS = 5.67

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
(CFS) (HR) 6-HR 24-HR 72-HR 59.92-HR
+ 70. 12.58 (CFS) 18. 6. 2. 2.
(INCHES) 4.570 5.648 5.648 5.648
(AC-FT) 9. 11. 11. 11.

CUMULATIVE AREA = .04 SQ MI

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* *
210 KK * O2 *
* *

OFFSITE AREA O2

212 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

213 BA SUBBASIN CHARACTERISTICS
TAREA 1.58 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
..... HYDRO-35 TP-40 TP-49
5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
.74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = 1.58

214 LS SCS LOSS RATE
STRTL .35 INITIAL ABSTRACTION
CRVNR 85.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

215 US SNYDER UNITGRAPH
TP .71 LAG
CP .58 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS

CLARK TC= .79 HR, R= .76 HR
SNYDER TP= .71 HR, CP= .58

UNIT HYDROGRAPH									
54 END-OF-PERIOD ORDINATES									
31.	115.	232.	367.	512.	648.	752.	817.	841.	808.
733.	657.	589.	528.	473.	424.	380.	341.	306.	274.
246.	220.	197.	177.	159.	142.	127.	114.	102.	92.
82.	74.	66.	59.	53.	48.	43.	38.	34.	31.
28.	25.	22.	20.	18.	16.	14.	13.	11.	10.
9.	8.	7.	7.						

*** *** *** *** ***

HYDROGRAPH AT STATION O2

TOTAL RAINFALL = 7.42, TOTAL LOSS = 1.77, TOTAL EXCESS = 5.66

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	59.92-HR	
+ 2171.	12.75	(CFS)	767.	239.	96.	96.
		(INCHES)	4.524	5.632	5.632	5.632
		(AC-FT)	380.	473.	473.	473.

CUMULATIVE AREA = 1.58 SQ MI

* *
216 KK * O3 *
* *

OFFSITE AREA O3

218 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPL0T	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
I0UT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.063	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

219 BA SUBBASIN CHARACTERISTICS

TAREA	.03	SUBBASIN AREA
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PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .03

220 LS SCS LOSS RATE

STRTL	.38	INITIAL ABSTRACTION
CRVNBR	84.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

221 US SNYDER UNITGRAPH

TP	.30	LAG
CP	.68	PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS

CLARK	TC= .35 HR,	R= .23 HR
SNYDER	TP= .30 HR,	CP= .68

UNIT HYDROGRAPH

18 END-OF-PERIOD ORDINATES									
5.	17.	30.	36.	32.	23.	16.	11.	8.	5.
4.	3.	2.	1.	1.	1.	0.	0.		

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HYDROGRAPH AT STATION O3

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	59.92-HR	
+ 62.	12.33	(CFS)	12.	4.	2.	2.

(INCHES) 4.500 5.539 5.539 5.539
 (AC-FT) 6. 7. 7. 7.
 CUMULATIVE AREA = .03 SQ MI

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 222 KK * S6 *
 * *

SUBAREA S6

224 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

225 BA SUBBASIN CHARACTERISTICS
 TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .02

226 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

227 US SNYDER UNITGRAPH
 TP .81 LAG
 CP .69 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS
 CLARK TC= .94 HR, R= .62 HR
 SNYDER TP= .81 HR, CP= .69

UNIT HYDROGRAPH
 46 END-OF-PERIOD ORDINATES
 0. 1. 3. 5. 6. 8. 10. 11. 12. 12.
 12. 11. 10. 8. 7. 6. 6. 5. 4. 4.
 3. 3. 2. 2. 2. 2. 1. 1. 1. 1.
 1. 1. 1. 1. 0. 0. 0. 0. 0. 0.
 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.

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HYDROGRAPH AT STATION S6

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
32.	12.83	10.	3.	1.	1.
		(INCHES) 4.475	5.534	5.534	5.534
		(AC-FT) 5.	6.	6.	6.

CUMULATIVE AREA = .02 SQ MI

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 * *
 228 KK * CS6 *
 * *

COMBINE AREAS DISCHARGING OFF OF P.B.

230 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

231 HC HYDROGRAPH COMBINATION
 ICOMP 5 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION CS6

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
+ 2664.	12.75	941.	305.	125.	125.
		(INCHES) 4.185	5.416	5.555	5.555
		(AC-FT) 467.	604.	620.	620.

CUMULATIVE AREA = 2.09 SQ MI

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 232 KK * 04 *
 * *

 OFFSITE AREA 04

234 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

235 BA SUBBASIN CHARACTERISTICS
 TAREA .13 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .13

236 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNER 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

237 US SNYDER UNITGRAPH
 TP .43 LAG
 CP .64 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS
 CLARK TC= .51 HR, R= .36 HR
 SNYDER TP= .43 HR, CP= .64

UNIT HYDROGRAPH
 27 END-OF-PERIOD ORDINATES

10.	36.	71.	105.	126.	131.	115.	92.	73.	58.
46.	37.	29.	23.	18.	15.	12.	9.	7.	6.
5.	4.	3.	2.	2.	1.	1.			

*** **

HYDROGRAPH AT STATION O4

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	59.92-HR	
269.	12.50	65.	20.	8.	8.	
		(INCHES)	4.491	5.534	5.534	5.534
		(AC-FT)	32.	40.	40.	40.

CUMULATIVE AREA = .13 SQ MI

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238 KK * CO4 *
* *

MIDWAY BRANCH DISCHARGING BACK ONTO P.B.

240 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

241 HC HYDROGRAPH COMBINATION

ICOMP	2	NUMBER OF HYDROGRAPHS TO COMBINE
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HYDROGRAPH AT STATION CO4

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	59.92-HR	
2881.	12.67	1006.	325.	133.	133.	
		(INCHES)	4.202	5.422	5.554	5.554
		(AC-FT)	499.	644.	659.	659.

CUMULATIVE AREA = 2.23 SQ MI

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242 KK * A6 *
* *

SUBAREA A6

244 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

245 BA SUBBASIN CHARACTERISTICS

TAREA	.02	SUBBASIN AREA
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PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .02

246 LS SCS LOSS RATE

STRTL	.33	INITIAL ABSTRACTION
CRVNBR	86.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

247 UK OVERLAND-FLOW ELEMENT NO. 1
 L 120. OVERLAND FLOW LENGTH
 S .2500 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

248 RD MUSKINGUM-CUNGE
 MAIN CHANNEL
 L 1314. CHANNEL LENGTH
 S .0020 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .02 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER
 Z 2.00 SIDE SLOPE
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS
 COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	2.13	1.67	.70	24.00	86.66	725.02	5.79	.61
MAIN	1.03	1.33	5.00	657.00	72.90	725.00	5.57	3.50

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .5311E+01 OUTFLOW= .5112E+01 BASIN STORAGE= .9760E-03 PERCENT ERROR= 3.7

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1.03 1.33 5.00 72.90 725.00 5.57

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HYDROGRAPH AT STATION A6

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (INCHES)	72-HR (AC-FT)	59.92-HR (CFS)
73.	12.08	9.	4.638	4.	1.
		9.	5.573	5.	1.
		4.638	5.573	5.	5.573
		4.	5.	5.	5.

CUMULATIVE AREA = .02 SQ MI

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 249 KK * S8 *
 * *

SUBAREA S8

251 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUV 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

252 BA SUBBASIN CHARACTERISTICS
 TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
 STORM AREA = .02

253 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNER 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

254 US SNYDER UNITGRAPH
 TP .31 LAG

CP .69 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS
CLARK TC= .37 HR, R= .24 HR
SNYDER TP= .31 HR, CP= .68

UNIT HYDROGRAPH
18 END-OF-PERIOD ORDINATES

3. 10. 18. 22. 20. 15. 10. 7. 5. 4.
2. 2. 1. 1. 1. 0. 0. 0. 0.

*** **

HYDROGRAPH AT STATION S8

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
39.	12.33	8.	2.	1.	1.
		(INCHES) 4.499	5.538	5.538	5.538
		(AC-FT) 4.	5.	5.	5.

CUMULATIVE AREA = .02 SQ MI

*** **

* *
255 KK * CS8 *
* *

MIDWAY BRANCH DISCHARGING OFF OF P.B.

257 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

258 HC HYDROGRAPH COMBINATION
ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION CS8

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
2919.	12.67	1022.	329.	135.	135.
		(INCHES) 4.207	5.424	5.554	5.554
		(AC-FT) 507.	653.	669.	669.

CUMULATIVE AREA = 2.26 SQ MI

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* *
259 KK * S1 *
* *

SUBAREA S1

261 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

262 BA SUBBASIN CHARACTERISTICS
TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
 STORM AREA = .02

263 LS SCS LOSS RATE
STRTL .38 INITIAL ABSTRACTION
CRVNBR 84.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

264 US SNYDER UNITGRAPH
TP .77 LAG
CP .70 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS

CLARK TC= .89 HR, R= .57 HR
SNYDER TP= .77 HR, CP= .69

UNIT HYDROGRAPH
42 END-OF-PERIOD ORDINATES

0.	1.	3.	4.	5.	7.	8.	9.	10.	10.
9.	8.	7.	6.	5.	4.	4.	3.	3.	2.
2.	2.	2.	1.	1.	1.	1.	1.	1.	1.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.								

*** **

HYDROGRAPH AT STATION S1

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	59.92-HR	
24.	12.83	8.	2.	1.	1.	
		(INCHES)	4.477	5.532	5.532	5.532
		(AC-FT)	4.	5.	5.	5.

CUMULATIVE AREA = .02 SQ MI

*** **

* *
265 KK * S2 *
* *

SUBAREA S2

267 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IFLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

268 BA SUBBASIN CHARACTERISTICS
TAREA .05 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
 STORM AREA = .05

269 LS SCS LOSS RATE
STRTL .38 INITIAL ABSTRACTION
CRVNBR 84.00 CURVE NUMBER

RTIMP .00 PERCENT IMPERVIOUS AREA
 270 US SNYDER UNITGRAPH
 TP 1.23 LAG
 CP .66 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS
 CLARK TC= 1.38 HR, R= 1.03 HR
 SNYDER TP= 1.23 HR, CP= .66

UNIT HYDROGRAPH
 75 END-OF-PERIOD ORDINATES

0.	1.	2.	4.	5.	7.	9.	10.	12.	14.
15.	16.	17.	17.	17.	17.	16.	15.	14.	13.
12.	11.	10.	9.	9.	8.	7.	7.	6.	6.
5.	5.	4.	4.	4.	3.	3.	3.	3.	3.
2.	2.	2.	2.	2.	2.	1.	1.	1.	1.
1.	1.	1.	1.	1.	1.	1.	1.	1.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

*** **

HYDROGRAPH AT STATION S2

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW 6-HR	24-HR	72-HR	59.92-HR
52.	13.25	23.	7.	3.	3.
		(INCHES)	4.418	5.533	5.533
		(AC-FT)	11.	14.	14.

CUMULATIVE AREA = .05 SQ MI

 * *
 271 KK * CH1 *
 * *

CHANNEL CH1

273 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPL0T	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

274 BA SUBBASIN CHARACTERISTICS
 TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .01

275 LS SCS LOSS RATE

STRTL	.38	INITIAL ABSTRACTION
CRVNR	84.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

276 UK OVERLAND-FLOW ELEMENT NO. 1

L	411.	OVERLAND FLOW LENGTH
S	.0050	SLOPE
N	.350	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

MUSKINGUM-CUNGE

277 RD MAIN CHANNEL

L	1283.	CHANNEL LENGTH
S	.0016	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.01	CONTRIBUTING AREA

SHAPE TRAP CHANNEL SHAPE
 WD 15.00 BOTTOM WIDTH OR DIAMETER
 Z 4.00 SIDE SLOPE
 RUPSTQ YES ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS
 COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	.30	1.67	3.98	45.67	17.56	741.79	5.55	.20
MAIN	.46	1.43	5.00	641.50	57.14	800.00	5.51	2.29

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1413E+02 EXCESS= .2757E+01 OUTFLOW= .1682E+02 BASIN STORAGE= .3597E-02 PERCENT ERROR= .4

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN .46 1.43 5.00 57.14 800.00 5.51

*** **

HYDROGRAPH AT STATION CH1

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	59.92-HR	
57.	13.33	27.	8.	3.	3.	
		(INCHES)	4.415	5.509	5.512	5.512
		(AC-FT)	13.	17.	17.	17.

CUMULATIVE AREA = .06 SQ MI

 * *
 278 KK * S3 *
 * *

SUBAREA S3

280 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IELOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUPT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .063 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

281 BA SUBBASIN CHARACTERISTICS
 TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .01

282 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNBR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

283 US SNYDER UNITGRAPH
 TP .35 LAG
 CP .72 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS
 CLARK TC= .45 HR, R= .23 HR
 SNYDER TP= .35 HR, CP= .72

UNIT HYDROGRAPH
 18 END-OF-PERIOD ORDINATES

1. 3. 6. 9. 9. 8. 6. 4. 3. 2.
 1. 1. 1. 0. 0. 0. 0. 0. 0.

*** **

HYDROGRAPH AT STATION S3

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	59.92-HR	
17.	12.42	3.	1.	0.	0.	
		(INCHES)	4.500	5.538	5.538	5.538
		(AC-FT)	2.	2.	2.	2.

CUMULATIVE AREA = .01 SQ MI

 * *
 284 KK * 05 *
 * *

OFFSITE AREA O5

286 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPILOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

287 BA SUBBASIN CHARACTERISTICS
 TAREA .18 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .18

288 LS SCS LOSS RATE

STRFL	.38	INITIAL ABSTRACTION
CRVNBR	84.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

289 US SNYDER UNITGRAPH

TP	.59	LAG
CP	.64	PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS
 CLARK TC= .67 HR, R= .52 HR
 SNYDER TP= .59 HR, CP= .64

UNIT HYDROGRAPH
 38 END-OF-PERIOD ORDINATES

7.	24.	48.	74.	100.	119.	129.	116.	99.
84.	72.	61.	52.	44.	38.	32.	27.	20.
17.	14.	12.	10.	9.	7.	6.	5.	4.
3.	3.	2.	2.	2.	1.	1.	1.	

*** **

HYDROGRAPH AT STATION O5

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
302.	12.67	88.	27.	11.	11.
		(INCHES)	4.481	5.533	5.533
		(AC-FT)	43.	54.	54.

CUMULATIVE AREA = .18 SQ MI

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* *
290 KK * CO5 *
* *

COMBINE WEST AREAS DISCHARGING TO ELM FORK

292 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

293 HC HYDROGRAPH COMBINATION
ICOMP 4 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION CO5

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	59.92-HR	
381.	12.67	126.	39.	16.	16.	
		(INCHES)	4.453	5.528	5.529	5.529
		(AC-FT)	62.	77.	77.	77.

CUMULATIVE AREA = .26 SQ MI

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* *
294 KK * CH2 *
* *

CHANNEL CH2

296 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

297 BA SUBBASIN CHARACTERISTICS
TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .01

298 LS SCS LOSS RATE
STRTL .38 INITIAL ABSTRACTION
CRVNR 84.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

299 UK OVERLAND-FLOW ELEMENT NO. 1
L 82. OVERLAND FLOW LENGTH
S .0122 SLOPE
N .350 ROUGHNESS COEFFICIENT
PA 100.0 PERCENT OF SUBBASIN
DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

300 RD MUSKINGUM-CUNGE
MAIN CHANNEL
L 1539. CHANNEL LENGTH
S .0016 SLOPE

N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .01 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 8.00 BOTTOM WIDTH OR DIAMETER
 Z 2.00 SIDE SLOPE
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)	DX (FT)				
PLANEL	.47	1.67	1.55	16.40	20.08	724.70	.19	
MAIN	.61	1.42	5.00	513.00	15.36	730.00	1.99	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .1512E+01 OUTFLOW= .1320E+01 BASIN STORAGE= .2050E-02 PERCENT ERROR= 12.5

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN .61 1.42 5.00 15.36 730.00 4.85

*** **

HYDROGRAPH AT STATION CH2

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	59.92-HR	
15.	12.17	2.	1.	0.	0.	
		(INCHES)	4.118	4.852	4.854	4.854
		(AC-FT)	1.	1.	1.	1.

CUMULATIVE AREA = .01 SQ MI

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 * *
 301 KK * A12 *
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SUBAREA A12

303 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

304 BA SUBBASIN CHARACTERISTICS
 TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .02

305 LS SCS LOSS RATE
 STRTL .33 INITIAL ABSTRACTION
 CRVNR 86.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

306 UK OVERLAND-FLOW ELEMENT NO. 1
 L 120. OVERLAND FLOW LENGTH
 S .2500 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

307 RD MUSKINGUM-CUNGE
 MAIN CHANNEL
 L 559. CHANNEL LENGTH
 S .0050 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT

CA .02 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER
 Z 2.00 SIDE SLOPE
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELERITY
		M	DT				
			(MIN)	(FT)	(CFS)	(MIN)	(IN)
PLANE1	2.13	1.67	.70	24.00	119.41	725.02	.61
MAIN	1.63	1.33	1.74	559.00	114.14	725.10	5.35

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .7317E+01 OUTFLOW= .6340E+01 BASIN STORAGE= .3260E-03 PERCENT ERROR= 13.4

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1.63 1.33 5.00 113.71 725.00 5.03

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HYDROGRAPH AT STATION A12

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	59.92-HR	
+ 114.	12.08	11.	3.	1.	1.	
		(INCHES)	4.308	5.032	5.033	5.033
		(AC-FT)	5.	6.	6.	6.

CUMULATIVE AREA = .02 SQ MI

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 308 KK * CA12 *
 * *

COMBINE CH2 AND A12

310 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

311 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION CA12

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	59.92-HR	
+ 126.	12.08	13.	4.	2.	2.	
		(INCHES)	4.273	5.000	5.001	5.001
		(AC-FT)	7.	8.	8.	8.

CUMULATIVE AREA = .03 SQ MI

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 * *
 312 KK * CH3 *
 * *

CHANNEL CH3

314 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

315 BA SUBBASIN CHARACTERISTICS
 TAREA .00 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
 STORM AREA = .00

316 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

317 UK OVERLAND-FLOW ELEMENT NO. 1
 L 92. OVERLAND FLOW LENGTH
 S .0435 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

318 RD MUSKINGUM-CUNGE
 MAIN CHANNEL
 L 840. CHANNEL LENGTH
 S .0012 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 10.00 BOTTOM WIDTH OR DIAMETER
 Z 2.00 SIDE SLOPE
 RUPSTQ YES ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)	DX (FT)				
PLANE1	.89	1.67	1.14	18.40	18.94	725.03	.31	
MAIN	.47	1.44	4.39	840.00	111.02	728.70	3.19	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .7682E+01 EXCESS= .1245E+01 OUTFLOW= .8789E+01 BASIN STORAGE= .1382E-02 PERCENT ERROR= 1.5

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN .47 1.44 5.00 106.75 730.00 4.99

*** **

HYDROGRAPH AT STATION CH3

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	
107.	12.17	15.	4.	2.	
		(INCHES)	4.266	4.989	4.990
		(AC-FT)	8.	9.	9.

CUMULATIVE AREA = .03 SQ MI

*** **

319 KK

 * *
 * A11 *
 * *

SUBAREA A11

321 KO OUTPUT CONTROL VARIABLES


```

IPRNT      3 PRINT CONTROL
IPLOT      0 PLOT CONTROL
QSCAL      0. HYDROGRAPH PLOT SCALE
IFNCH      7 PUNCH COMPUTED HYDROGRAPH
IOUT       21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1      1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2      720 LAST ORDINATE PUNCHED OR SAVED
TIMINT     .083 TIME INTERVAL IN HOURS

```

SUBBASIN RUNOFF DATA

```

322 BA SUBBASIN CHARACTERISTICS
TAREA .03 SUBBASIN AREA

```

PRECIPITATION DATA

```

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
..... HYDRO-35 ..... TP-40 ..... TP-49 .....
5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
.74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
STORM AREA = .03

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323 LS SCS LOSS RATE
STRTL .33 INITIAL ABSTRACTION
CRVNBR 86.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

```

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324 UK KINEMATIC WAVE
OVERLAND-FLOW ELEMENT NO. 1
L 120. OVERLAND FLOW LENGTH
S .2500 SLOPE
N .350 ROUGHNESS COEFFICIENT
PA 100.0 PERCENT OF SUBBASIN
DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

```

```

325 RD MUSKINGUM-CUNGE
MAIN CHANNEL
L 842. CHANNEL LENGTH
S .0050 SLOPE
N .030 CHANNEL ROUGHNESS COEFFICIENT
CA .03 CONTRIBUTING AREA
SHAPE TRAP CHANNEL SHAPE
WD .00 BOTTOM WIDTH OR DIAMETER
Z 2.00 SIDE SLOPE
RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

```

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)	DX (FT)				
PLANE1	2.13	1.67	.70	24.00	173.83	725.02	.61	
MAIN	1.63	1.33	2.39	421.00	164.16	724.07	5.87	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .1065E+02 OUTFLOW= .1038E+02 BASIN STORAGE= .4782E-03 PERCENT ERROR= 2.5

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

```

MAIN 1.63 1.33 5.00 157.65 725.00 5.64

```

*** **

HYDROGRAPH AT STATION A11

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
158.	12.08	17.	5.	2.	2.
		(INCHES) 4.643	5.637	5.638	5.638
		(AC-FT) 9.	10.	10.	10.

CUMULATIVE AREA = .03 SQ MI

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* *
326 KK * CALL *
* *
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COMBINE WITH CH3 AND A11

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328 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL

```

I PLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

329 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION CA11

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
261.	12.08	32.	10.	4.	4.
		(INCHES) 4.458	5.320	5.321	5.321
		(AC-FT) 16.	19.	19.	19.

CUMULATIVE AREA = .07 SQ MI

*** **

 * *
 330 KK * CH4 *
 * *

CHANNEL CH4

332 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 I PLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

333 BA SUBBASIN CHARACTERISTICS
 TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .01

334 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNBR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

335 UK OVERLAND-FLOW ELEMENT NO. 1
 L 101. OVERLAND FLOW LENGTH
 S .0792 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

336 RD MUSKINGUM-CUNGE
 MAIN CHANNEL
 L 1180. CHANNEL LENGTH
 S .0025 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .01 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 10.00 BOTTOM WIDTH OR DIAMETER
 Z 2.00 SIDE SLOPE
 RUPSTQ YES ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	M	COMPUTATION TIME STEP		PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
			DT (MIN)	DX (FT)				
PLANE1	1.20	1.67	.99	20.20	31.93	724.55	5.56	.38

MAIN .68 1.44 3.86 1180.00 260.55 728.77 5.29 5.10

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1916E+02 EXCESS= .2075E+01 OUTFLOW= .2103E+02 BASIN STORAGE= .1474E-02 PERCENT ERROR= .9

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN .68 1.44 5.00 250.54 730.00 5.30

*** *** *** *** ***

HYDROGRAPH AT STATION CH4

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
251.	12.17	36.	11.	4.	4.
		4.452 (INCHES)	5.300	5.301	5.301
		18. (AC-FT)	21.	21.	21.

CUMULATIVE AREA = .07 SQ MI

*** **

337 KK A10T

SUBAREA A10T

339 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPL0T	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

340 BA SUBBASIN CHARACTERISTICS
TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .02

341 LS SCS LOSS RATE

STRFL	.38	INITIAL ABSTRACTION
CRVNR	84.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

342 UK OVERLAND-FLOW ELEMENT NO. 1

L	265.	OVERLAND FLOW LENGTH
S	.0400	SLOPE
N	.350	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

343 RD MUSKINGUM-CUNGE MAIN CHANNEL

L	772.	CHANNEL LENGTH
S	.0050	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.02	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	.00	BOTTOM WIDTH OR DIAMETER
Z	2.00	SIDE SLOPE
RUPSTQ	NO	ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS
COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	.85	1.67	2.24	53.00	64.44	727.52	5.55	.40
MAIN	1.63	1.33	2.81	386.00	62.64	729.38	5.46	4.59

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .5722E+01 OUTFLOW= .5617E+01 BASIN STORAGE= .7387E-03 PERCENT ERROR= 1.8

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

	MAIN	1.63	1.33	5.00	61.97	730.00	5.45
***	***	***	***	***	***		
	HYDROGRAPH AT STATION		A10T				
	TOTAL RAINFALL =	7.44,	TOTAL LOSS =	1.88,	TOTAL EXCESS =	5.56	
PEAK FLOW	TIME		6-HR	24-HR	72-HR	59.92-HR	
+	(CFS)	(HR)	(CFS)				
+	62.	12.17	9.	3.	1.	1.	
			(INCHES)	4.488	5.450	5.455	5.455
			(AC-FT)	5.	6.	6.	6.
	CUMULATIVE AREA =		.02 SQ MI				

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 344 KK * A10S *
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SUBAREA A10S

346 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLPT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

347 BA SUBBASIN CHARACTERISTICS

TAREA	.03	SUBBASIN AREA
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PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

.....	HYDRO-35	TP-40	TP-49			
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .03

348 LS SCS LOSS RATE

STRTL	.33	INITIAL ABSTRACTION
CRVNBR	86.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

349 UK OVERLAND-FLOW ELEMENT NO. 1

L	120.	OVERLAND FLOW LENGTH
S	.2500	SLOPE
N	.350	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

350 RD MUSKINGUM-CUNGE MAIN CHANNEL

L	764.	CHANNEL LENGTH
S	.0050	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.03	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	.00	BOTTOM WIDTH OR DIAMETER
Z	2.00	SIDE SLOPE
RUPSTQ	NO	ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS

	COMPUTATION TIME STEP							
ELEMENT	ALPHA	M	DT	DX	PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELERITY
			(MIN)	(FT)	(CFS)	(MIN)	(IN)	(FPS)
PLANE1	2.13	1.67	.70	24.00	130.50	725.02	5.79	.61
MAIN	1.63	1.33	2.33	382.00	126.55	724.58	5.65	5.47

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .7997E+01 OUTFLOW= .7801E+01 BASIN STORAGE= .4245E-03 PERCENT ERROR= 2.4

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

```

MAIN          1.63    1.33    5.00          122.75    725.00    5.65
***          ***          ***          ***          ***
HYDROGRAPH AT STATION  A10S
TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79
PEAK FLOW      TIME          MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)          6-HR      24-HR      72-HR      59.92-HR
+ 123.         12.08          (CFS)
                (INCHES)  4.659    4.        2.        2.
                (AC-FT)   6.       5.654    8.        5.655   5.655
                (AC-FT)   6.       8.        8.        8.
CUMULATIVE AREA = .03 SQ MI

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*      *
351 KK *    CA10 *
*      *
*****

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COMBINE A10 SUBAREAS

```

353 KO  OUTPUT CONTROL VARIABLES
        IPRNT      3  PRINT CONTROL
        IPLOT      0  PLOT CONTROL
        QSCAL      0. HYDROGRAPH PLOT SCALE
        IPNCH      7  PUNCH COMPUTED HYDROGRAPH
        IOUT       21 SAVE HYDROGRAPH ON THIS UNIT
        ISAV1      1  FIRST ORDINATE PUNCHED OR SAVED
        ISAV2     720 LAST ORDINATE PUNCHED OR SAVED
        TIMINT     .083 TIME INTERVAL IN HOURS

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354 HC  HYDROGRAPH COMBINATION
        ICOMP      2  NUMBER OF HYDROGRAPHS TO COMBINE

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*** *** *** *** ***

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HYDROGRAPH AT STATION  CA10
PEAK FLOW      TIME          MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)          6-HR      24-HR      72-HR      59.92-HR
+ 180.         12.08          (CFS)
                (INCHES)  4.582    7.        3.        3.
                (AC-FT)   11.      5.567    13.      5.569   5.569
                (AC-FT)   11.      13.     13.     13.
CUMULATIVE AREA = .05 SQ MI

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*****
*      *
355 KK *    A9 *
*      *
*****

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SUBAREA A9

```

357 KO  OUTPUT CONTROL VARIABLES
        IPRNT      3  PRINT CONTROL
        IPLOT      0  PLOT CONTROL
        QSCAL      0. HYDROGRAPH PLOT SCALE
        IPNCH      7  PUNCH COMPUTED HYDROGRAPH
        IOUT       21 SAVE HYDROGRAPH ON THIS UNIT
        ISAV1      1  FIRST ORDINATE PUNCHED OR SAVED
        ISAV2     720 LAST ORDINATE PUNCHED OR SAVED
        TIMINT     .083 TIME INTERVAL IN HOURS

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SUBBASIN RUNOFF DATA

```

358 BA  SUBBASIN CHARACTERISTICS
        TAREA      .02  SUBBASIN AREA

```

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .02

359 LS SCS LOSS RATE
 STRTL .33 INITIAL ABSTRACTION
 CRVNR 86.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

360 UK KINEMATIC WAVE
 OVERLAND-FLOW ELEMENT NO. 1
 L 120. OVERLAND FLOW LENGTH
 S .2500 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

361 RD MUSKINGUM-CUNGE
 MAIN CHANNEL
 L 399. CHANNEL LENGTH
 S .0050 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .02 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER
 Z 2.00 SIDE SLOPE
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)				
PLANE1	2.13	1.67	.70	24.00	110.33	725.02	5.79
MAIN	1.63	1.33	1.27	399.00	106.95	724.60	5.08

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .6762E+01 OUTFLOW= .5937E+01 BASIN STORAGE= .2341E-03 PERCENT ERROR= 12.2

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1.63 1.33 5.00 104.68 725.00 5.10

*** **

HYDROGRAPH AT STATION A9

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	59.92-HR	
105.	12.08	10.	3.	1.	1.	
		(INCHES)	4.361	5.095	5.096	5.096
		(AC-FT)	5.	6.	6.	6.

CUMULATIVE AREA = .02 SQ MI

*** **

 * *
 362 KK * P2 *
 * *

DETENTION POND P2

364 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .063 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

365 BA SUBBASIN CHARACTERISTICS
 TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .02

366 LS SCS LOSS RATE
 STRTL .00 INITIAL ABSTRACTION
 CRVNER 100.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

367 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .00 LAG

UNIT HYDROGRAPH
 5 END-OF-PERIOD ORDINATES
 113. 32. 6. 1. 0.

*** **

HYDROGRAPH AT STATION P2

TOTAL RAINFALL = 7.44, TOTAL LOSS = .00, TOTAL EXCESS = 7.44

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
		(CFS)			
+ 101.	12.08	12.	4.	2.	2.
		(INCHES)	5.468	7.437	7.440
		(AC-FT)	6.	8.	8.

CUMULATIVE AREA = .02 SQ MI

*** **

 * *
 368 KK * P2-IN *
 * *

COMBINE AREAS DISCHARGING TO POND P2

370 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPILOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

371 HC HYDROGRAPH COMBINATION
 ICOMP 4 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION P2-IN

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
		(CFS)			
+ 616.	12.08	80.	24.	10.	10.
		(INCHES)	4.590	5.594	5.608
		(AC-FT)	39.	48.	48.

CUMULATIVE AREA = .16 SQ MI

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 372 KK * RP2 *
 * *

ROUTE THROUGH POND P2

374 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPILOT 0 PLOT CONTROL

QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

HYDROGRAPH ROUTING DATA

375 RS STORAGE ROUTING
 NSTPS 1 NUMBER OF SUBREACHES
 ITYP ELEV TYPE OF INITIAL CONDITION
 RSVRIC 454.00 INITIAL CONDITION
 X .00 WORKING R AND D COEFFICIENT

376 SA AREA .0 4.4 6.8 8.3 8.4 8.5 8.6 8.9 9.1

377 SE ELEVATION 454.00 454.50 455.00 455.50 456.00 456.50 457.00 458.00 459.00

379 SL LOW-LEVEL OUTLET
 ELEV 456.00 ELEVATION AT CENTER OF OUTLET
 CAREA 14.14 CROSS-SECTIONAL AREA
 COQL .80 COEFFICIENT
 EXPL .50 EXPONENT OF HEAD

378 SS SPILLWAY
 CREL 458.00 SPILLWAY CREST ELEVATION
 SPWID 25.00 SPILLWAY WIDTH
 COQW 2.60 WEIR COEFFICIENT
 EXPW 1.50 EXPONENT OF HEAD

COMPUTED STORAGE-ELEVATION DATA

STORAGE	.00	.74	3.53	7.28	11.44	15.66	19.94	28.69	37.69
ELEVATION	454.00	454.50	455.00	455.50	456.00	456.50	457.00	458.00	459.00

COMPUTED OUTFLOW-ELEVATION DATA

OUTFLOW	.00	.00	122.28	123.10	123.94	124.78	125.64	126.50	127.38	128.27
ELEVATION	454.00	456.00	457.82	457.84	457.87	457.89	457.92	457.95	457.97	458.00
OUTFLOW	137.24	141.43	146.68	153.10	160.79	169.87	180.43	192.58	206.44	222.10
ELEVATION	458.16	458.21	458.28	458.36	458.44	458.54	458.64	458.75	458.87	459.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	.74	3.53	7.28	11.44	15.66	19.94	27.08	27.29	27.51
OUTFLOW	.00	.00	.00	.00	.00	64.14	90.70	122.28	123.10	123.94
ELEVATION	454.00	454.50	455.00	455.50	456.00	456.50	457.00	457.82	457.84	457.87
STORAGE	27.74	27.97	28.20	28.44	28.69	30.08	30.60	31.19	31.87	32.63
OUTFLOW	124.78	125.64	126.50	127.38	128.27	137.24	141.43	146.68	153.10	160.79
ELEVATION	457.89	457.92	457.95	457.97	458.00	458.16	458.21	458.28	458.36	458.44
STORAGE	33.47	34.40	35.41	36.51	37.69					
OUTFLOW	169.87	180.43	192.58	206.44	222.10					
ELEVATION	458.54	458.64	458.75	458.87	459.00					

*** *** *** *** ***

HYDROGRAPH AT STATION RP2

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	59.92-HR
+ (CFS)	(HR)	(CFS)				
+ 118.	12.75	64.	19.	7.	7.	
		(INCHES)	3.717	4.277	4.277	4.277
		(AC-FT)	32.	37.	37.	37.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
			6-HR	24-HR	72-HR	59.92-HR
+ (AC-FT)	(HR)					
+ 26.	12.75	18.	13.	10.	10.	
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
			6-HR	24-HR	72-HR	59.92-HR
+ (FEET)	(HR)					
+ 457.72	12.75	456.73	456.20	455.78	455.78	

CUMULATIVE AREA = .16 SQ MI

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 380 KK CH5 *
 * *

CHANNEL CH5

382 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH FLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

383 BA SUBBASIN CHARACTERISTICS
 TAREA .00 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
 STORM AREA = .00

384 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

385 UK OVERLAND-FLOW ELEMENT NO. 1
 L 197. OVERLAND FLOW LENGTH
 S .0051 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

386 RD MUSKINGUM-CUNGE
 MAIN CHANNEL
 L 155. CHANNEL LENGTH
 S .0050 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 20.00 BOTTOM WIDTH OR DIAMETER
 Z 2.00 SIDE SLOPE
 RUPSTQ YES ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELERITY
		M	DT DX				
PLANE1	.30	1.67	3.83 39.40	3.15	735.42	5.55	.17
MAIN	.65	1.51	.58 155.00	119.57	765.36	4.28	4.46

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3677E+02 EXCESS= .3558E+00 OUTFLOW= .3709E+02 BASIN STORAGE= .2947E-03 PERCENT ERROR= .1

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN .65 1.51 5.00 119.56 765.00 4.28

*** **

HYDROGRAPH AT STATION CH5

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
+ 120.	12.75	(CFS)			
		65.	19.	7.	7.
		{INCHES}	3.719	4.282	4.283
		(AC-FT)	32.	37.	37.

CUMULATIVE AREA = .16 SQ MI

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387 KK *****
 * *
 * A7T *
 * *

SUBAREA A7T

389 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

390 BA SUBBASIN CHARACTERISTICS
 TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TF-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .02

391 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

392 UK OVERLAND-FLOW ELEMENT NO. 1
 L 312. OVERLAND FLOW LENGTH
 S .0400 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

MUSKINGUM-CUNGE

393 RD MAIN CHANNEL
 L 1133. CHANNEL LENGTH
 S .0050 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .02 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER
 Z 2.00 SIDE SLOPE
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)	DX (FT)				
PLANE1	.85	1.67	2.54	62.40	67.33	728.32	.42	
MAIN	1.63	1.33	4.08	566.50	66.56	730.43	4.63	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .6285E+01 OUTFLOW= .6162E+01 BASIN STORAGE= .1163E-02 PERCENT ERROR= 1.9

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1.63 1.33 5.00 66.14 730.00 5.45

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HYDROGRAPH AT STATION A7T

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW {CFS}	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
+ 66.	12.17	{CFS}	10.	3.	1.
		(INCHES)	4.491	5.448	5.454
		(AC-FT)	5.	6.	6.

CUMULATIVE AREA = .02 SQ MI

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394 KK *****
 * *
 * A7S *
 * *

SUBAREA A7S

396 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

397 BA SUBBASIN CHARACTERISTICS
 TAREA .03 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .03

398 LS SCS LOSS RATE
 STRTL .33 INITIAL ABSTRACTION
 CRVNR 86.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

399 UK OVERLAND-FLOW ELEMENT NO. 1
 L 120. OVERLAND FLOW LENGTH
 S .2500 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

MUSKINGUM-CUNGE

400 RD MAIN CHANNEL
 L 1094. CHANNEL LENGTH
 S .0050 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .03 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER
 Z 2.00 SIDE SLOPE
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELERITY
		M	DT				
		(MIN)	(FT)	(CFS)	(MIN)	(IN)	(FPS)
PLANE1	2.13	1.67	.70	24.00	160.22	725.02	5.79
MAIN	1.63	1.33	3.17	547.00	147.31	725.68	5.63

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .9818E+01 OUTFLOW= .9550E+01 BASIN STORAGE= .6044E-03 PERCENT ERROR= 2.7

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1.63 1.33 5.00 143.97 725.00 5.64

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HYDROGRAPH AT STATION A7S

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
(CFS)	(HR)	(CFS)	(CFS)	(CFS)	(CFS)
+ 144.	12.08	16.	5.	2.	2.
		(INCHES)	4.654	5.639	5.639
		(AC-FT)	8.	10.	10.

CUMULATIVE AREA = .03 SQ MI

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401 KK *****
 * *
 * CA7 *
 * *

COMBINE A7 SUBAREAS

403 KO OUTPUT CONTROL VARIABLES

IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

404 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** *** *** *** ***

HYDROGRAPH AT STATION CA7

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	59.92-HR	
201.	12.08	26.	8.	3.	3.	
		(INCHES)	4.584	5.562	5.565	5.565
		(AC-FT)	13.	16.	16.	16.

CUMULATIVE AREA = .05 SQ MI

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 405 KK * A8 *
 * *

SUBAREA A8

407 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

408 BA SUBBASIN CHARACTERISTICS
 TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

12 FH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .02

409 LS SCS LOSS RATE
 STRTL .33 INITIAL ABSTRACTION
 CRVNR 86.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

410 UK OVERLAND-FLOW ELEMENT NO. 1
 L 120. OVERLAND FLOW LENGTH
 S .2500 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

MUSKINGUM-CUNGE

411 RD MAIN CHANNEL
 L 399. CHANNEL LENGTH
 S .0050 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .02 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER
 Z 2.00 SIDE SLOPE
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS
 COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT	DX	PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELERITY
			(MIN)	(FT)	(CFS)	(MIN)	(IN)	(FPS)

PLANE1	2.13	1.67	.70	24.00	84.63	725.03	5.79	.61
MAIN	1.63	1.33	1.36	399.00	80.42	724.17	5.06	4.90

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .5187E+01 OUTFLOW= .4535E+01 BASIN STORAGE= .2273E-03 PERCENT ERROR= 12.6

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	1.63	1.33	5.00	79.62	725.00	5.07
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HYDROGRAPH AT STATION A8

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
80.	12.08	8.	2.	1.	1.
		(INCHES) 4.333	5.066	5.067	5.067
		(AC-FT) 4.	5.	5.	5.

CUMULATIVE AREA = .02 SQ MI

412 KK * P3 *

DETENTION POND P3

414 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPL0T	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

415 BA SUBBASIN CHARACTERISTICS

TAREA	.02	SUBBASIN AREA
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PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

.....	HYDRO-35	TP-40	TP-49					
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .02

416 LS SCS LOSS RATE

STRTL	.00	INITIAL ABSTRACTION
CRVNR	100.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

417 UD SCS DIMENSIONLESS UNITGRAPH

TLAG	.00	LAG
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UNIT HYDROGRAPH
5 END-OF-PERIOD ORDINATES

97.	27.	5.	1.	0.
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HYDROGRAPH AT STATION P3

TOTAL RAINFALL = 7.44, TOTAL LOSS = .00, TOTAL EXCESS = 7.44

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
87.	12.08	10.	3.	1.	1.
		(INCHES) 5.468	7.437	7.440	7.440
		(AC-FT) 5.	7.	7.	7.

CUMULATIVE AREA = .02 SQ MI

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418 KK * P3-IN *
* *

COMBINE AREAS DISCHARGING TO POND P3

420 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

421 HC HYDROGRAPH COMBINATION
ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION P3-IN

PEAK FLOW (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	59.92-HR
+	368.	12.08	44.	14.	5.	5.
		(INCHES)	4.691	5.811	5.832	5.832
		(AC-FT)	22.	27.	27.	27.

CUMULATIVE AREA = .09 SQ MI

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422 KK * RP3 *
* *

ROUTE THROUGH POND P3

424 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

HYDROGRAPH ROUTING DATA

425 RS STORAGE ROUTING
NSFPS 1 NUMBER OF SUBREACHES
ITYP ELEV TYPE OF INITIAL CONDITION
RSVRIC 453.00 INITIAL CONDITION
X .00 WORKING R AND D COEFFICIENT

426 SA AREA .0 5.4 7.8 8.0 8.2 8.4 8.6

427 SE ELEVATION 453.00 454.00 455.00 456.00 457.00 458.00 459.00

429 SL LOW-LEVEL OUTLET
ELEVEL 454.50 ELEVATION AT CENTER OF OUTLET
CAREA 7.07 CROSS-SECTIONAL AREA
COQL .80 COEFFICIENT
EXPL .50 EXPONENT OF HEAD

428 SS SPILLWAY
CREL 458.00 SPILLWAY CREST ELEVATION
SEWID 25.00 SPILLWAY WIDTH
COQW 2.60 WEIR COEFFICIENT
EXPW 1.50 EXPONENT OF HEAD

COMPUTED STORAGE-ELEVATION DATA

STORAGE	.00	1.79	8.31	16.18	24.24	32.50	40.96
ELEVATION	453.00	454.00	455.00	456.00	457.00	458.00	459.00

COMPUTED OUTFLOW-ELEVATION DATA

OUTFLOW	.00	.00	53.75	56.72	60.04	63.77	67.99	72.81	78.37	84.85
ELEVATION	453.00	454.50	455.90	456.06	456.25	456.48	456.75	457.08	457.49	458.00
OUTFLOW	86.01	87.68	90.42	94.49	100.15	107.65	117.25	129.21	143.78	161.21
ELEVATION	458.04	458.09	458.15	458.23	458.32	458.42	458.54	458.68	458.83	459.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	1.79	4.75	8.31	15.42	16.18	16.69	18.20	20.00	22.19
OUTFLOW	.00	.00	.00	32.07	53.75	55.55	56.72	60.04	63.77	67.99
ELEVATION	453.00	454.00	454.50	455.00	455.90	456.00	456.06	456.25	456.48	456.75
STORAGE	24.24	24.87	28.23	32.50	32.88	33.25	33.75	34.39	35.15	36.05
OUTFLOW	71.71	72.81	78.37	84.85	86.01	87.68	90.42	94.49	100.15	107.65
ELEVATION	457.00	457.08	457.49	458.00	458.04	458.09	458.15	458.23	458.32	458.42
STORAGE	37.07	38.23	39.53	40.96						
OUTFLOW	117.25	129.21	143.78	161.21						
ELEVATION	458.54	458.68	458.83	459.00						

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HYDROGRAPH AT STATION RP3

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
(CFS)	(HR)	(CFS)	(INCHES)	(AC-FT)	
+	53.	12.92	37.	11.	4.
			3.954	4.804	4.805
			18.	22.	22.
PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	59.92-HR
(AC-FT)	(HR)				
+	15.	12.92	11.	6.	5.
PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	59.92-HR
(FEET)	(HR)				
+	455.87	12.92	455.29	454.73	454.38

CUMULATIVE AREA = .09 SQ MI

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430 KK * CH6 *
* *

CHANNEL CH6

432 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	720	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

433 BA SUBBASIN CHARACTERISTICS

TAREA	.00	SUBBASIN AREA
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PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .00

434 LS SCS LOSS RATE

STRTL	.38	INITIAL ABSTRACTION
CRVNBR	84.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

435 UK KINEMATIC WAVE OVERLAND-FLOW ELEMENT NO. 1

L	50.	OVERLAND FLOW LENGTH
S	.1000	SLOPE
N	.350	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

436 RD MUSKINGUM-CUNGE
 MAIN CHANNEL
 L 155. CHANNEL LENGTH
 S .0050 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 20.00 BOTTOM WIDTH OR DIAMETER
 Z 2.00 SIDE SLOPE
 RUPSTQ YES ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (F/S)
		M	DT (MIN)				
PLANE1	1.35	1.67	.60	10.00	6.48	724.83	5.56
MAIN	.65	1.51	.76	155.00	53.61	770.47	4.81

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2219E+02 EXCESS= .3854E+00 OUTFLOW= .2253E+02 BASIN STORAGE= .2239E-03 PERCENT ERROR= .2

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

 MAIN .65 1.51 5.00 53.61 770.00 4.81

HYDROGRAPH AT STATION CCH6

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR (CFS)	24-HR (CFS)	72-HR (CFS)	59.92-HR (CFS)
54.	12.83	37.	11.	5.	5.
		(INCHES) 3.950	4.806	4.808	4.808
		(AC-FT) 19.	23.	23.	23.

CUMULATIVE AREA = .09 SQ MI

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 * *
 437 KK * CCH6 *
 * *

COMBINE AREAS UPSTREAM OF S8

439 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

440 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION CCH6

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR (CFS)	24-HR (CFS)	72-HR (CFS)	59.92-HR (CFS)
173.	12.75	102.	30.	12.	12.
		(INCHES) 3.799	4.466	4.467	4.467
		(AC-FT) 51.	60.	60.	60.

CUMULATIVE AREA = .25 SQ MI

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441 KK * S9 *
* *

SUBAREA S9

443 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

444 BA SUBBASIN CHARACTERISTICS
TAREA .04 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
..... HYDRO-35 TP-40 TP-49
5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
.74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .04

445 LS SCS LOSS RATE
STRTL .38 INITIAL ABSTRACTION
CRVNBR 84.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

446 US SNYDER UNITGRAPH
TP .37 LAG
CP .68 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS
CLARK TC= .45 HR, R= .28 HR
SNYDER TP= .37 HR, CP= .68

UNIT HYDROGRAPH
21 END-OF-PERIOD ORDINATES
4. 14. 28. 38. 42. 38. 29. 21. 16. 12.
9. 6. 5. 4. 3. 2. 1. 1. 1. 1.
0.

*** **

HYDROGRAPH AT STATION S9

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	59.92-HR
80.	12.42	17.	5.	2.	2.
		(INCHES) 4.495	5.534	5.534	5.534
		(AC-FT) 9.	10.	10.	10.

CUMULATIVE AREA = .04 SQ MI

* *
447 KK * S10 *
* *

SUBAREA S10

449 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

450 BA SUBBASIN CHARACTERISTICS
TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

12 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .02

451 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

452 US SNYDER UNITGRAPH
 TP .27 LAG
 CP .68 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS
 CLARK TC= .34 HR, R= .20 HR
 SNYDER TP= .27 HR, CP= .68

UNIT HYDROGRAPH
 15 END-OF-PERIOD ORDINATES
 4. 13. 23. 26. 22. 14. 9. 6. 4. 3.
 2. 1. 1. 1. 0.

*** **

HYDROGRAPH AT STATION S10

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	59.92-HR
+	44.	12.33			
		(CFS)			
		8.	2.	1.	1.
		(INCHES)	4.495	5.532	5.532
		(AC-FT)	4.	5.	5.

CUMULATIVE AREA = .02 SQ MI

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 * *
 453 KK * CS9 *
 * *

COMBINE AREAS DISCHARGING SOUTH OFF OF P.B.

455 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 720 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

456 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION CS9

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	59.92-HR
+	286.	12.42			
		(CFS)			
		126.	38.	15.	15.
		(INCHES)	3.865	4.649	4.651
		(AC-FT)	62.	75.	75.

CUMULATIVE AREA = .30 SQ MI

1

RUNOFF SUMMARY
 FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS, AREA IN SQUARE MILES

PEAK TIME OF AVERAGE FLOW FOR MAXIMUM PERIOD BASIN MAXIMUM TIME OF

	OPERATION	STATION	FLOW	PEAK	6-HOUR	24-HOUR	72-HOUR	AREA	STAGE	MAX STAGE
+	HYDROGRAPH AT									
+		O1	298.	12.42	70.	22.	9.	.14		
+	HYDROGRAPH AT	S4	94.	12.92	33.	10.	4.	.07		
+	2 COMBINED AT	CS4	364.	12.50	102.	32.	13.	.20		
+	HYDROGRAPH AT	A1T	27.	12.17	4.	1.	1.	.01		
+	HYDROGRAPH AT	A1S	131.	12.08	14.	4.	2.	.03		
+	2 COMBINED AT	CA1	156.	12.08	19.	6.	2.	.04		
+	HYDROGRAPH AT	CH14	7.	12.08	1.	0.	0.	.00		
+	2 COMBINED AT	CCH14	163.	12.08	19.	6.	2.	.04		
+	HYDROGRAPH AT	A2T	57.	12.17	9.	3.	1.	.02		
+	HYDROGRAPH AT	A2S	144.	12.08	16.	5.	2.	.03		
+	2 COMBINED AT	CA2	195.	12.08	25.	8.	3.	.05		
+	HYDROGRAPH AT	CH12	4.	12.08	0.	0.	0.	.00		
+	HYDROGRAPH AT	CH13	9.	12.08	1.	0.	0.	.00		
+	3 COMBINED AT	CCH13	208.	12.08	26.	8.	3.	.05		
+	HYDROGRAPH AT	A3	61.	12.08	6.	2.	1.	.01		
+	HYDROGRAPH AT	CH10	6.	12.08	1.	0.	0.	.00		
+	HYDROGRAPH AT	CH11	4.	12.08	0.	0.	0.	.00		
+	3 COMBINED AT	CCH11	72.	12.08	7.	2.	1.	.01		
+	3 COMBINED AT	CA3	443.	12.08	53.	16.	6.	.11		
+	HYDROGRAPH AT	CH7	17.	12.08	2.	1.	0.	.00		
+	HYDROGRAPH AT	A5	134.	12.08	15.	4.	2.	.03		
+	2 COMBINED AT	CA5	150.	12.08	17.	5.	2.	.03		
+	HYDROGRAPH AT	CH8	166.	12.08	19.	6.	2.	.04		
+	HYDROGRAPH AT	A4	100.	12.08	10.	3.	1.	.02		
+	2 COMBINED AT	CA4	267.	12.08	29.	9.	3.	.06		
+	HYDROGRAPH AT	CH9	275.	12.08	31.	9.	4.	.06		
+	HYDROGRAPH AT	P1	186.	12.08	21.	7.	3.	.04		
+	3 COMBINED AT	P1-IN	904.	12.08	105.	33.	13.	.21		
+	ROUTED TO	RP1	28.	15.17	28.	23.	11.	.21		
+									457.46	15.17
+	2 COMBINED AT	CP1	389.	12.50	125.	52.	23.	.41		
+	HYDROGRAPH AT	S5	21.	12.58	6.	2.	1.	.01		

+	2 COMBINED AT	CS5	408.	12.50	131.	54.	24.	.42
	HYDROGRAPH AT	S7	17.	12.50	4.	1.	1.	.01
+	2 COMBINED AT	CS7	426.	12.50	135.	55.	25.	.43
	HYDROGRAPH AT	O1A	70.	12.58	18.	6.	2.	.04
+	HYDROGRAPH AT	O2	2171.	12.75	767.	239.	96.	1.58
+	HYDROGRAPH AT	O3	62.	12.33	12.	4.	2.	.03
+	HYDROGRAPH AT	S6	32.	12.83	10.	3.	1.	.02
+	5 COMBINED AT	CS6	2664.	12.75	941.	305.	125.	2.09
	HYDROGRAPH AT	O4	269.	12.50	65.	20.	8.	.13
+	2 COMBINED AT	CO4	2881.	12.67	1006.	325.	133.	2.23
	HYDROGRAPH AT	A6	73.	12.08	9.	3.	1.	.02
+	HYDROGRAPH AT	S8	39.	12.33	8.	2.	1.	.02
+	3 COMBINED AT	CS8	2919.	12.67	1022.	329.	135.	2.26
	HYDROGRAPH AT	S1	24.	12.83	8.	2.	1.	.02
+	HYDROGRAPH AT	S2	52.	13.25	23.	7.	3.	.05
+	HYDROGRAPH AT	CH1	57.	13.33	27.	8.	3.	.06
+	HYDROGRAPH AT	S3	17.	12.42	3.	1.	0.	.01
+	HYDROGRAPH AT	O5	302.	12.67	88.	27.	11.	.18
+	4 COMBINED AT	CO5	381.	12.67	126.	39.	16.	.26
	HYDROGRAPH AT	CH2	15.	12.17	2.	1.	0.	.01
+	HYDROGRAPH AT	A12	114.	12.08	11.	3.	1.	.02
+	2 COMBINED AT	CA12	126.	12.08	13.	4.	2.	.03
	HYDROGRAPH AT	CH3	107.	12.17	15.	4.	2.	.03
+	HYDROGRAPH AT	A11	158.	12.08	17.	5.	2.	.03
+	2 COMBINED AT	CA11	261.	12.08	32.	10.	4.	.07
	HYDROGRAPH AT	CH4	251.	12.17	36.	11.	4.	.07
+	HYDROGRAPH AT	A10T	62.	12.17	9.	3.	1.	.02
+	HYDROGRAPH AT	A10S	123.	12.08	13.	4.	2.	.03
+	2 COMBINED AT	CA10	180.	12.08	22.	7.	3.	.05
	HYDROGRAPH AT	A9	105.	12.08	10.	3.	1.	.02
+	HYDROGRAPH AT	P2	101.	12.08	12.	4.	2.	.02
+	4 COMBINED AT	P2-IN	616.	12.08	80.	24.	10.	.16

ROUTED TO

+		RP2	118.	12.75	64.	19.	7.	.16		
+									457.72	12.75
		HYDROGRAPH AT								
+		CH5	120.	12.75	65.	19.	7.	.16		
		HYDROGRAPH AT								
+		A7T	66.	12.17	10.	3.	1.	.02		
		HYDROGRAPH AT								
+		A7S	144.	12.08	16.	5.	2.	.03		
		2 COMBINED AT								
+		CA7	201.	12.08	26.	8.	3.	.05		
		HYDROGRAPH AT								
+		A8	80.	12.08	8.	2.	1.	.02		
		HYDROGRAPH AT								
+		P3	87.	12.08	10.	3.	1.	.02		
		3 COMBINED AT								
+		P3-IN	368.	12.08	44.	14.	5.	.09		
		ROUTED TO								
+		RP3	53.	12.92	37.	11.	4.	.09		
+									455.87	12.92
		HYDROGRAPH AT								
+		CH6	54.	12.83	37.	11.	5.	.09		
		2 COMBINED AT								
+		CCH6	173.	12.75	102.	30.	12.	.25		
		HYDROGRAPH AT								
+		S9	80.	12.42	17.	5.	2.	.04		
		HYDROGRAPH AT								
+		S10	44.	12.33	8.	2.	1.	.02		
		3 COMBINED AT								
+		CS9	286.	12.42	126.	38.	15.	.30		
1										

SUMMARY OF KINEMATIC WAVE -- MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	INTERPOLATED TO COMPUTATION INTERVAL			
						DT	PEAK	TIME TO PEAK	VOLUME
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
	A1T MANE	2.26	27.96	728.16	5.50	5.00	27.39	730.00	5.49
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2520E+01 OUTFLOW= .2491E+01 BASIN STORAGE= .4099E-03 PERCENT ERROR= 1.1									
	A1S MANE	2.61	137.15	724.04	5.64	5.00	131.18	725.00	5.64
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .8923E+01 OUTFLOW= .8693E+01 BASIN STORAGE= .4875E-03 PERCENT ERROR= 2.6									
	CH14 MANE	3.46	7.12	725.83	5.49	5.00	7.05	725.00	5.48
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .4743E+00 OUTFLOW= .4688E+00 BASIN STORAGE= .3115E-03 PERCENT ERROR= 1.1									
	A2T MANE	3.28	57.59	730.43	5.45	5.00	57.39	730.00	5.45
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .5484E+01 OUTFLOW= .5382E+01 BASIN STORAGE= .9579E-03 PERCENT ERROR= 1.9									
	A2S MANE	2.67	150.43	723.85	5.64	5.00	144.46	725.00	5.63
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .9942E+01 OUTFLOW= .9680E+01 BASIN STORAGE= .5134E-03 PERCENT ERROR= 2.6									
	CH12 MANE	2.38	4.44	724.72	5.50	5.00	4.31	725.00	5.51
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2668E+00 OUTFLOW= .2641E+00 BASIN STORAGE= .1752E-03 PERCENT ERROR= .9									
	CH13 MANE	3.96	9.58	723.77	5.48	5.00	8.74	725.00	5.47
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .5929E+00 OUTFLOW= .5848E+00 BASIN STORAGE= .3570E-03 PERCENT ERROR= 1.3									
	A3 MANE	2.30	61.93	724.85	5.65	5.00	61.14	725.00	5.68

CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.0000E+00	EXCESS=	.3890E+01	OUTFLOW=	.3800E+01	BASIN STORAGE=	.3366E-03	PERCENT ERROR=	2.3
CH10	MANE	3.36	6.35	724.81	5.51	5.00	6.23	725.00	5.55	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.0000E+00	EXCESS=	.3854E+00	OUTFLOW=	.3819E+00	BASIN STORAGE=	.2777E-03	PERCENT ERROR=	.8
CH11	MANE	2.38	4.44	724.72	5.50	5.00	4.31	725.00	5.51	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.0000E+00	EXCESS=	.2668E+00	OUTFLOW=	.2641E+00	BASIN STORAGE=	.1752E-03	PERCENT ERROR=	.9
CH7	MANE	5.00	16.54	725.00	5.35	5.00	16.54	725.00	5.35	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.0000E+00	EXCESS=	.1067E+01	OUTFLOW=	.1026E+01	BASIN STORAGE=	.7822E-03	PERCENT ERROR=	3.7
A5	MANE	2.97	140.34	724.03	5.63	5.00	133.57	725.00	5.62	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.0000E+00	EXCESS=	.9170E+01	OUTFLOW=	.8918E+01	BASIN STORAGE=	.5553E-03	PERCENT ERROR=	2.7
CH8	MANE	1.07	168.61	725.84	5.57	5.00	166.32	725.00	5.57	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.9924E+01	EXCESS=	.1571E+01	OUTFLOW=	.1146E+02	BASIN STORAGE=	.2671E-03	PERCENT ERROR=	.3
A4	MANE	1.29	102.51	724.49	5.08	5.00	100.30	725.00	5.09	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.0000E+00	EXCESS=	.6515E+01	OUTFLOW=	.5714E+01	BASIN STORAGE=	.2350E-03	PERCENT ERROR=	12.3
CH9	MANE	.88	280.65	725.43	5.41	5.00	274.91	725.00	5.41	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.1720E+02	EXCESS=	.1423E+01	OUTFLOW=	.1860E+02	BASIN STORAGE=	.2560E-03	PERCENT ERROR=	.2
A6	MANE	5.00	72.90	725.00	5.57	5.00	72.90	725.00	5.57	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.0000E+00	EXCESS=	.5311E+01	OUTFLOW=	.5112E+01	BASIN STORAGE=	.9760E-03	PERCENT ERROR=	3.7
CH1	MANE	5.00	57.14	800.00	5.51	5.00	57.14	800.00	5.51	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.1413E+02	EXCESS=	.2757E+01	OUTFLOW=	.1682E+02	BASIN STORAGE=	.3597E-02	PERCENT ERROR=	.4
CH2	MANE	5.00	15.36	730.00	4.85	5.00	15.36	730.00	4.85	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.0000E+00	EXCESS=	.1512E+01	OUTFLOW=	.1320E+01	BASIN STORAGE=	.2050E-02	PERCENT ERROR=	12.5
A12	MANE	1.74	114.14	725.10	5.02	5.00	113.71	725.00	5.03	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.0000E+00	EXCESS=	.7317E+01	OUTFLOW=	.6340E+01	BASIN STORAGE=	.3260E-03	PERCENT ERROR=	13.4
CH3	MANE	4.39	111.02	728.70	4.99	5.00	106.75	730.00	4.99	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.7682E+01	EXCESS=	.1245E+01	OUTFLOW=	.8789E+01	BASIN STORAGE=	.1382E-02	PERCENT ERROR=	1.5
A11	MANE	2.39	164.16	724.07	5.64	5.00	157.65	725.00	5.64	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.0000E+00	EXCESS=	.1065E+02	OUTFLOW=	.1038E+02	BASIN STORAGE=	.4782E-03	PERCENT ERROR=	2.5
CH4	MANE	3.86	260.55	728.77	5.29	5.00	250.54	730.00	5.30	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.1916E+02	EXCESS=	.2075E+01	OUTFLOW=	.2103E+02	BASIN STORAGE=	.1474E-02	PERCENT ERROR=	.9
A10T	MANE	2.81	62.64	729.38	5.46	5.00	61.97	730.00	5.45	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.0000E+00	EXCESS=	.5722E+01	OUTFLOW=	.5617E+01	BASIN STORAGE=	.7387E-03	PERCENT ERROR=	1.8
A10S	MANE	2.33	126.55	724.58	5.65	5.00	122.75	725.00	5.65	
CONTINUITY SUMMARY (AC-FT) -	INFLOW=	.0000E+00	EXCESS=	.7997E+01	OUTFLOW=	.7801E+01	BASIN STORAGE=	.4245E-03	PERCENT ERROR=	2.4

A9	MANE	1.27	106.95	724.60	5.08	5.00	104.68	725.00	5.10
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .6762E+01 OUTFLOW= .5937E+01 BASIN STORAGE= .2341E-03 PERCENT ERROR= 12.2									
CH5	MANE	.58	119.57	765.36	4.28	5.00	119.56	765.00	4.28
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3677E+02 EXCESS= .3558E+00 OUTFLOW= .3709E+02 BASIN STORAGE= .2947E-03 PERCENT ERROR= .1									
A7T	MANE	4.08	66.56	730.43	5.45	5.00	66.14	730.00	5.45
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .6285E+01 OUTFLOW= .6162E+01 BASIN STORAGE= .1163E-02 PERCENT ERROR= 1.9									
A7S	MANE	3.17	147.31	725.68	5.63	5.00	143.97	725.00	5.64
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .9818E+01 OUTFLOW= .9550E+01 BASIN STORAGE= .6044E-03 PERCENT ERROR= 2.7									
A8	MANE	1.36	80.42	724.17	5.06	5.00	79.62	725.00	5.07
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .5187E+01 OUTFLOW= .4535E+01 BASIN STORAGE= .2273E-03 PERCENT ERROR= 12.6									
CH6	MANE	.76	53.61	770.47	4.81	5.00	53.61	770.00	4.81
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2219E+02 EXCESS= .3854E+00 OUTFLOW= .2253E+02 BASIN STORAGE= .2239E-03 PERCENT ERROR= .2									

*** NORMAL END OF HEC-1 ***

VOLUME CALCULATIONS

EXCESS RAINFALL VOLUME CALCULATION

The volume generated by the site and the surrounding properties is calculated for the 25-year storm event. A summary of the design information that is included in this Appendix and related appendices are listed below.

- Excess rainfall and drainage areas used in the volume calculations were taken from the HEC-1 analysis located on pages IIIF-A-31 through IIIF-A-104.
- Post-development condition volume information is summarized on pages IIIF-A-107 through IIIF-A-110.

CAMELOT LANDFILL
1339-351-11-02-01
25-YEAR EXCESS RAINFALL
VOLUME CALCULATIONS

Required: Determine the 25-year 24-hour storm volume generated by the site and offsite areas using the excess rainfall calculated in the HEC-1 analysis of the proposed expansion site conditions.

Method: 1. Use the excessive rainfall data generated by the HEC-1 analysis (pages III F-A-31 through III F-A-104) to determine the volume produced by the site for the proposed expansion conditions.

Proposed Expansion Conditions

1. Volume Discharging Southeast Downstream of Entrance Road

1a. Landfill Areas Discharging into Pond P1 and Flowing under Entrance Road

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
A1T	0.0085	5.56	5.47	3
A1S	0.0289	5.79	18.48	9
A2T	0.0185	5.56	11.83	5
A2S	0.0322	5.79	20.59	10
A3	0.0126	5.79	8.07	4
CH7	0.0036	5.56	2.33	1
A5	0.0297	5.79	19.01	9
CH8	0.0053	5.56	3.37	2
A4	0.0211	5.79	13.51	7
CH9	0.0048	5.56	3.09	1
CH10	0.0013	5.56	0.85	0
CH11	0.0009	5.56	0.56	0
CH12	0.0009	5.56	0.59	0
CH13	0.0020	5.56	1.29	1
CH14	0.0016	5.56	1.02	0
P1	0.0361	7.44	23.10	14
Total Volume Flowing under Entrance Road				67

1b. Volume Upstream of Entrance Road

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
O1	0.1367	5.90	87.47	43
O1A	0.0366	5.67	23.42	11
O2	1.5754	5.66	1,008.23	476
S4	0.0677	5.56	43.34	20
S5	0.0115	5.56	7.34	3
S7	0.0084	5.56	5.39	2
Total Volume Upstream of Entrance Road				556

CAMELOT LANDFILL
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25-YEAR EXCESS RAINFALL
VOLUME CALCULATIONS

1c. Non-Landfill Areas Downstream of Entrance Road

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
S6	0.0218	5.56	13.92	6
O3	0.0253	5.56	16.18	7
Total Volume of Non-Landfill Areas D.S. of Entrance Road				14

Total Volume Discharging Southeast Downstream of Entrance Road = **636 ac-ft**

2. Volume in Midway Branch Exiting Permit Boundary

2a. Volume in Midway Branch Entering Permit Boundary

Offsite Area Entering Midway Branch	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
O4	0.1344	5.56	86.04	40
Total Volume in Midway Branch Entering Permit Boundary				40

2b. Landfill Areas Flowing East into Midway Branch

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
A6	0.0172	5.79	11.00	5
S8	0.0158	5.56	10.12	5
Total Volume Flowing East into Midway Branch				10

Total Volume in Midway Branch Excluding Section 1 Discharge Volume = **50 ac-ft**

Total Volume in Midway Branch Exiting Permit Boundary = **686 ac-ft**

3. Volume Discharging South into Elm Fork

3a. Areas Discharging into Pond P2

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
CH2	0.0051	5.56	3.29	2
A12	0.0237	5.79	15.17	7
CH3	0.0042	5.56	2.71	1
A11	0.0345	5.79	22.08	11
CH4	0.0070	5.56	4.45	2
A10T	0.0193	5.56	12.37	6
A10S	0.0259	5.79	16.60	8
A9	0.0219	5.79	13.99	7
P2	0.0196	7.44	12.55	8
Total Volume Discharging into Pond P2				51

CAMELOT LANDFILL
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25-YEAR EXCESS RAINFALL
VOLUME CALCULATIONS

3b. Areas Discharging into Pond P3

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
A7T	0.0212	5.56	13.58	6
A7S	0.0318	5.79	20.36	10
A8	0.0168	5.79	10.75	5
P3	0.0168	7.44	10.74	7
Total Volume Discharging into Pond P3				28

3c. Flow Downstream of Ponds P2 and P3

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
CH5	0.0012	5.56	0.76	0
CH6	0.0013	5.56	0.83	0
Total Volume Downstream of Ponds P2 and P3				1

Total Volume Discharged South to Elm Fork = **80 ac-ft**

4. Volume Discharging Southeast into Elm Fork

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
S10	0.0168	5.56	10.76	5
Total Volume Discharging Southeast into Elm Fork				5

5. Volume Discharging Southwest into Elm Fork

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
S9	0.0355	5.56	22.75	11
Total Volume Discharging Southwest into Elm Fork				11

CAMELOT LANDFILL
1339-351-11-02-01
25-YEAR EXCESS RAINFALL
VOLUME CALCULATIONS

6. Southern Volume Discharging Southwest Towards Elm Fork

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
S3	0.0071	5.56	4.55	2
Total Southern Volume Discharging Southwest Towards Elm Fork				2

7. Northern Volume Discharging West Towards Elm Fork

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
S2	0.0482	5.56	30.86	14
CH1	0.0093	5.56	5.94	3
Total Northern Volume Discharging West Towards Elm Fork				17

8. Volume Discharging from Northwest Corner Towards Elm Fork

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
S1	0.0160	5.56	10.26	5
Total Volume Discharging from NW Corner Towards Elm Fork				5

<p>Total Volume Exiting Permit Boundary = 805 ac-ft</p>
--

VELOCITY CALCULATIONS

Required: Determine the flow velocities entering and exiting the permit boundary using HYDROCALC HYDRAULICS (Version 1.2a, 1996) for the flows calculated for the 25-year storm event in the HEC-1 analysis. HEC-RAS is used to determine the velocity in Elm Fork.

Method:

1. Use the flow data generated by the HEC-1 analysis to determine velocity of runoff entering the landfill permit boundary.
2. Use the flow data generated by the HEC-1 analysis to determine velocity of runoff exiting the landfill permit boundary.

I. Flow Velocity entering the landfill permit boundary

DP1

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$$Q_{25} = 2171 \text{ cfs}$$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	2171	0.010	0.03	4.00	20.00	60.00	2.85	8.08

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

DP2

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$$Q_{25} = 62 \text{ cfs}$$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	62	0.090	0.03	4.00	6.00	87.00	0.16	4.38

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

DP4

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$$Q_{25} = 2881 \text{ cfs}$$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	2881	0.005	0.03	10.00	2.00	22.00	6.00	8.28

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

DP12

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$$Q_{25} = 298 \text{ cfs}$$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	298	0.001	0.03	77.00	83.00	0.00	1.65	1.38

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

CAMELOT LANDFILL
1339-351-11-02-6B.6
25-YEAR VELOCITY CALCULATIONS

DP13

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$Q_{25} = 70 \text{ cfs}$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	70	0.019	0.03	50.00	48.00	0.00	0.66	3.27

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

2. Flow Velocity exiting the landfill permit boundary

DP3

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$Q_{25} = 2664 \text{ cfs}$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	2664	0.008	0.03	16.00	17.00	27.00	3.85	7.63

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

DP5

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$Q_{25} = 2919 \text{ cfs}$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	2919	0.008	0.03	2.00	2.00	9.00	8.73	12.63

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

DP6

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$Q_{25} = 173 \text{ cfs}$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	173	0.030	0.03	1.00	2.00	1.00	2.98	10.60

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

DP7

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$Q_{25} = 44 \text{ cfs}$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	44	0.010	0.03	24.00	29.00	0.00	0.79	2.67

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

CAMELOT LANDFILL
1339-351-11-02-6B.6
25-YEAR VELOCITY CALCULATIONS

DP8

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$$Q_{25} = 80 \text{ cfs}$$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	80	0.083	0.03	4.50	5.00	0.00	1.27	10.39

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

DP9

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$$Q_{25} = 17 \text{ cfs}$$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	17	0.089	0.03	99.00	100.00	0.00	0.22	3.44

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

DP10

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$$Q_{25} = 57 \text{ cfs}$$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	57	0.001	0.03	3.00	3.00	20.00	1.37	1.72

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

DP11

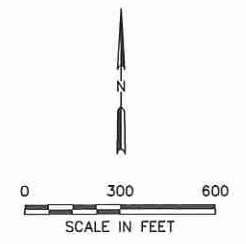
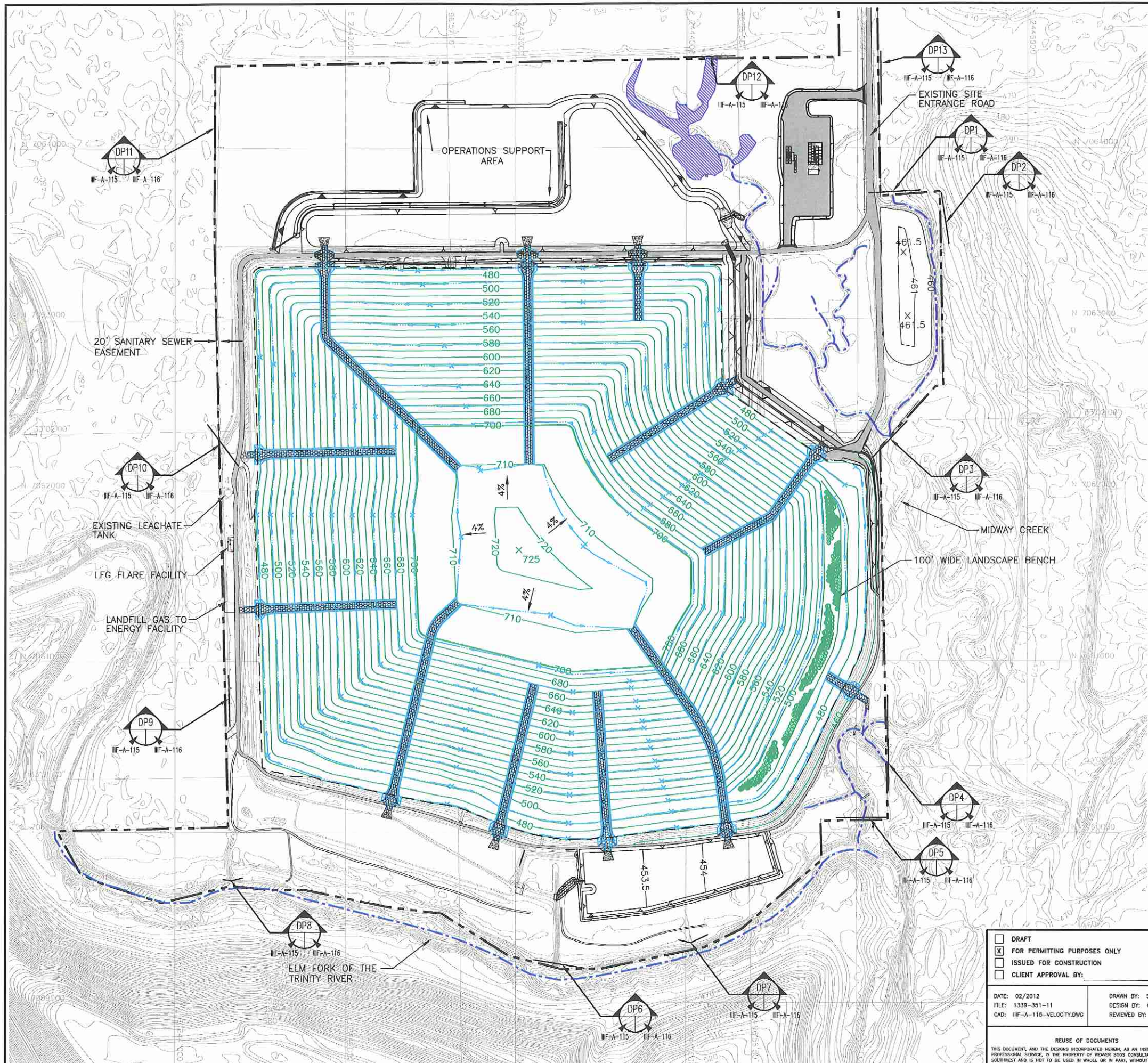
- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$$Q_{25} = 24 \text{ cfs}$$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	24	0.001	0.03	100.00	100.00	0.00	0.59	0.69

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

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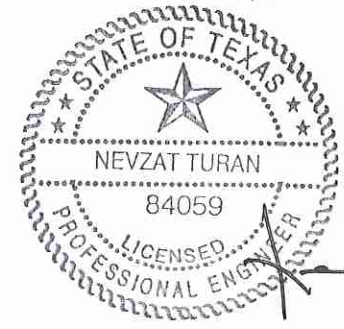


LEGEND

- PERMIT BOUNDARY
- PROPOSED LIMIT OF WASTE
- STATE PLANE COORDINATE SYSTEM
- GEODETIC COORDINATE SYSTEM
- EXISTING CONTOUR (SEE NOTE 1)
- FINAL COVER CONTOUR
- PERMITTED DRAINAGE LETDOWN
- PERMITTED DRAINAGE SWALE
- USACE SECTION 404 JURISDICTIONAL WATERS OF THE U.S. (SEE NOTE 5)
- USACE JURISDICTIONAL WETLANDS

NOTE:

1. CONTOURS AND ELEVATIONS PROVIDED BY METROPOLITAN AERIAL SURVEYS COMPILED FROM AERIAL PHOTOGRAPHY FLOWN 8-28-2010. THE GRID SYSTEM IS TIED TO THE TEXAS STATE PLANE COORDINATE SYSTEM NORTH CENTRAL ZONE NAD 1983. ELEVATIONS ARE BASED ON NAVD 1988. OFF-SITE CONTOURS AND ELEVATIONS PROVIDED BY DFWMAPS.COM FROM AERIAL SURVEYS COMPILED FROM AERIAL PHOTOGRAPHY FLOWN JANUARY TO MARCH 2007.
2. PERMIT BOUNDARY WAS PREPARED BY PEISER SUREYING CO. IN DECEMBER 2010.
3. MAXIMUM FINAL COVER ELEVATION IS 725 FT-MSL. MAXIMUM TOP OF WASTE ELEVATION IS 721.5 FT-MSL.
4. REFER TO SHEET IIF-A-28 FOR COMPLETE OFFSITE DRAINAGE AREA DELINEATIONS.
5. SECTION 404 JURISDICTIONAL WATERS OF THE U.S. AND WETLANDS REPRODUCED FROM THE GOSHAWK ENVIRONMENTAL CONSULTANTS, INC. SEPTEMBER 2010 REPORT WHICH IS INCLUDED IN PARTS I/II, APPENDIX I/II.



[Handwritten Signature]
2-28-12

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<input checked="" type="checkbox"/> FOR PERMITTING PURPOSES ONLY	CITY OF FARMERS BRANCH
<input type="checkbox"/> ISSUED FOR CONSTRUCTION	
<input type="checkbox"/> CLIENT APPROVAL BY:	
DATE: 02/2012	DRAWN BY: SRF
FILE: 1339-351-11	DESIGN BY: CRM
CAD: IIF-A-115-VELOCITY.DWG	REVIEWED BY: JPY
REUSE OF DOCUMENTS	
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REVISIONS		
NO.	DATE	DESCRIPTION

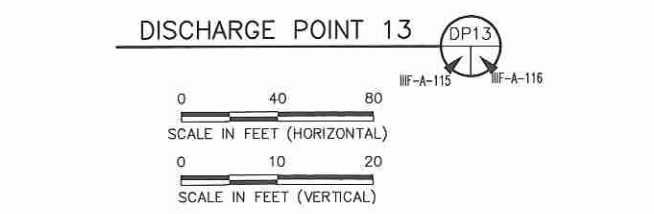
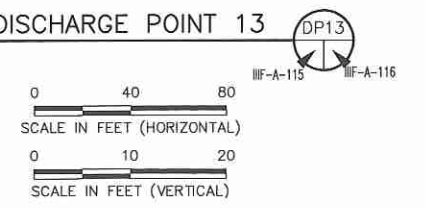
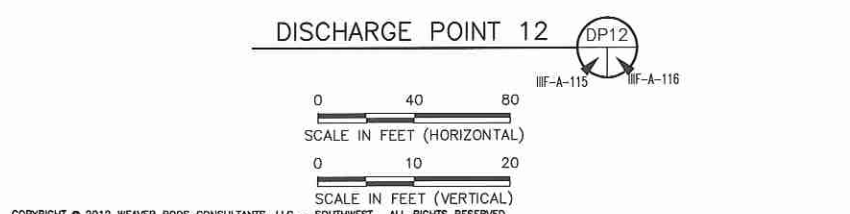
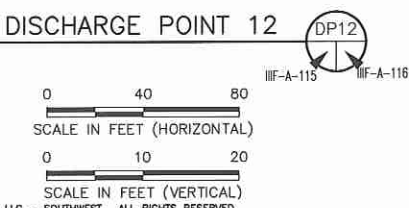
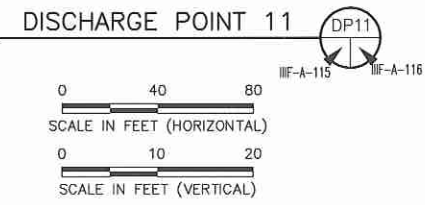
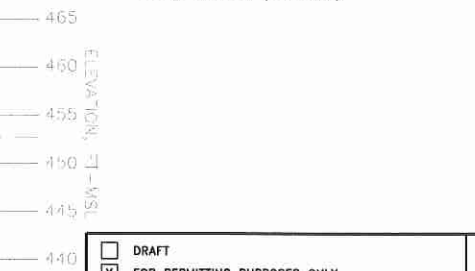
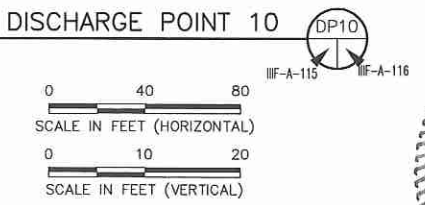
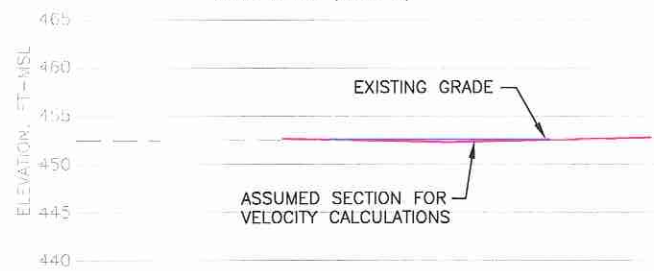
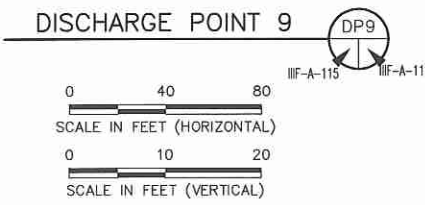
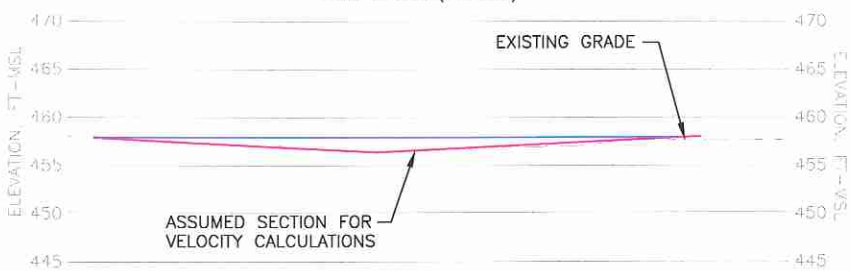
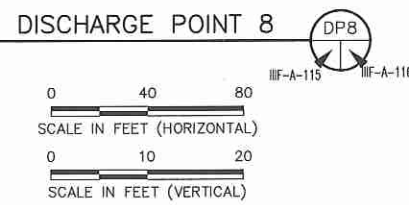
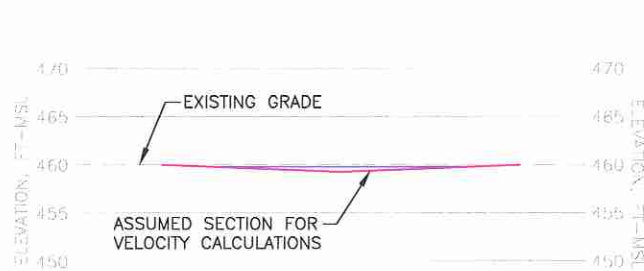
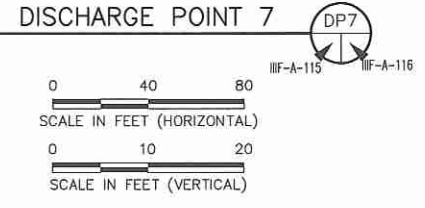
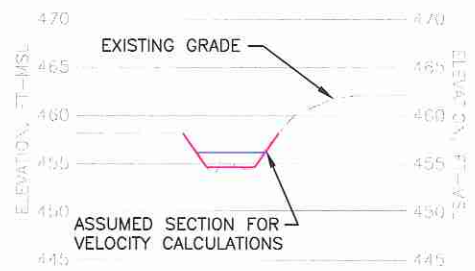
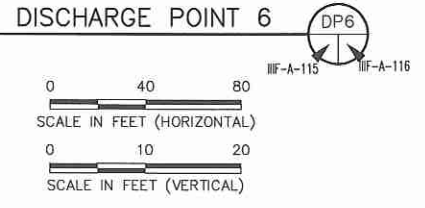
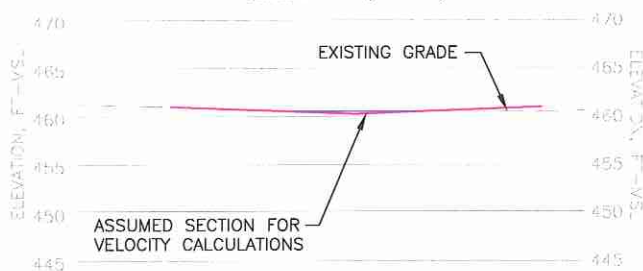
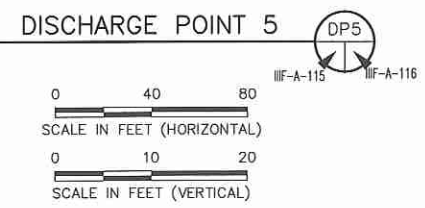
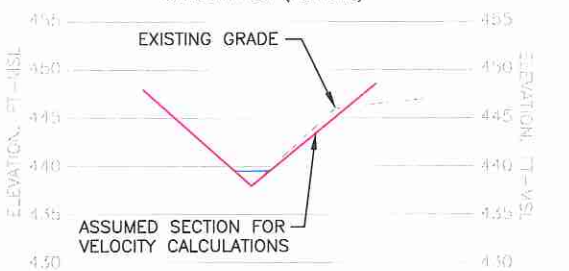
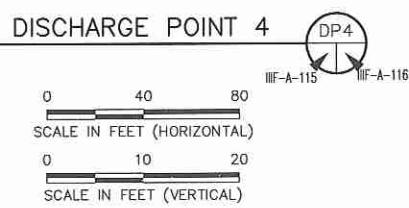
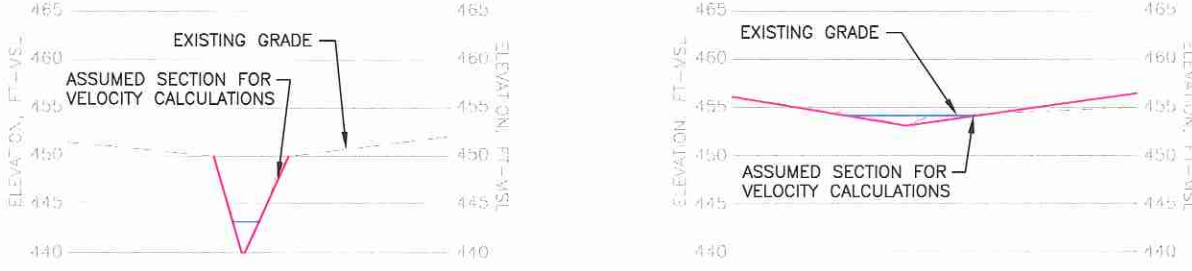
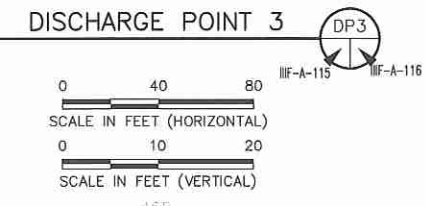
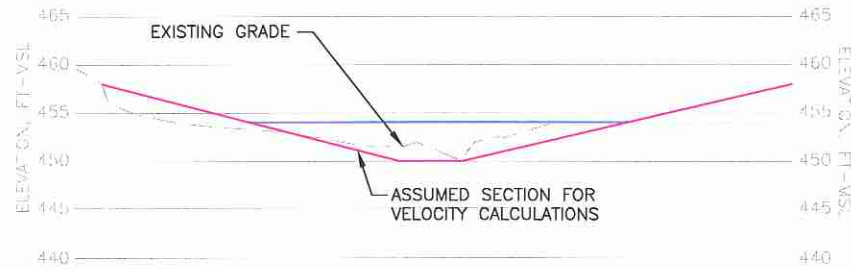
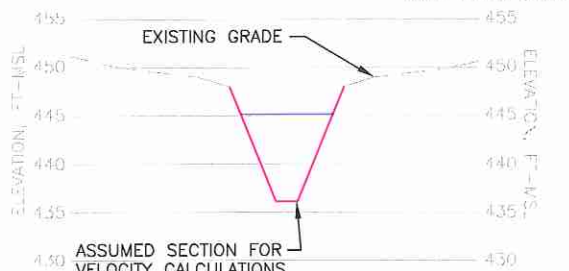
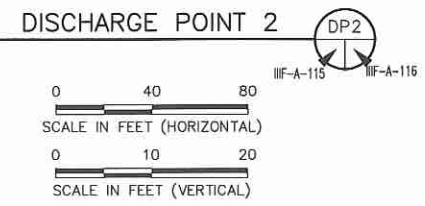
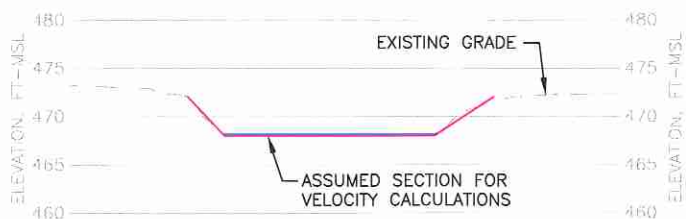
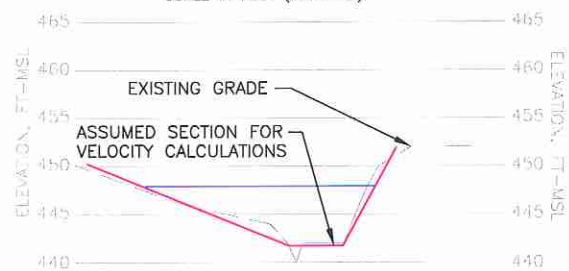
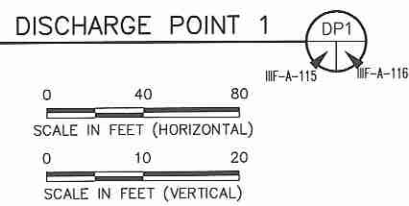
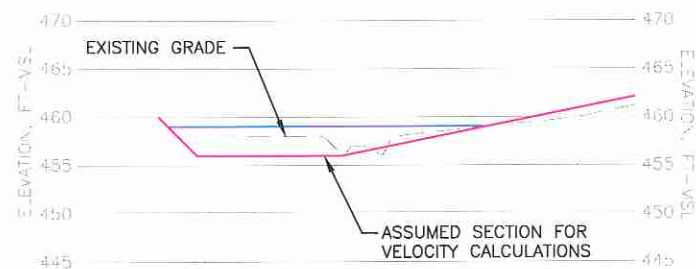
**MAJOR PERMIT AMENDMENT
UPDATED PERMITTED DISCHARGE
POINT VELOCITY CALCULATIONS**

CAMELOT LANDFILL
DENTON COUNTY, TEXAS

Weaver Boos Consultants
TBPE REGISTRATION NO. F-3727

CHICAGO, IL	FORT WORTH, TX	GRIFITH, IN
NAPEVILLE, IL	SOUTH BEND, IN	SPRINGFIELD, IL
COLUMBUS, OH	(817) 735-9770	ST. LOUIS, MO
		SHEET IIF-A-115

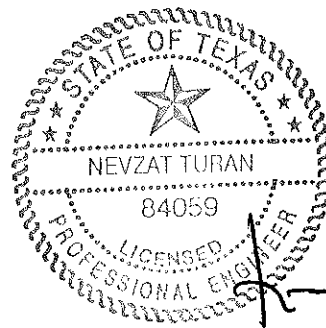
O:\1359\351\EXPANSION 2009\PART III-SUP\IIF-A-116-DISCHARGE POINT SECTIONS.dwg, jwilson, 1:2



<input type="checkbox"/> DRAFT <input checked="" type="checkbox"/> FOR PERMITTING PURPOSES ONLY <input type="checkbox"/> ISSUED FOR CONSTRUCTION <input type="checkbox"/> CLIENT APPROVAL BY:	PREPARED FOR CITY OF FARMERS BRANCH	MAJOR PERMIT AMENDMENT UPDATED PERMITTED DISCHARGE POINT VELOCITY CALCULATIONS CAMELOT LANDFILL DENTON COUNTY, TEXAS												
DATE: 02/2012 FILE: 1339-351-11 CAD: IIF-A-116-VELOCITY.DWG	DRAWN BY: SRF DESIGN BY: CRM REVIEWED BY: JPY	Weaver Boos Consultants TBPE REGISTRATION NO. F-3727												
REUSE OF DOCUMENTS <small>THIS DOCUMENT, AND THE DESIGNS INCORPORATED HEREIN, AS AN INSTRUMENT OF PROFESSIONAL SERVICE, IS THE PROPERTY OF WEAVER BOOS CONSULTANTS, LLC - SOUTHWEST AND IS NOT TO BE USED IN WHOLE OR IN PART, WITHOUT THE WRITTEN AUTHORIZATION OF WEAVER BOOS CONSULTANTS, LLC - SOUTHWEST.</small>		CHICAGO, IL NAPERVILLE, IL COLUMBUS, OH DENVER, CO												
REVISIONS <table border="1"> <thead> <tr> <th>NO.</th> <th>DATE</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> </tr> </tbody> </table>		NO.	DATE	DESCRIPTION										GRIFFITH, IN SOUTH BEND, IN SPRINGFIELD, IL ST. LOUIS, MO
NO.	DATE	DESCRIPTION												
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APPENDIX IIIF-B

**PERIMETER CHANNEL, DETENTION POND,
AND CULVERT DESIGN**

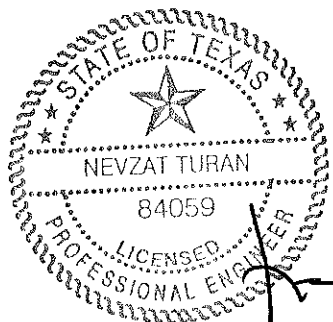


2-28-12

Includes Pages IIIF-B-1 through IIIF-B-19

CONTENTS

Perimeter Channel Design	IIIF-B-1
Channel Erosion Control Design	IIIF-B-5
Detention Pond Design	IIIF-B-7
Culvert Design	IIIF-B-12



2-28-12

PERIMETER CHANNEL DESIGN

Perimeter channels have been designed to contain stormwater runoff from the 25-year storm frequency. A summary of the design information that is included in this Appendix is listed below.

- Flow rates used for the perimeter channel design were taken from the HEC-1 analysis included in Appendix IIIF-A.
- Perimeter channel design system information is summarized on Drawing IIIF.4 in Appendix IIIF.
- Channel profiles are presented on Drawings IIIF.5 through IIIF.8 in Appendix IIIF.
- Hydraulic calculations are summarized on pages IIIF-B-2.
- Channel Erosion Control Design information is included on page IIIF-B-5.

CAMELOT LANDFILL
1339-357-11-02-0B.6
PERIMETER CHANNEL HYDRAULIC ANALYSIS

Channel ²	From	Station ²	To	Flow Rate ³ (cfs)	Bottom Slope (ft/ft)	Bottom Width (ft)	Left Side Slope (ft/ft)	Right Side Slope (ft/ft)	Manning's n-Value	Normal Depth (ft)	Flow Vel. (fps)	Froude No.	Vel. Head (ft)	Energy Head (ft)	Flow Area ¹ (sq.ft.)	Top width of Flow ¹ (ft)
A ⁶	0+00.00	4+61.95		31	0.0014	10	3	3	0.03	1.25	1.80	0.521	0.05	1.30	17.19	17.50
A	4+61.95	10+42.64		31	0.0015	10	3	3	0.03	1.23	1.85	0.331	0.05	1.28	16.78	17.36
A	10+42.64	18+25.15		31	0.0015	20	3	3	0.03	0.86	1.60	0.322	0.04	0.90	19.37	25.15
B ⁶	0+00.00	0+66.39		21	0.0142	0	3	3	0.03	1.28	4.24	0.932	0.28	1.56	4.96	7.71
B	0+66.39	2+30.02		21	0.0011	0	3	3	0.03	2.07	1.63	0.282	0.04	2.11	12.90	12.44
B	2+30.02	15+97.80		21	0.0016	0	3	3	0.03	1.93	1.87	0.336	0.05	1.99	11.21	11.60
B	15+97.80	17+05.54		21	0.0020	0	3	3	0.03	1.85	2.04	0.373	0.06	1.92	10.31	11.13
B	17+05.54	21+08.28		21	0.0020	15	3	3	0.03	0.74	1.66	0.361	0.04	0.78	12.69	19.42
C	0+00.00	13+84.14		57	0.0010	15	3	3	0.03	1.59	1.82	0.283	0.05	1.64	31.35	24.52
D	0+00.00	4+01.14		261	0.0010	15	3	3	0.03	3.57	2.84	0.315	0.13	3.70	91.86	36.43
D	4+01.14	4+39.23		261	0.0010	15	3	3	0.03	3.57	2.84	0.315	0.13	3.70	91.86	36.43
D	4+39.23	21+08.04		126	0.0015	15	3	3	0.03	1.22	5.54	0.968	0.48	1.70	22.74	22.31
D	21+08.04	21+61.47		126	0.0010	15	3	3	0.03	2.44	2.31	0.300	0.08	2.53	54.56	29.66
E	0+00.00	5+32.89		7	0.0050	0	3	3	0.03	1.04	2.18	0.533	0.07	1.11	3.22	6.21
F	0+00.00	6+35.76		9	0.0050	0	3	3	0.03	1.14	2.32	0.544	0.08	1.22	3.87	6.82
G	0+00.00	3+12.15		4	0.0050	0	3	3	0.03	0.84	1.89	0.514	0.06	0.90	2.12	5.04
H	0+00.00	3+10.52		4	0.0050	0	3	3	0.03	0.84	1.89	0.514	0.06	0.90	2.12	5.04
I	0+00.00	4+83.50		6	0.0050	0	3	3	0.03	0.98	2.10	0.530	0.07	1.04	2.86	5.86
J	0+00.00	13+77.20		275	0.0010	10	3	3	0.03	4.16	2.94	0.317	0.13	4.29	93.48	34.95
J	13+77.20	15+67.00		17	0.0047	0	3	3	0.03	1.46	2.66	0.549	0.11	1.57	6.39	8.76
J	15+67.00	16+13.94		17	0.0032	0	3	3	0.03	1.57	2.30	0.458	0.08	1.65	7.38	9.41
J	16+13.94	16+67.60		17	0.0037	0	3	3	0.03	1.53	2.43	0.491	0.09	1.62	6.99	9.16
J	16+67.60	23+72.35		118	0.0030	1.5	3	3	0.03	1.75	3.33	0.498	0.17	1.92	35.46	25.51
K	0+00.00	2+02.21		173	0.0300	0	3	3	0.03	2.46	9.51	1.511	1.41	3.87	18.19	14.78
K	2+02.21	6+16.92		53	0.0025	2.5	3	3	0.03	1.06	1.78	0.322	0.05	1.11	29.76	31.34
L	0+00.00	1+37.63		80	0.0574	8	3	2.5	0.03	0.85	9.14	1.937	1.30	2.15	8.75	12.66
M	0+00.00	3+13.50		389	0.0020	20	17	22	0.03	2.26	2.69	0.409	0.11	2.37	144.75	108.12
N	0+00.00	755.84		32	0.0023	10	10	30	0.03	0.81	1.50	0.373	0.03	0.85	21.35	42.52
O	0+00.00	12+00.29		2664	0.0048	10	4.3	2.5	0.03	7.87	9.20	0.760	1.31	9.19	289.55	63.54
P	0+00.00	26+45.81		2881	0.0044	10	3	3.5	0.03	8.41	9.18	0.735	1.31	9.72	313.81	64.65
Q	0+00.00	9+22.87		73	0.0397	5	3	3	0.03	1.08	8.17	1.635	1.04	2.12	8.93	11.50
R	0+00.00	3+06.76														

Note: 1) Calculations were performed using the HYDROCALC HYDRAULIC FOR WINDOWS Computer Program developed by Dodson and Associates (Version 1.2a, 1996).

2) Refer to Drawing III-F-4 for channel locations.

3) Flow rates shown are the peak flow rates obtained from the HEC-1 model. See HEC-1 Output-Postdevelopment Conditions in Appendix III-F-A.

4) Channel D is designed to flow through 3-48" CMP culverts (Culvert "2") at Stations 4+01.14 to 4+39.23. See Page III-F-B-14 for Culvert Design.

5) Channel J is designed to flow through a 36" CMP culvert (Culvert "4") at Stations 13+77.20 to 15+67.00. See Page III-F-B-16 for Culvert Design.

6) Channels A and B are each designed to convey a portion of the total runoff rate from Drainage Area S2 (52 cfs). The finalized design and usage of the operation support area, which is part of Drainage Area S2, may impact the proportion of runoff going into Channels A and B.

7) Channels M through R are existing, natural channels that do not accept runoff directly from the landfill development. The geometries listed in the table are average values approximated along the length of the channels. These calculations are provided to show that the existing channel system can convey runoff from the 2.5-year storm event within the existing channel banks inside the permit boundary.

Example Calculation: Calculate the normal depth for Channel D between stations 4+39.23 and 21+08.04.

List of Symbols

- Q_d = peak flow rate for channel, cfs - obtained from HEC-1 Analysis (Appendix III F-A)
- R = hydraulic radius, ft
- n = Manning's roughness coefficient
- S = channel slope, ft/ft
- b = bottom width of channel, ft
- z = z-ratio (ratio of run to rise for channel sideslope)
- A_f = flow area, sf
- g = gravitational acceleration = 32.2 ft/s²
- T = top width of flow, ft
- d = normal depth of channel, ft

The program uses an iterative process to calculate the normal depth of the channel to satisfy Manning's Equation

$$Q = \frac{1.486}{n} A R^{0.67} S^{0.5}$$

Design Inputs:

- Q_d = 261 cfs (for Channel D including Area A11)
- S = 0.001 ft/ft
- b = 15 ft
- z = 3 (H) : 1 (V)
- n = 0.03

Step 1 - Based on the geometry of the channel cross-section, solve for R and A_f

$$R = \frac{bd + zd^2}{b + 2d(z^2 + 1)^{0.5}}$$

$$A_f = bd + zd^2$$

assume: $d = 3.57$ ft

$$R = 2.442 \text{ ft}$$

$$A_f = 91.86 \text{ sf}$$

solve for Q: $Q = 261$

if Q is not equal to Q_d , select a new d and repeat calculations

Step 2 - solve for velocity, T, Froude number, velocity head, and energy head

$$Q = VA \Rightarrow V = Q/A$$

$$V = 2.84 \text{ ft/s}$$

$$T = b + 2(z \times d)$$

$$T = 36.43 \text{ ft}$$

$$F_r = \frac{V}{(gA/T)^{0.5}}$$

$$F_r = 0.315$$

$$\text{Velocity Head} = \frac{V^2}{2g}$$

$$\text{Velocity Head} = 0.13 \text{ ft}$$

Energy Head = water elevation + velocity head

$$\text{Energy Head} = 3.70 \text{ ft}$$

CHANNEL EROSION CONTROL DESIGN

Channel erosion controls have been designed for flow velocities resulted from the 25-year frequency flow rates. As shown on page IIIF-B-2 velocities in the perimeter channels range from 1.50 ft/s to 9.51 ft/s. The channel lining needed to protect against erosive velocities is shown on Drawings IIIF.5 through IIIF.8 in Appendix IIIF. All channels and drainage features will be inspected and maintained in accordance with the Site Operating Plan.

The following was used to select the type of channel lining material.

- Vegetation – used in all areas where velocities are less than 4 ft/s for channels.
- Turf reinforcement matting – used in channels for velocities between 4 ft/s and 13 ft/s. Please refer to page IIIF-B-6 for more information.
- 2-foot-thick Gabions – used at chute discharges in channels, areas in channels where flow velocities exceed 13 ft/s, and detention ponds (see Appendix IIIF-C – Final Cover Erosion Control Structure Design).

Channel lining details are presented on Drawings IIIF.10 in Appendix IIIF.

TECHNICAL DATA SHEET

MACMAT® NC10

Composite Turf Reinforcement Mat

MacMat® NC10 provides immediate erosion protection to prevent soil loss and creates the optimum micro-environment to enhance seed germination and plant emergence. The inclusion of the specially formulated MacMat® component, with its 95% open structure, adds the best permanent protection available. The biodegradable component of MacMat® NC10 is designed to create the right environment to enhance seed germination by insulating the seed bed, while absorbing and retaining optimal moisture.

Technical Data				
Physical Properties	Property	Roll Value (MD)		Test Method
	Tensile Strength	150 lbs/ft (2189 N/m ²)		ASTM D 5035 (modified)
	Thickness	0.4 in (10 mm)		ASTM D 5199
	Mass Unit/Area	15.0 oz/yd ² (.508 kg/m ²)		ASTM D 5261
	UV Stability	80% (strength retained)		ASTM D G53/D4355 ASATM D 5035 (modified)
	Resiliency	80% (thickness retained)		ASTM D 6524
	Sediment Trapping Capacity	376 in ³ /yd ² (7367 cm ³ /m ²)		Calculated
Performance Properties	Property	Roll Value		Test Method
		Unvegetated	Vegetated*	
	Permissible Velocity-30 min	13.0 ft/s (3.96 m/s)	19.0 ft/s (5.79 m/s)	Large Scale Flume Test ¹
	Permissible Velocity-50 hr	7.0 ft/s (2.13 m/s)	14.0 ft/s (4.26 m/s)	Large Scale Flume Test ¹
	Permissible Shear-30 min	3.1 lbs/ft ² (.148 kN/m ²)	10.0 lbs/ft ² (.478 kN/m ²)	Large Scale Flume Test ¹
	Permissible Shear-50 hr	2.2 lbs/ft ² (.105 kN/m ²)	8.0 lbs/ft ² (.383 kN/m ²)	Large Scale Flume Test ¹
	*Vegetated data extrapolated from actual test data with historically predictable results. ¹ Flume test performed at independent laboratory-data and details available upon request.			
Index Properties	Property	Roll Value (MD)		Test Method
	"Benchscale" Shear (unvegetated)	>5 lbs/ft ² (.239 kN/m ²)		ECTC TM #3
	Water Absorption	400%		ECTC Modified

Seller makes no warranty, express or implied, concerning the product furnished hereunder other than at the time of delivery it shall be of the quality and specifications stated herein. *ANY IMPLIED WARRANTY OF FITNESS FOR A PARTICULAR PURPOSE IS EXPRESSLY EXCLUDED AND, TO THE EXTENT THAT IT IS CONTRARY TO THE FOREGOING SENTENCE, ANY IMPLIED WARRANTY OF MERCHANTABILITY IS EXPRESSLY EXCLUDED.* Any recommendations made by the Seller concerning uses or applications of said product are believed reliable, and Seller makes no warranty of results to be obtained. The technical information supplied for this product type is subject to change at any time without notice.

This Data Sheet supersedes all previous Data Sheets for this style and is subject to change without notice.

MMAT-NC10 8/2006

DETENTION POND DESIGN

Detention ponds have been analyzed by using HEC-1, storage routing method. The input parameters for the model are presented in Appendix III F-A. A summary of HEC-1 results are presented on page III F-B-8. As can be seen on the table, during the 25-year storm event, none of the ponds flow over their spillways.

Downstream sides of the low-water outlets will be designed with either rock riprap or gabions as shown on pages III F-B-9 and III F-B-10.

Purpose: Demonstrate that the detention pond outlet structure designs are adequate to convey runoff from the various subbasins to their discharge points.

Method:

1. Use the 25-year, 24-hour flow rates and water surface elevations for the drainage areas that will discharge to each detention pond from the HEC-1 analysis (see Appendix IIIF-A).
2. Use the Weir Equation to calculate the flow rate over the spillways as appropriate.

Solution:

	P1	P2	P3
Bottom ELEV, ft ¹	454.0	454.0	453.0
Spillway ELEV, ft	458.0	458.0	458.0
Spillway Length, ft	25	25	25
Top of Road/Berm, ft	464.0	459.0	460.0
Discharge Pipe Downstream Invert ELEV, ft	453.00	452.6	452.35
Peak Inflow Q ₂₅ , cfs	904	616	368
Peak Outflow Q ₂₅ , cfs	28	118	53
Peak Stage in Pond Q ₂₅ , ft	457.46	457.72	455.87
Est. Flow (Q ₂₅) over Spillway, cfs	--	--	--
Velocity (Q ₂₅) over Spillway, fps	--	--	--

- Note:
- 1) Details of the pond outlet structures are presented on Drawings IIIF.19 and IIIF.20. As shown, gabions are provided downstream of all the spillways.
 - 2) The flow over the spillway is estimated using the formula $Q = CLH^{3/2}$ where C = 2.64, L is the length of the spillway in feet, and H is the head on the spillway in feet. The flow over the spillway conservatively assumes no flow through the low water outlet.
 - 3) Calculations for velocity over the spillway were performed using the HYDROCALC HYDRAULICS FOR WINDOWS Computer Program developed by Dodson and Associates (Version 1.2a, 1996).

DETENTION POND OUTLET STRUCTURE AND CULVERT EROSION PROTECTION CALCULATIONS

Required: Determine the minimum length and median diameter of riprap required at the detention pond outlet structures and creek culverts to control erosion in the detention pond outlet channels.

- Reference:**
1. Haan, Barfield, and Hayes, *Design Hydrology and Sedimentology for Small Catchments*, 1994.
 2. Dodson's and Associates, Inc., *ProHec-1 Plus Program Documentation*, 1995.
 3. Freeman, Gary E., J. Craig Fischenich, *Gabion for Streambank Erosion Control*, 2000. EMRRP Technical Notes Collection (ERDC TN-EMRRP-SR-22), U.S. Army Engineer Research and Development Center, Vicksburg, MS.

Solution: The riprap will be designed for the 25-year flow rates at the detention pond outlet structures and culverts. The flow at the outlet structures and culverts can be divided into two categories:

1. Flow over the Spillway/Road

As shown on pages III-F-B-8 through III-F-B-10, none of the detention ponds nor any creek culverts are expected to have flow over the spillways or roadways during the 25-year storm event. Erosion protection calculations for the drainage structures will be based on flow through low water outlets/culverts only.

Flow Structure Spillway Topslope	25-Year Flow Rate (cfs)	25-Year Velocity (ft/s)	25-Year Flow Depth (ft)	25-Year Foude Number	25-Year Velocity Head (ft)	25-Year Energy Head (ft)	25-Year Flow Area (sq. ft.)	25-Year Top Width (ft)
P1	--	--	--	--	--	--	--	--
P2	--	--	--	--	--	--	--	--
P3	--	--	--	--	--	--	--	--
Culvert "1"	--	--	--	--	--	--	--	--
Culvert "2"	--	--	--	--	--	--	--	--
Culvert "3"	--	--	--	--	--	--	--	--
Culvert "4"	--	--	--	--	--	--	--	--
Culvert "5"	--	--	--	--	--	--	--	--
Culvert "6"	--	--	--	--	--	--	--	--
Culvert "7"	--	--	--	--	--	--	--	--

Flow Structure Spillway Sideslope	25-Year Flow Rate (cfs)	25-Year Velocity (ft/s)	25-Year Flow Depth (ft)	25-Year Foude Number	25-Year Velocity Head (ft)	25-Year Energy Head (ft)	25-Year Flow Area (sq. ft.)	25-Year Top Width (ft)
P1	--	--	--	--	--	--	--	--
P2	--	--	--	--	--	--	--	--
P3	--	--	--	--	--	--	--	--
Culvert "1"	--	--	--	--	--	--	--	--
Culvert "2"	--	--	--	--	--	--	--	--
Culvert "3"	--	--	--	--	--	--	--	--
Culvert "4"	--	--	--	--	--	--	--	--
Culvert "5"	--	--	--	--	--	--	--	--
Culvert "6"	--	--	--	--	--	--	--	--
Culvert "7"	--	--	--	--	--	--	--	--

DETENTION POND OUTLET STRUCTURE AND CULVERT EROSION PROTECTION CALCULATIONS

2. Flow through the Low Water Outlet

The flow rate through the low water outlet (LWO) is summarized below.

Flow Structure	Pond Bottom Elev (ft-msl)	LWO Invert Elev.		LWO Diameter (in)	25-Year Flow Rate ² (cfs)	25-Year Outlet Velocity ¹ (ft/s)
		Upstream (ft-msl)	Downstream (ft-msl)			
P1	454.00	454.00	453.00	24	28.0	9.23
P2	454.00	454.00	452.60	2-36	59.0	10.60
P3	453.00	453.00	452.35	36	53.0	7.36
Culvert "1"	457.70	457.70	454.00	24	21.0	6.68
Culvert "2"	455.70	455.70	453.80	3-48	87.0	13.83
Culvert "3"	454.30	454.30	454.00	4-48	68.8	5.95
Culvert "4"	457.00	457.00	455.70	36	17.0	2.41
Culvert "5"	459.00	459.00	458.50	24	15.0	6.41
Culvert "6"	456.00	456.00	455.50	36	30.0	6.89
Culvert "7"	453.10	453.10	452.80	4-48	97.3	7.74

¹ Velocities through the low water outlet for P1, P2, and P3 were calculated using the HYDROCALC HYDRAULICS FOR WINDOWS program developed by Dodson and Associates (Version 1.2a, 1996). All other low water outlet velocities are provided in the HEC-RAS output file included in Appendix III-F-A.

² The flowrates for all low water outlets are the peak discharges for the respective areas as calculated by HEC-1 since the spillway crest is not overtopped in the 25-year event. Flowrates shown for P2, Culvert 2, Culvert 3, and Culvert 7 are the flow in each pipe of the culvert system. The total 25-year flowrate discharging from P2 is 118 cfs / 2 pipes = 59 cfs, from Culvert 2 = 261 cfs / 3 pipes = 87 cfs, from Culvert 3 = 275 cfs / 4 pipes = 68.8 cfs, and from Culvert 7 is 389 cfs / 4 pipes = 97.3 cfs.

The velocity through the low water outlet is larger than the velocity over the spillway, when there is a low water outlet present. The flowrate through the low water outlet is used to design the riprap apron.

The nomograph used for design of the length of the riprap and the median diameter are shown on page III-F-11 (Figure 5.25).

The minimum riprap length and diameter for each outlet is summarized below. The length of the riprap is increased by 20 percent to provide for a conservative design.

Pond	Riprap Design Flowrate (cfs)	Pipe Diameter (in)	Riprap Length (ft)	Adjusted Length L x 1.2 (ft)	Median Rock Diameter (ft)
P1	28.0	24	28	34	1.65
P2	59.0	2-36	18	22	1.40
P3	53.0	36	10	12	1.20
Culvert "1"	21.0	24	10	12	1.20
Culvert "2"	87.0	3-48	10	12	1.20
Culvert "3"	68.8	4-48	10	12	1.20
Culvert "4"	17.0	36	10	12	1.20
Culvert "5"	15.0	24	10	12	1.20
Culvert "6"	30.0	36	10	12	1.20
Culvert "7"	97.3	4-48	10	12	1.20

Apron width required for the ponds (e.g., width of erosion protection in outlet channel) are:
 $W_{req} = \text{LWO diameter} + 0.4 * (\text{RipRap Length})$

Pond	W _{req} (ft)	W _{provided} (ft)
P1	17.2	60.0
P2	13.2	202.0
P3	10.0	142.0

The riprap will be provided over the entire width of the spillway of ponds P2 and P3 and the outlet channel downstream of all the spillways/low water outlets.

The median diameter of riprap is intended to determine the minimum diameter of the riprap that will be used. As an alternative, 2-foot thick gabions with a d₅₀ of 6-inches can be used.

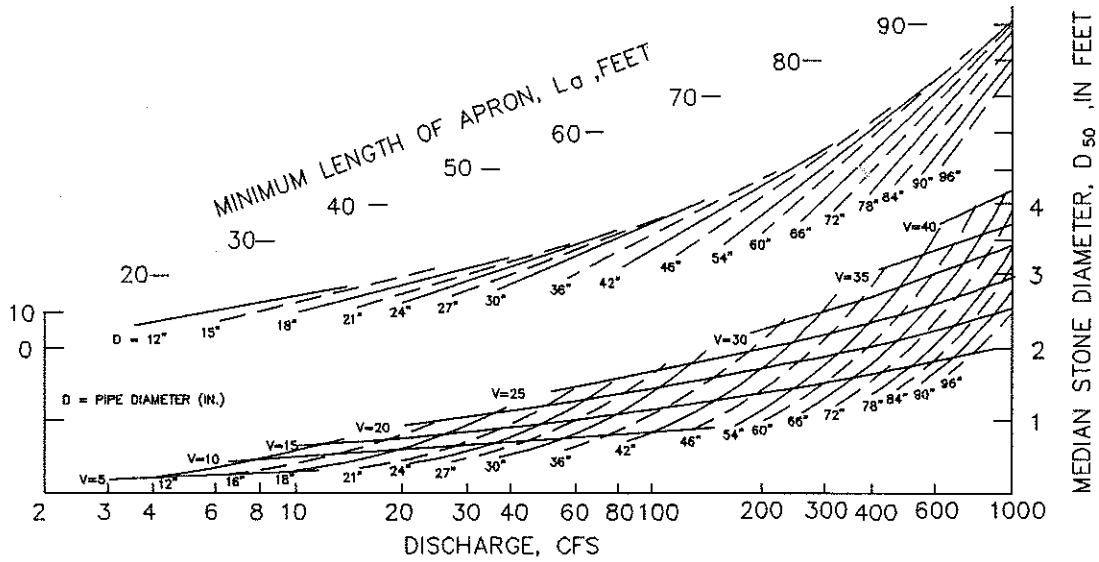


Figure 5.24 Design of outlet protection—minimum tailwater condition, $T_w < 0.5D$ (Environmental Protection Agency, 1976).

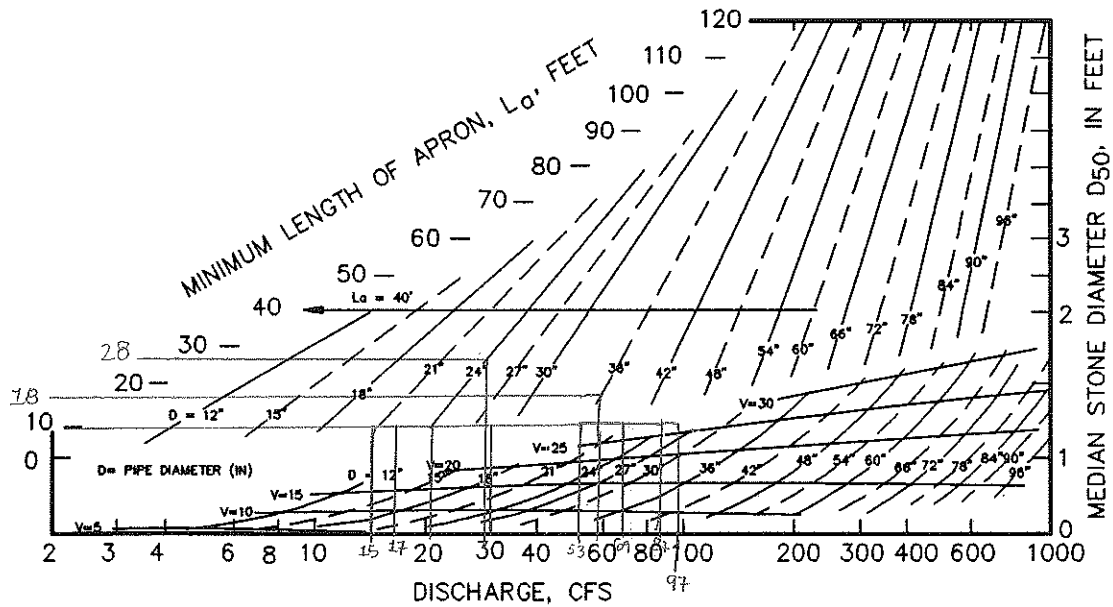


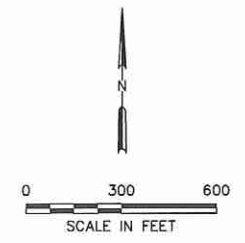
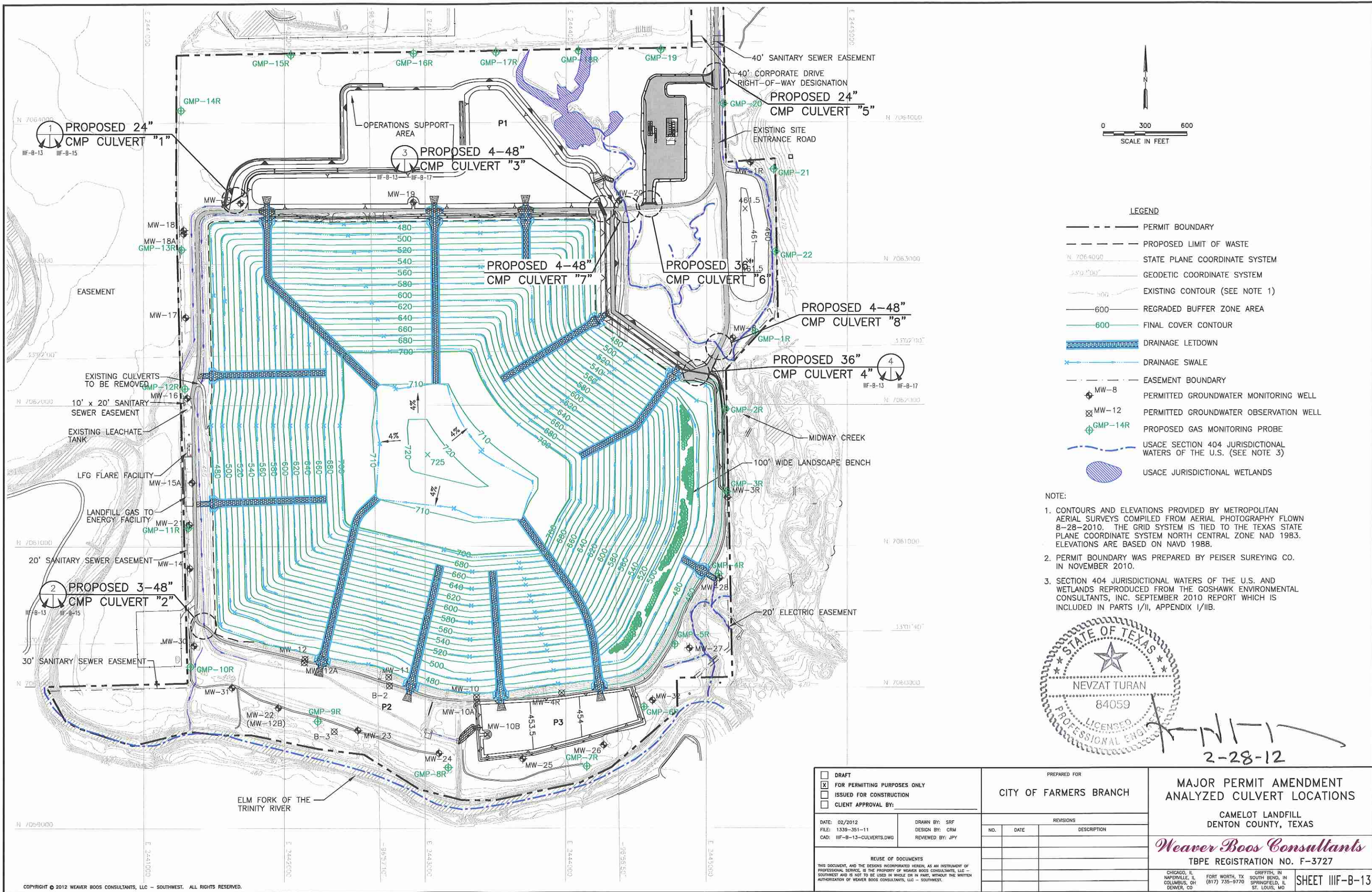
Figure 5.25 Design of outlet protection—maximum tailwater condition, $T_w \geq 0.5D$ (Environmental Protection Agency, 1976).

into the riser 3 ft below its top, what discharge will pass through the four holes with the water level at 1, 2, 4, and 8 ft above the riser? (c) What is the total discharge through the pipe? (d) How might the orifices be sized to provide better stormwater control? (e) Explain whether you would expect two rows (each consisting of four holes) of 8-in.-diameter holes to provide better results? Assume that one row is 2 ft below the riser invert and the other row is 4 ft below the riser invert.

(5.6) A gravel roadway is constructed in a low-lying area such that the roadway is frequently overtopped as a result of severe storms. The roadway is 40 ft wide, and its elevation is 36 ft. (a) If the water level upstream of the roadway is 2 ft above the crest of the roadway, what is the discharge across the roadway? (b) If the roadway is paved, what upstream depth would be required to carry the same flow? (c) Would paving reduce flooding problems?

CULVERT DESIGN

0:\1339\051\EXPANSION 2009\PART III-SPP\IIF-B-13-CULVERT LOCATIONS.dwg, jwilson, 1:2



- LEGEND**
- PERMIT BOUNDARY
 - - - PROPOSED LIMIT OF WASTE
 - N 7064000 STATE PLANE COORDINATE SYSTEM
 - 5392700 GEODETIC COORDINATE SYSTEM
 - EXISTING CONTOUR (SEE NOTE 1)
 - 600 REGRADED BUFFER ZONE AREA
 - 600 FINAL COVER CONTOUR
 - DRAINAGE LETDOWN
 - DRAINAGE SWALE
 - EASEMENT BOUNDARY
 - MW-8 PERMITTED GROUNDWATER MONITORING WELL
 - MW-12 PERMITTED GROUNDWATER OBSERVATION WELL
 - GMP-14R PROPOSED GAS MONITORING PROBE
 - USACE SECTION 404 JURISDICTIONAL WATERS OF THE U.S. (SEE NOTE 3)
 - USACE JURISDICTIONAL WETLANDS

- NOTE:**
- CONTOURS AND ELEVATIONS PROVIDED BY METROPOLITAN AERIAL SURVEYS COMPILED FROM AERIAL PHOTOGRAPHY FLOWN 8-28-2010. THE GRID SYSTEM IS TIED TO THE TEXAS STATE PLANE COORDINATE SYSTEM NORTH CENTRAL ZONE NAD 1983. ELEVATIONS ARE BASED ON NAVD 1988.
 - PERMIT BOUNDARY WAS PREPARED BY PEISER SUREYING CO. IN NOVEMBER 2010.
 - SECTION 404 JURISDICTIONAL WATERS OF THE U.S. AND WETLANDS REPRODUCED FROM THE GOSHAWK ENVIRONMENTAL CONSULTANTS, INC. SEPTEMBER 2010 REPORT WHICH IS INCLUDED IN PARTS I/II, APPENDIX I/II.



[Signature]
2-28-12

<input type="checkbox"/> DRAFT <input checked="" type="checkbox"/> FOR PERMITTING PURPOSES ONLY <input type="checkbox"/> ISSUED FOR CONSTRUCTION <input type="checkbox"/> CLIENT APPROVAL BY:	PREPARED FOR	MAJOR PERMIT AMENDMENT ANALYZED CULVERT LOCATIONS CAMELOT LANDFILL DENTON COUNTY, TEXAS <i>Weaver Boos Consultants</i> TBPE REGISTRATION NO. F-3727 <small>CHICAGO, IL FORT WORTH, TX GRIFFITH, IN NAPERVILLE, IL SOUTH BEND, IN COLUMBUS, OH (817) 735-9770 SPRINGFIELD, IL DENVER, CO ST. LOUIS, MO</small>												
	CITY OF FARMERS BRANCH													
DATE: 02/2012 FILE: 1339-351-11 CAD: IIF-B-13-CULVERTS.DWG	DRAWN BY: SRF DESIGN BY: CRM REVIEWED BY: JPY	REVISIONS <table border="1"> <thead> <tr> <th>NO.</th> <th>DATE</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> </tbody> </table>	NO.	DATE	DESCRIPTION									
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CAMELOT LANDFILL
1339-357-11-02-6B.6
CULVERT DESIGN

Required: Design culverts to convey the flow.

Method: Use HYDROCALC Hydraulics for Windows computer program to determine number and size of the culverts.
Use total 25-year frequency storm event flow estimated by HEC-1 included in Appendix III-F-A.

For proposed 24" CMP culvert at downstream end of Channel "B", Culvert "1"

Total Flow= 21 cfs
No. of Culverts= 1
Culvert Span= -- inches
Culvert Rise= -- inches
Culvert Diameter= 24 inches

Culvert ID	Culvert Span (ft)	Culvert Span (ft)	FHWA Chart Number	FHWA Scale Number	Culvert Diameter (ft)	Manning's Coefficient	Entrance Loss Coefficient	Culvert Length (ft)	Downstream Invert Elevation (ft msl)	Upstream Invert Elevation (ft msl)	Flow Rate (cfs)	Tailwater Depth ² (ft)	Headwater Inlet Control (ft)	Headwater Outlet Control (ft)	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
1	--	--	2	2	2	0.024	0.8	154.8	454.0	457.7	21.0	1.59	3.60	3.01	2.00	1.64	2.00	6.68

- Calculations were performed using the HYDROCALC Hydraulics for Windows program developed by Dodson and Associates (Version 1.2a, 1996).
- Tailwater depth is assumed to be the 25-year, 24-hour storm event flow depth in Channel "C" (see page III-F-B-2 for flow depths).
- Culvert crossing cross sections are shown on Page III-F-B-15.

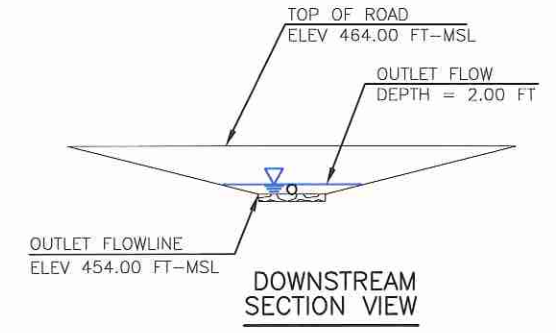
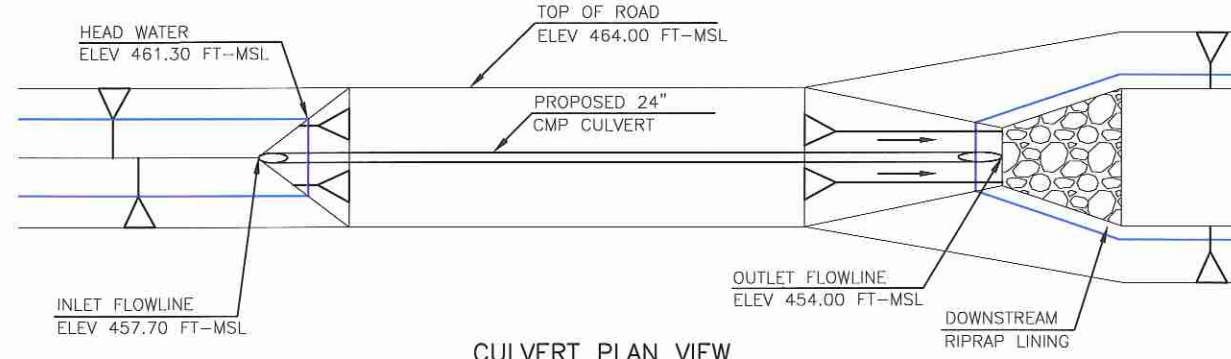
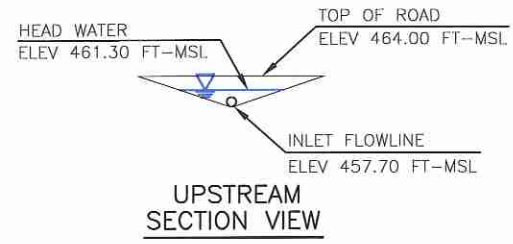
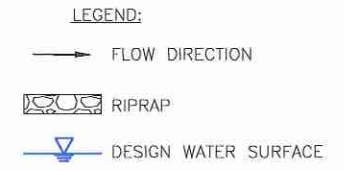
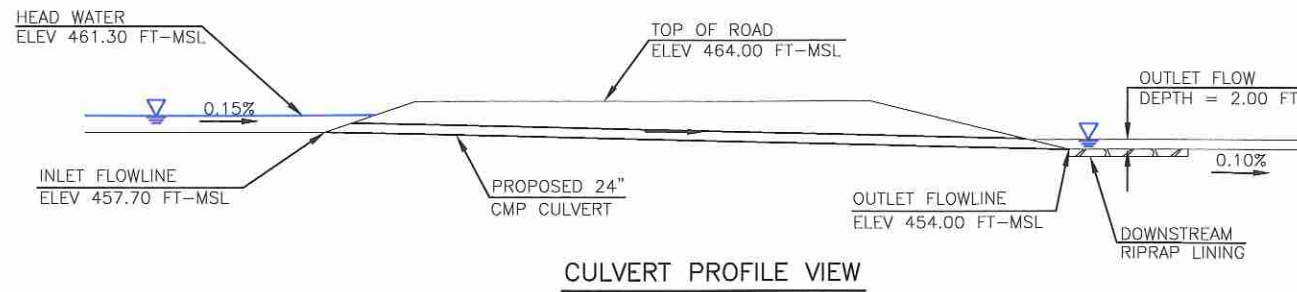
For proposed 3-48" CMP culverts under access road in Channel "D", Culvert "2":

Total Flow= 261 cfs
No. of Culverts= 3
Culvert Span= -- inches
Culvert Rise= -- inches
Culvert Diameter= 48 inches

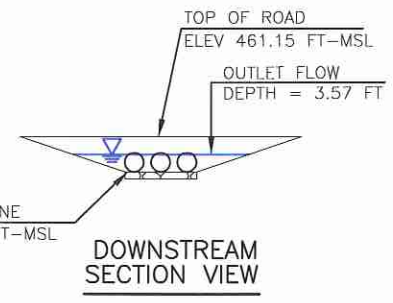
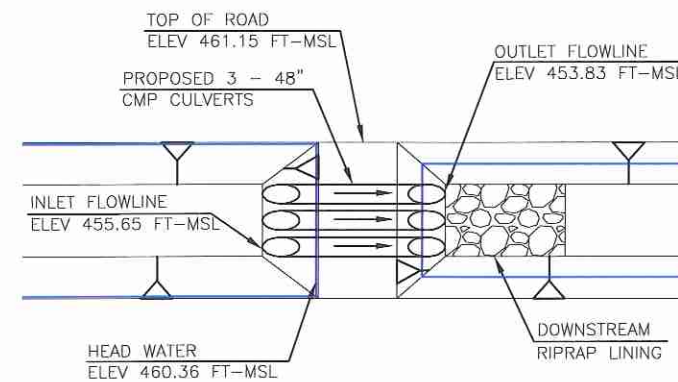
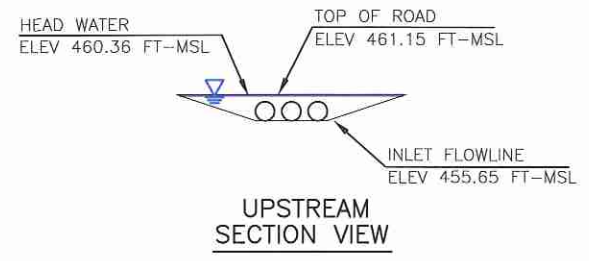
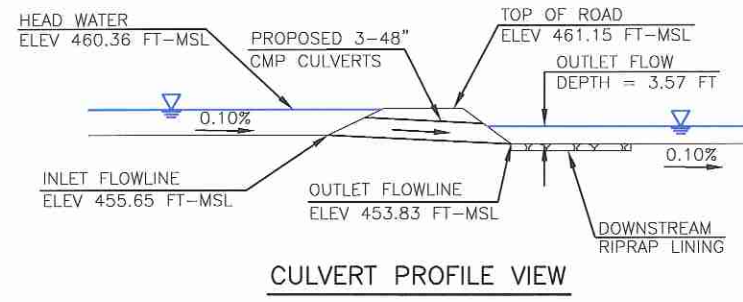
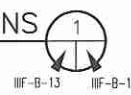
Culvert ID	Culvert Span (ft)	Culvert Span (ft)	FHWA Chart Number	FHWA Scale Number	Culvert Diameter (ft)	Manning's Coefficient	Entrance Loss Coefficient	Culvert Length (ft)	Downstream Invert Elevation (ft msl)	Upstream Invert Elevation (ft msl)	Flow Rate (cfs)	Tailwater Depth ² (ft)	Headwater Inlet Control (ft)	Headwater Outlet Control (ft)	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
2	--	--	2	2	4	0.024	0.8	38.1	453.8	455.7	87.0	3.57	4.71	3.57	2.00	2.83	3.57	13.83

- Calculations were performed using the HYDROCALC Hydraulics for Windows program developed by Dodson and Associates (Version 1.2a, 1996).
- Tailwater depth is assumed to be the 25-year, 24-hour storm event flow depth in Channel "D" downstream of the culvert (see page III-F-B-2 for flow depths).
- Culvert crossing cross sections are shown on Page III-F-B-15.

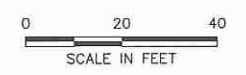
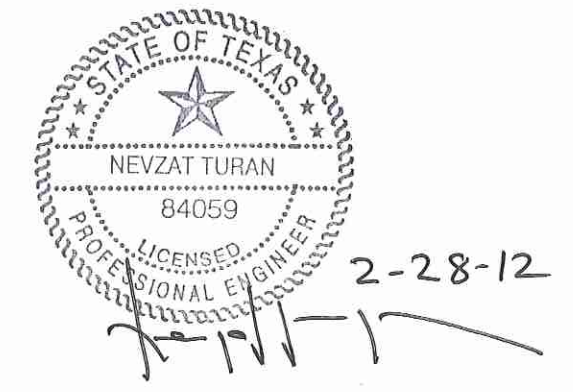
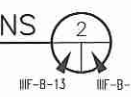
O:\1339\351\EXPANSION 2009\PART III-SDP\III-F\III-F-15-CULVERT CROSS SECTIONS.dwg, jwilson, 1:2



CULVERT "1" SECTIONS



CULVERT "2" SECTIONS



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	CITY OF FARMERS BRANCH										
DATE: 02/2012 FILE: 1339-351-11 CAD: III-F-B-15-CROSS SECTIONS.DWG	DRAWN BY: SRF DESIGN BY: CRM REVIEWED BY: JPY	REVISIONS <table border="1"> <thead> <tr> <th>NO.</th> <th>DATE</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> </tr> </tbody> </table>	NO.	DATE	DESCRIPTION						
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FORT WORTH, TX (817) 735-9770		GRIFFITH, IN SOUTH BEND, IN SPRINGFIELD, IL ST. LOUIS, MO									
SHEET III-F-B-15		SHEET III-F-B-15									

CAMELOT LANDFILL
1339-357-11-02-6B.6
CULVERT DESIGN

For proposed 4'-48" CMP culverts under access road at the downstream end of Channel 'J', Culvert '3':

Total Flow= 275 cfs
No. of Culverts= 4
Culvert Span= -- inches
Culvert Rise= -- inches
Culvert Diameter= 48 inches

Culvert ID	Culvert Span (ft)	FHWA Chart Number	FHWA Scale Number	Culvert Diameter (ft)	Manning's Coefficient	Entrance Loss Coefficient	Culvert Length (ft)	Downstream Invert Elevation (ft msl)	Upstream Invert Elevation (ft msl)	Flow Rate (cfs)	Tailwater Depth ² (ft)	Headwater Inlet Control (ft)	Headwater Outlet Control (ft)	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
3	--	2	2	4	0.024	0.8	101.0	454.0	454.3	68.8	3.46	3.90	4.78	4.00	2.51	3.46	5.95

1. Calculations were performed using the HYDROCALC Hydraulics for Windows program developed by Dodson and Associates (Version 1.2a, 1996).
2. Tailwater depth is assumed to be the 25-year, 24-hour storm event flow depth in Pond P1 (see page III-F-B-3 for Pond flow depths).
3. Culvert crossing cross sections are shown on Page III-F-B-17.

For proposed 36" CMP culvert under access road in Channel 'J', Culvert '4':

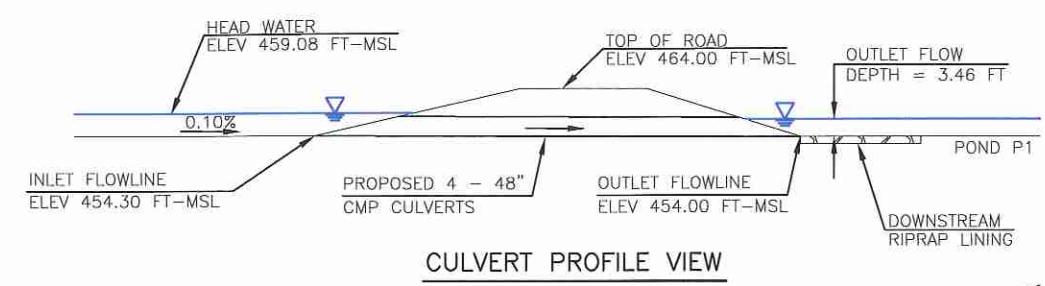
Total Flow= 17 cfs
No. of Culverts= 1
Culvert Span= -- inches
Culvert Rise= -- inches
Culvert Diameter= 36 inches

Culvert ID	Culvert Span (ft)	FHWA Chart Number	FHWA Scale Number	Culvert Diameter (ft)	Manning's Coefficient	Entrance Loss Coefficient	Culvert Length (ft)	Downstream Invert Elevation (ft msl)	Upstream Invert Elevation (ft msl)	Flow Rate (cfs)	Tailwater Depth ² (ft)	Headwater Inlet Control (ft)	Headwater Outlet Control (ft)	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
4	--	2	2	3	0.024	0.8	189.8	455.7	457.0	17.0	4.06	1.93	3.34	1.62	1.32	3.00	2.41

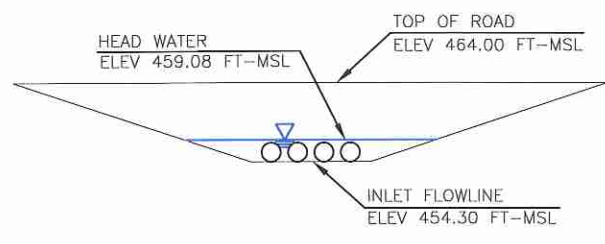
1. Calculations were performed using the HYDROCALC Hydraulics for Windows program developed by Dodson and Associates (Version 1.2a, 1996).
2. Tailwater depth is assumed to be the 25-year, 24-hour storm event flow depth in Channel 'J' downstream of the culvert (see page III-F-B-2 for flow depths).
3. Culvert crossing cross sections are shown on Page III-F-B-17.

O:\1339\351\EXPANSION 2009\PART III-SDP\III-B-17-CULVERT CROSS SECTIONS.dwg, jwilson, 1:2

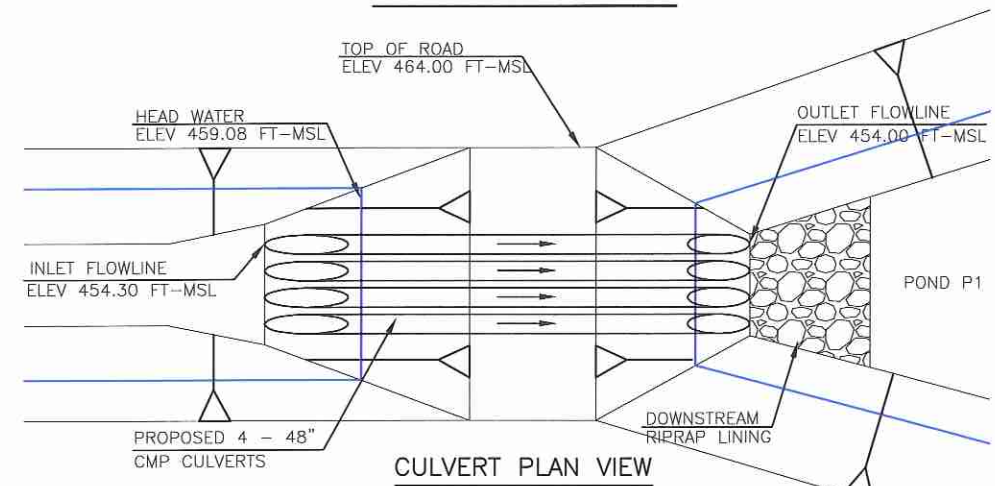
LEGEND:
 FLOW DIRECTION
 RIPRAP
 DESIGN WATER SURFACE



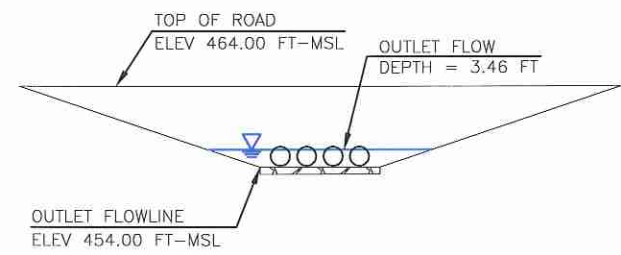
CULVERT PROFILE VIEW



UPSTREAM SECTION VIEW

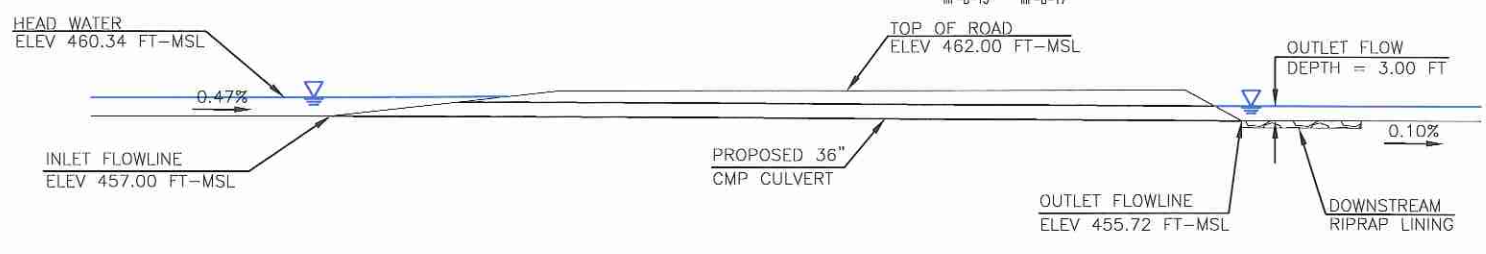


CULVERT PLAN VIEW

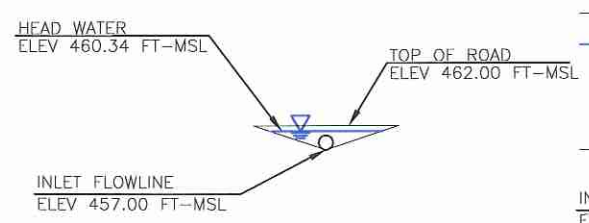


DOWNSTREAM SECTION VIEW

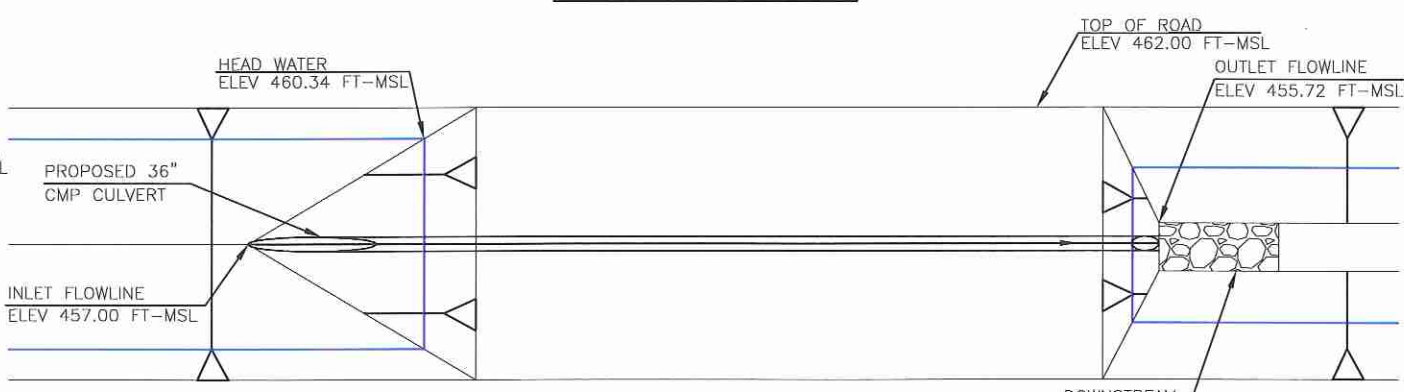
CULVERT "3" SECTIONS



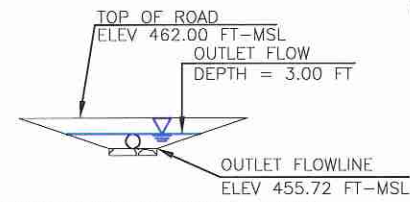
CULVERT PROFILE VIEW



UPSTREAM SECTION VIEW



CULVERT PLAN VIEW

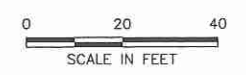


DOWNSTREAM SECTION VIEW

CULVERT "4" SECTIONS



(Handwritten Signature)
 2-28-12



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	DATE: 02/2012 FILE: 1339-351-11 CAD: III-B-17-CROSS SECTIONS.DWG		REVISIONS <table border="1"> <thead> <tr> <th>NO.</th> <th>DATE</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> </tbody> </table>	NO.	DATE	DESCRIPTION							
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		GRIFITH, IN SOUTH BEND, IN SPRINGFIELD, IL ST. LOUIS, MO											

CAMELOT LANDFILL
1339-357-11-02-6B.6
CULVERT DESIGN

For proposed 24" CMP culverts under entrance facility access road, Culvert "5":

Total Flow= 15.2 cfs
No. of Culverts= 1
Culvert Span= 24 inches
Culvert Rise= 24 inches
Culvert Diameter= 24 inches

Culvert ID	Culvert Span (ft)	Culvert Span (ft)	FHWA Chart Number	FHWA Scale Number	Culvert Diameter (ft)	Manning's Coefficient	Entrance Loss Coefficient	Culvert Length (ft)	Downstream Invert Elevation (ft msl)	Upstream Invert Elevation (ft msl)	Flow Rate (cfs)	Tailwater Depth ³ (ft)	Headwater Inlet Control ⁴ (ft)	Headwater Outlet Control ⁴ (ft)	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
5	24	24	2	2	2	0.024	0.8	101.0	458.5	459.0	15.0	0.00	2.25	2.95	2.00	1.40	1.40	6.41

1. Calculations were performed using the HYDROCALC Hydraulics for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

2. Flow rate is an estimated portion of the total peak flow rate of Drainage Area S4 (see Appendix III-F-A).

3. There is no assumed tailwater depth due to the geometry downstream of the culvert.

4. Culvert calculations are performed to show that installation of the culvert will not cause overtopping of the road. The road elevation is 462.00, which gives 3.00 feet of available headwater.

For proposed 36" CMP culverts under entrance facility access road, Culvert "6":

Total Flow= 30.2 cfs
No. of Culverts= 1
Culvert Span= 36 inches
Culvert Rise= 36 inches
Culvert Diameter= 36 inches

Culvert ID	Culvert Span (ft)	Culvert Span (ft)	FHWA Chart Number	FHWA Scale Number	Culvert Diameter (ft)	Manning's Coefficient	Entrance Loss Coefficient	Culvert Length (ft)	Downstream Invert Elevation (ft msl)	Upstream Invert Elevation (ft msl)	Flow Rate (cfs)	Tailwater Depth ³ (ft)	Headwater Inlet Control ⁴ (ft)	Headwater Outlet Control ⁴ (ft)	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
6	36	36	2	2	3	0.024	0.8	101.1	455.5	456.0	30.0	0.00	2.73	3.13	3.00	1.77	1.77	6.89

1. Calculations were performed using the HYDROCALC Hydraulics for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

2. Flow rate is an estimated portion of the total peak flow rate of Drainage Area S4 (see Appendix III-F-A).

3. There is no assumed tailwater depth due to the geometry downstream of the culvert.

4. Culvert calculations are performed to show that installation of the culvert will not cause overtopping of the road. The road elevation is 462.00, which gives 6.00 feet of available headwater.

CAMELOT LANDFILL
1339-357-11-02-6B.6
CULVERT DESIGN

For proposed 4-48" CMP culverts under access road in Channel "N", Culvert "7":

Total Flow= 389 cfs
No. of Culverts= 4
Culvert Span= -- inches
Culvert Rise= -- inches
Culvert Diameter= 48 inches

Culvert ID	Culvert Span (ft)	FHWA Chart Number	FHWA Scale Number	Culvert Diameter (ft)	Manning's Coefficient	Entrance Loss Coefficient	Culvert Length (ft)	Downstream Invert Elevation (ft msl)	Upstream Invert Elevation (ft msl)	Flow Rate (cfs)	Tailwater Depth ² (ft)	Headwater Inlet Control ³ (ft)	Headwater Outlet Control ³ (ft)	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
7	--	2	2	4	0.024	0.8	72.3	452.8	453.1	97.3	2.26	5.69	5.01	4.00	2.99	4.00	7.74

- Calculations were performed using the HYDROCALC Hydraulics for Windows program developed by Dodson and Associates (Version 1.2a, 1996).
- Tailwater depth is assumed to be the 25-year, 24-hour storm event flow depth in Channel "N" downstream of the culvert (see page IIF-B-2 for flow depths).
- Culvert calculations are performed to show that installation of the culvert will not cause overtopping of the road. The road elevation is 459.00, which gives 6.9 feet of available headwater.

For proposed 4-48" CMP culverts under access road at south end of Channel "N", Culvert "8":

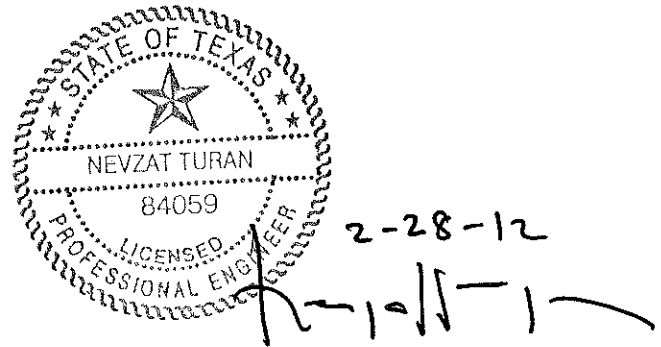
Total Flow= 426 cfs
No. of Culverts= 4
Culvert Span= -- inches
Culvert Rise= -- inches
Culvert Diameter= 48 inches

Culvert ID	Culvert Span (ft)	FHWA Chart Number	FHWA Scale Number	Culvert Diameter (ft)	Manning's Coefficient	Entrance Loss Coefficient	Culvert Length (ft)	Downstream Invert Elevation (ft msl)	Upstream Invert Elevation (ft msl)	Flow Rate (cfs)	Tailwater Depth ² (ft)	Headwater Inlet Control ³ (ft)	Headwater Outlet Control ³ (ft)	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
8	--	2	2	4	0.024	0.8	90.5	452.0	452.3	106.5	2.26	6.33	5.85	4.00	3.12	4.00	8.48

- Calculations were performed using the HYDROCALC Hydraulics for Windows program developed by Dodson and Associates (Version 1.2a, 1996).
- Tailwater depth is assumed to be the 25-year, 24-hour storm event flow depth in Channel "N" downstream of the culvert (see page IIF-B-2 for flow depths).
- Culvert calculations are performed to show that installation of the culvert will not cause overtopping of the road. The road elevation is 460.00, which gives 7.7 feet of available headwater.

APPENDIX IIIF-C

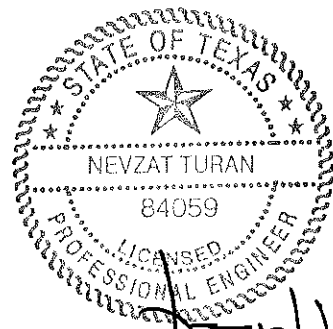
FINAL COVER EROSION CONTROL STRUCTURE DESIGN



Includes pages IIIF-C-1 through IIIF-C-18

CONTENTS

Drainage Swale Design	IIIF-C-1
Drainage Letdown (or Chute) Design	IIIF-C-8

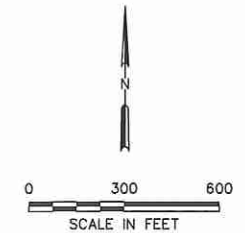
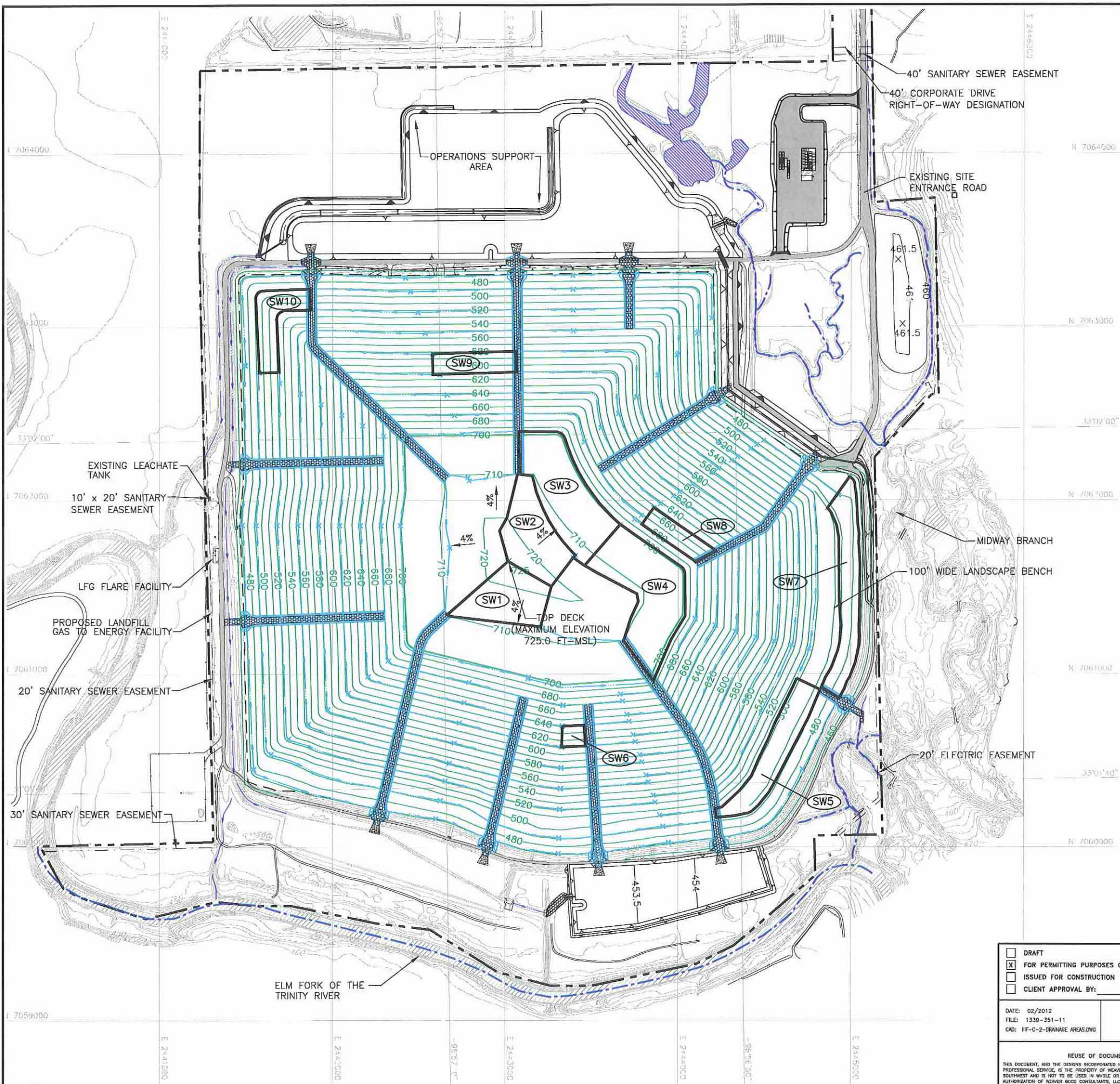


2-28-12

DRAINAGE SWALE DESIGN

- The drainage swale layout is shown on Drawing IIIF.1 – Drainage Structure Plan. A swale detail is provided on Drawing IIIF.9 – Drainage Details.
- Typical Swale Design Summary:
 - Typical swale drainage areas analyzed are shown on sheet IIIF-C-2.
 - Hydraulic calculations are summarized on page IIIF-C-5.
 - Maximum normal depth is 1.59 feet (Drainage Area SW7).
 - Maximum flow velocity is 2.89 fps (Drainage Area SW7).
 - Vegetation will be established on the swales to protect against erosion.
 - Typical swale drainage areas were selected such that all slope conditions (4% and 25%) are included in this analysis. Additionally, swales with large individual drainage areas and short and long swale lengths are included in this analysis.

O:\1339\351\EXPANSION 2009\PART III-SWP\III-C-2-SWALE DRAINAGE AREAS.dwg, jwilson, 1:2



- LEGEND**
- PERMIT BOUNDARY
 - - - PROPOSED LIMIT OF WASTE
 - N 7064000 STATE PLANE COORDINATE SYSTEM
 - 33°02'00" GEODETIC COORDINATE SYSTEM
 - 500 EXISTING CONTOUR (SEE NOTE 1)
 - 600 REGRADED BUFFER ZONE AREA
 - 600 PROPOSED FINAL COVER CONTOUR
 - PROPOSED LETDOWN STRUCTURE
 - DRAINAGE SWALE
 - USACE SECTION 404 JURISDICTIONAL WATERS OF THE U.S. (SEE NOTE 3)
 - USACE JURISDICTIONAL WETLANDS
 - SW1 TYPICAL SWALE DRAINAGE AREA DESIGNATION
 - TYPICAL SWALE DRAINAGE AREA BOUNDARY

- NOTE:**
- CONTOURS AND ELEVATIONS PROVIDED BY METROPOLITAN AERIAL SURVEYS COMPILED FROM AERIAL PHOTOGRAPHY FLOWN 8-28-2010. THE GRID SYSTEM IS TIED TO THE TEXAS STATE PLANE COORDINATE SYSTEM NORTH CENTRAL ZONE NAD 1983. ELEVATIONS ARE BASED ON NAVD 1988.
 - MAXIMUM FINAL COVER ELEVATION IS 725 FT-MSL. MAXIMUM TOP OF WASTE ELEVATION IS 721.5 FT-MSL.
 - SECTION 404 JURISDICTIONAL WATERS OF THE U.S. AND WETLANDS REPRODUCED FROM THE GOSHAWK ENVIRONMENTAL CONSULTANTS, INC. SEPTEMBER 2010 REPORT WHICH IS INCLUDED IN PARTS I/II, APPENDIX I/II/B.



TYPICAL SWALE DRAINAGE AREA DESIGNATION	AREA (ACRES)
SW1	3.01
SW2	3.40
SW3	5.01
SW4	5.59
SW5	3.01
SW6	0.36
SW7	3.38
SW8	1.12
SW9	1.34
SW10	1.80

<input type="checkbox"/> DRAFT	<input checked="" type="checkbox"/> FOR PERMITTING PURPOSES ONLY
<input type="checkbox"/> ISSUED FOR CONSTRUCTION	<input type="checkbox"/> CLIENT APPROVAL BY:
DATE: 02/2012	DRAWN BY: SRF
FILE: 1339-351-11	DESIGN BY: CRM
CAD: IIF-C-2-DRAINAGE AREAS.DWG	REVIEWED BY: JPY
REUSE OF DOCUMENTS	
THIS DOCUMENT, AND THE DESIGNS INCORPORATED HEREIN, AS AN INSTRUMENT OF PROFESSIONAL SERVICE, IS THE PROPERTY OF WEAVER BOOS CONSULTANTS, LLC. SOUTHWEST AND IS NOT TO BE USED IN WHOLE OR IN PART, WITHOUT THE WRITTEN AUTHORIZATION OF WEAVER BOOS CONSULTANTS, LLC - SOUTHWEST.	

PREPARED FOR		
CITY OF FARMERS BRANCH		
REVISIONS		
NO.	DATE	DESCRIPTION

**MAJOR PERMIT AMENDMENT
TYPICAL SWALE DRAINAGE AREAS**

CAMELOT LANDFILL
DENTON COUNTY, TEXAS

Weaver Boos Consultants
TBPE REGISTRATION NO. F-3727

CHICAGO, IL	FORT WORTH, TX	GRIFITH, IN
NAPERVILLE, IL	(817) 735-9770	SOUTH BEND, IN
COLUMBUS, OH		SPRINGFIELD, IL
DENVER, CO		ST. LOUIS, MO

SHEET IIF-C-2

Required: Analyze typical swales to determine the adequacy of the swale design.

Method: 1. Determine the 25-year, 24-hour flow rates for the typical swale drainage areas (see sheet IIIIF-C-2) by the Rational Method.

Reference: 1. State of Texas, Department of Transportation, Bridge Division, Hydraulic Design Manual, April 2002.

Solution: 1. Determine the 25-year intensity flow rates.

$$Q = CIA$$

Where: C= 0.7 (runoff coefficient, Ref 1.)
I = intensity in/hr
A= drainage area, ac

$$I = \frac{b}{(t_c + d)^e}$$

b = 90 From Ref 1, for Denton County
d = 8.5 25-year storm event
e = 0.781
t_c is assumed to be 10 min.

$$I = 9.22 \text{ in/hr}$$

Swale	Area (ac)	Flow Rate (cfs)
SW1	3.01	19.4
SW2	3.40	21.9
SW3	5.01	32.3
SW4	5.59	36.1
SW5	3.01	19.4
SW6	0.36	2.3
SW7	3.38	21.8
SW8	1.12	7.2
SW9	1.34	8.6
SW10	1.80	11.6

Rainfall Intensity-Duration-Frequency Coefficients for Texas Counties

County name	2-year				5-year				10-year				25-year				50-year				100-year																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
	a	b	d	e	a	b	d	e	a	b	d	e	a	b	d	e	a	b	d	e	a	b	d	e																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																															
Davison	0.820	1118	10.0	0.818	1489	10.4	0.814	1727	10.4	0.807	1956	10.4	0.801	2184	10.4	0.800	2438	10.0	0.809	2769	2362	2591	10.0	0.798	2982	2616	2844	10.0	0.799	3277	2870	3109	2903	3142	10.0	0.799	3589	3277	3516	10.0	0.799	3897	3585	3824	10.0	0.799	4195	3873	4112	10.0	0.799	4493	4161	4399	10.0	0.799	4791	4449	4686	10.0	0.799	5089	4737	4974	10.0	0.799	5387	5025	5262	10.0	0.799	5685	5313	5550	10.0	0.799	5983	5601	5838	10.0	0.799	6281	5889	6126	10.0	0.799	6579	6177	6414	10.0	0.799	6877	6465	6702	10.0	0.799	7175	6753	6990	10.0	0.799	7473	7041	7278	10.0	0.799	7771	7329	7566	10.0	0.799	8069	7617	7854	10.0	0.799	8367	7905	8142	10.0	0.799	8665	8193	8430	10.0	0.799	8963	8481	8718	10.0	0.799	9261	8769	9006	10.0	0.799	9559	9057	9294	10.0	0.799	9857	9345	9582	10.0	0.799	10155	9633	9870	10.0	0.799	10453	9921	10158	10.0	0.799	10751	10209	10446	10.0	0.799	11049	10497	10734	10.0	0.799	11347	10785	11022	10.0	0.799	11645	11073	11310	10.0	0.799	11943	11361	11598	10.0	0.799	12241	11649	11886	10.0	0.799	12539	11937	12174	10.0	0.799	12837	12225	12462	10.0	0.799	13135	12513	12750	10.0	0.799	13433	12801	13038	10.0	0.799	13731	13089	13326	10.0	0.799	14029	13377	13614	10.0	0.799	14327	13665	13902	10.0	0.799	14625	13953	14190	10.0	0.799	14923	14241	14478	10.0	0.799	15221	14529	14766	10.0	0.799	15519	14817	15054	10.0	0.799	15817	15105	15342	10.0	0.799	16115	15393	15630	10.0	0.799	16413	15681	15918	10.0	0.799	16711	15969	16206	10.0	0.799	17009	16267	16504	10.0	0.799	17307	16555	16792	10.0	0.799	17605	16843	17080	10.0	0.799	17903	17131	17368	10.0	0.799	18201	17419	17656	10.0	0.799	18499	17707	17944	10.0	0.799	18797	17995	18232	10.0	0.799	19095	18283	18520	10.0	0.799	19393	18571	18808	10.0	0.799	19691	18859	19096	10.0	0.799	19989	19147	19384	10.0	0.799	20287	19435	19672	10.0	0.799	20585	19723	19960	10.0	0.799	20883	20011	20248	10.0	0.799	21181	20299	20536	10.0	0.799	21479	20587	20824	10.0	0.799	21777	20875	21112	10.0	0.799	22075	21163	21400	10.0	0.799	22373	21451	21688	10.0	0.799	22671	21739	21976	10.0	0.799	22969	22027	22264	10.0	0.799	23267	22315	22552	10.0	0.799	23565	22603	22840	10.0	0.799	23863	22891	23128	10.0	0.799	24161	23179	23416	10.0	0.799	24459	23467	23704	10.0	0.799	24757	23755	23992	10.0	0.799	25055	24043	24280	10.0	0.799	25353	24331	24568	10.0	0.799	25651	24619	24856	10.0	0.799	25949	24907	25144	10.0	0.799	26247	25195	25432	10.0	0.799	26545	25483	25720	10.0	0.799	26843	25771	26008	10.0	0.799	27141	26059	26296	10.0	0.799	27439	26347	26584	10.0	0.799	27737	26635	26872	10.0	0.799	28035	26923	27160	10.0	0.799	28333	27211	27448	10.0	0.799	28631	27499	27736	10.0	0.799	28929	27787	28024	10.0	0.799	29227	28075	28312	10.0	0.799	29525	28363	28600	10.0	0.799	29823	28651	28888	10.0	0.799	30121	28939	29176	10.0	0.799	30419	29227	29464	10.0	0.799	30717	29515	29752	10.0	0.799	31015	29803	30040	10.0	0.799	31313	30091	30328	10.0	0.799	31611	30379	30616	10.0	0.799	31909	30667	30904	10.0	0.799	32207	30955	31192	10.0	0.799	32505	31243	31480	10.0	0.799	32803	31531	31768	10.0	0.799	33101	31819	32056	10.0	0.799	33400	32107	32344	10.0	0.799	33698	32395	32632	10.0	0.799	33996	32683	32920	10.0	0.799	34294	32971	33208	10.0	0.799	34592	33259	33496	10.0	0.799	34890	33547	33784	10.0	0.799	35188	33835	34072	10.0	0.799	35486	34123	34360	10.0	0.799	35784	34411	34648	10.0	0.799	36082	34699	34936	10.0	0.799	36380	34987	35224	10.0	0.799	36678	35275	35512	10.0	0.799	36976	35563	35800	10.0	0.799	37274	35851	36088	10.0	0.799	37572	36139	36376	10.0	0.799	37870	36427	36664	10.0	0.799	38168	36715	36952	10.0	0.799	38466	37003	37240	10.0	0.799	38764	37291	37528	10.0	0.799	39062	37579	37816	10.0	0.799	39360	37867	38104	10.0	0.799	39658	38155	38392	10.0	0.799	39956	38443	38680	10.0	0.799	40254	38731	38968	10.0	0.799	40552	39019	39256	10.0	0.799	40850	39307	39544	10.0	0.799	41148	39595	39832	10.0	0.799	41446	39883	40120	10.0	0.799	41744	40171	40408	10.0	0.799	42042	40459	40696	10.0	0.799	42340	40747	40984	10.0	0.799	42638	41035	41272	10.0	0.799	42936	41323	41560	10.0	0.799	43234	41611	41848	10.0	0.799	43532	41899	42136	10.0	0.799	43830	42097	42334	10.0	0.799	44128	42385	42622	10.0	0.799	44426	42673	42910	10.0	0.799	44724	42961	43198	10.0	0.799	45022	43249	43486	10.0	0.799	45320	43537	43774	10.0	0.799	45618	43825	44062	10.0	0.799	45916	44113	44350	10.0	0.799	46214	44401	44638	10.0	0.799	46512	44689	44926	10.0	0.799	46810	44977	45214	10.0	0.799	47108	45265	45502	10.0	0.799	47406	45553	45790	10.0	0.799	47704	45841	46078	10.0	0.799	48002	46129	46366	10.0	0.799	48300	46417	46654	10.0	0.799	48598	46705	46942	10.0	0.799	48896	46993	47230	10.0	0.799	49194	47281	47518	10.0	0.799	49492	47569	47806	10.0	0.799	49790	47857	48094	10.0	0.799	50088	48145	48382	10.0	0.799	50386	48433	48670	10.0	0.799	50684	48721	48958	10.0	0.799	50982	49009	49246	10.0	0.799	51280	49297	49534	10.0	0.799	51578	49585	49822	10.0	0.799	51876	49873	50110	10.0	0.799	52174	50161	50398	10.0	0.799	52472	50449	50686	10.0	0.799	52770	50737	50974	10.0	0.799	53068	51025	51262	10.0	0.799	53366	51313	51550	10.0	0.799	53664	51601	51838	10.0	0.799	53962	51889	52126	10.0	0.799	54260	52087	52324	10.0	0.799	54558	52375	52612	10.0	0.799	54856	52663	52900	10.0	0.799	55154	52951	53188	10.0	0.799	55452	53239	53476	10.0	0.799	55750	53527	53764	10.0	0.799	56048	53815	54052	10.0	0.799	56346	54103	54340	10.0	0.799	56644	54391	54628	10.0	0.799	56942	54679	54916	10.0	0.799	57240	54967	55204	10.0	0.799	57538	55255	55492	10.0	0.799	57836	55543	55780	10.0	0.799	58134	55831	56068	10.0	0.799	58432	56119	56356	10.0	0.799	58730	56407	56644	10.0	0.799	59028	56695	56932	10.0	0.799	59326	56983	57220	10.0	0.799	59624	57271	57508	10.0	0.799	59922	57559	57796	10.0	0.799	60220	57847	58084	10.0	0.799	60518	58135	58372	10.0	0.799	60816	58423	58660	10.0	0.799	61114	58711	58948	10.0	0.799	61412	59000	59236	10.0	0.799	61710	59288	59525	10.0	0.799	62008	59576	59813	10.0	0.799	62306	59864	60101	10.0	0.799	62604	60152	60389	10.0	0.799	62902	60440	60677	10.0	0.799	63200	60728	60965	10.0	0.799	63498	61016	61253	10.0	0.799	63796	61304	61541	10.0	0.799	64094	61592	61829	10.0	0.799	64392	61880	62117	10.0	0.799	64690	62168	62405	10.0	0.799	64988	62466	62703	10.0	0.799	65286	62754	62991	10.0	0.799	65584	63042	63279	10.0	0.799	65882	63330	63567	10.0	0.799	66180	63618	63855	10.0	0.799	66478	63906	64143	10.0	0.799	66776	64194	64431	10.0	0.799	67074	64482	64719	10.0	0.799	67372	64770	65007	10.0	0.799	67670	65058	65295	10.0	0.799	67968	65346	65583	10.0	0.799	68266	65634	65871	10.0	0.799	68564	65922	66159	10.0	0.799	68862	66210	66447	10.0	0.799	69160	66498	66735	10.0	0.799	69458	66786	67023	10.0	0.799	69756	67074	67311	10.0	0.799	70054	67362	67599	10.0	0.799	70352	67650	67887	10.0	0.799	70650	67938	68175	10.0	0.799	70948	68226	68463	10.0	0.799	71246	68514	68751	10.0	0.799	71544	68802	69039	10.0	0.799	71842	69090	69327	10.0	0.799	72140	69378	69615	10.0	0.799	72438	69666	69903	10.0	0.799	72736	69954	70191	10.0	0.799	73034	70242	70479	10.0	0.799	73332	70530	70767	10.0	0.799	73630	70818	71055	10.0	0.799	73928	71106	71343	10.0	0.799	74226	71394	71631	10.0	0.799	74524	71682	71919	10.0	0.799	74822	71970	72207	10.0	0.799	75120	72258	72495

Prep By: CRM
Date: 2/21/2012

CAMELOT LANDFILL
1339-351-11-02
SWALE ANALYSIS

Chkd By: REE
Date: 2-29-12

Swale	Flow Rate (cfs)	Bottom Slope (ft/ft)	n-value	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)	Froude No.	Velocity Head (ft)	Energy Head (ft)	Flow Area (sq. ft.)	Top Width of Flow (ft)
SW1	19.4	0.005	0.03	2	25	0	0.85	1.97	0.531	0.06	0.91	9.86	23.07
SW2	21.9	0.005	0.03	2	25	0	0.89	2.03	0.535	0.06	0.96	10.79	24.13
SW3	32.3	0.005	0.03	2	25	0	1.03	2.24	0.549	0.08	1.11	14.43	27.92
SW4	36.1	0.005	0.03	2	25	0	1.08	2.31	0.554	0.08	1.16	15.65	29.07
SW5	19.4	0.005	0.03	2	4	0	1.52	2.81	0.568	0.12	1.64	6.91	9.11
SW6	2.3	0.005	0.03	2	4	0	0.68	1.65	0.498	0.04	0.72	1.40	4.09
SW7	21.8	0.005	0.03	2	4	0	1.59	2.89	0.572	0.13	1.72	7.55	9.52
SW8	7.2	0.005	0.03	2	4	0	1.05	2.18	0.532	0.07	1.12	3.30	6.29
SW9	8.6	0.005	0.03	2	4	0	1.12	2.29	0.540	0.08	1.20	3.75	6.71
SW10	11.6	0.005	0.03	2	4	0	1.25	2.46	0.549	0.09	1.35	4.71	7.52

Note: Calculations were performed using the HYDROCALC HYDRAULICS program developed by Dodson and Associates (Version 1.2a, 1996).

Maximum flow depth is 1.59 ft < 2.0 ft (swale height).

Design is okay.

Example Calculation: Calculate the normal depth for the swale for drainage area SW3 (see sheet IIIF-C-2).

List of Symbols

- Q_d = design flow rate for channel, cfs
- R = hydraulic radius, ft
- n = Manning's roughness coefficient
- S = channel slope, ft/ft
- b = bottom width of channel, ft
- z_r = z-ratio (ratio of run to rise for channel sideslope) for right sideslope of swale
- z_l = z-ratio (ratio of run to rise for channel sideslope) for left sideslope of swale
- A_f = flow area, sf
- g = gravitational acceleration = 32.2 ft/s²
- T = top width of flow, ft
- d = normal depth of swale, ft

The program uses an iterative process to calculate the normal depth of the swale to satisfy Manning's Equation

$$Q = \frac{1.486}{n} A R^{0.67} S^{0.5}$$

Design Inputs:	$Q_d =$	32.3	cfs (from page IIIF-C-3)
	$S =$	0.005	ft/ft
	$b =$	0	ft
	$z_r =$	2	(H) : 1 (V)
	$z_l =$	25	(H) : 1 (V)
	$n =$	0.03	

Step 1 - Based on the geometry of the swale cross-section, solve for R and A_f

$$R = \frac{bd + 1/2d^2(z_r + z_l)}{b + d((z_l^2 + 1)^{0.5} + (z_r^2 + 1))}$$

$$A_f = bd + 1/2d^2(z_r + z_l)$$

assume: $d = 1.03$ ft

$R = 0.510$ ft

$A_f = 14.43$ sf

solve for Q: $Q = 32.3$

if Q is not equal to Q_d , select a new d and repeat calculations

Step 2 - solve for velocity, T, Froude number, velocity head, and energy head

$$Q = VA \Rightarrow V = Q/A$$

$$V = 2.24 \text{ ft/s}$$

$$T = b + d(z_1 + z_r)$$

$$T = 27.92 \text{ ft}$$

$$F_r = \frac{V}{(gA/T)^{0.5}}$$

$$F_r = 0.549$$

$$\text{Velocity Head} = \frac{V^2}{2g}$$

$$\text{Velocity Head} = 0.08 \text{ ft}$$

Energy Head = water elevation + velocity head

$$\text{Energy Head} = 1.11 \text{ ft}$$

DRAINAGE LETDOWN (OR CHUTE) DESIGN

Chute Design

The letdown structures are designed using gabions as a liner. Bedding for the gabions will be prepared subgrade soil overlain by 8 oz/sy geotextile (refer to Drawing III.F.9). The gabions are placed along the entire chute to protect the chute bottom and the final cover from erosion due to potential erosive velocities. Tumbling flow concrete energy dissipators will be placed at the bottom end of the letdown structure to dissipate excess energy present in the water as it travels down the two and three percent slopes in the low-water crossings over the perimeter road.

The following design information is included in this Appendix:

- Flow rates used in the chutes are presented in Appendix III.F-A – HEC-1 computer program output file.
- Hydraulic calculations are summarized on pages III.F-C-9 and III.F-C-10, and the calculation procedure is provided on pages III.F-C-11 and III.F-C-12.
- Chute layouts and drainage areas are shown on Sheet III.F-C-13.
- The chute energy dissipater sizing calculation procedure is provided on pages III.F-C-14 through III.F-C-18.
- Additional stormwater details are included on Drawings III.F.10 through III.F.12.

CAMELOT LANDFILL
1339-351-11-02
CHUTE ANALYSIS
NORMAL DEPTH CALCULATIONS FOR
GABION-LINED CHUTES

Drainage Area	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)	Froude Number	Velocity Head (ft)	Energy Head (ft)	Flow Area (sf)
TOPSLOPE (4%) AREAS												
A1T	27	0.04	0.04	4.0	4.0	13.0	0.45	4.04	1.123	0.25	0.71	6.68
A2T	57	0.04	0.04	4.0	4.0	13.0	0.69	5.20	1.193	0.42	1.11	10.96
A7T	66	0.04	0.04	4.0	4.0	13.0	0.75	5.46	1.207	0.46	1.22	12.09
A10T	62	0.04	0.04	4.0	4.0	13.0	0.73	5.34	1.201	0.44	1.17	11.59
SIDESLOPE (25%) AREAS												
A1S	156	0.25	0.04	4.0	4.0	13.0	0.73	13.40	3.005	2.79	3.52	11.64
A2S	195	0.25	0.04	4.0	4.0	13.0	0.83	14.40	3.058	3.22	4.05	13.54
A3	61	0.25	0.04	4.0	4.0	13.0	0.43	9.75	2.784	1.48	1.90	6.26
A4	100	0.25	0.04	4.0	4.0	13.0	0.57	11.56	2.900	2.07	2.64	8.65
A5	134	0.25	0.04	4.0	4.0	13.0	0.67	12.74	2.969	2.52	3.19	10.52
A6	73	0.25	0.04	4.0	4.0	13.0	0.47	10.38	2.826	1.67	2.15	7.03
A7S	201	0.25	0.04	4.0	4.0	13.0	0.84	14.54	3.065	3.29	4.13	13.82
A8	80	0.25	0.04	4.0	4.0	13.0	0.50	10.71	2.847	1.78	2.28	7.47
A9	105	0.25	0.04	4.0	4.0	13.0	0.58	11.75	2.911	2.14	2.73	8.94
A10S	180	0.25	0.04	4.0	4.0	13.0	0.79	14.03	3.039	3.06	3.85	12.83
A11	158	0.25	0.04	4.0	4.0	13.0	0.74	13.45	3.008	2.81	3.55	11.75
A12	114	0.25	0.04	4.0	4.0	13.0	0.61	12.08	2.931	2.27	2.88	9.44

CAMELOT LANDFILL
1339-351-11-02
CHUTE ANALYSIS
NORMAL DEPTH CALCULATIONS FOR
GABION-LINED CHUTES

Drainage Area	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)	Froude Number	Velocity Head (ft)	Energy Head (ft)	Flow Area (sf)	Flow Top Width (ft)
LOW WATER CROSSING (2%) AREAS													
A1S	156	0.02	0.04	8.0	8.0	13.0	1.33	4.95	0.910	0.38	1.71	31.52	34.32
A2S	195	0.02	0.04	8.0	8.0	13.0	1.49	5.26	0.924	0.43	1.92	37.07	36.81
A3	61	0.02	0.04	8.0	8.0	13.0	0.82	3.79	0.853	0.22	1.05	16.08	26.15
A4	100	0.02	0.04	8.0	8.0	13.0	1.06	4.37	0.883	0.30	1.36	22.88	30.02
A5	134	0.02	0.04	8.0	8.0	13.0	1.23	4.74	0.901	0.35	1.58	28.24	32.75
A6	73	0.02	0.04	8.0	8.0	13.0	0.90	4.00	0.863	0.25	1.15	18.27	27.45
A7S	201	0.02	0.04	8.0	8.0	13.0	1.51	5.30	0.926	0.44	1.95	37.89	37.17
A8	80	0.02	0.04	8.0	8.0	13.0	0.95	4.10	0.869	0.26	1.21	19.51	28.16
A9	105	0.02	0.04	8.0	8.0	13.0	1.09	4.43	0.886	0.31	1.40	23.70	30.45
A10S	180	0.02	0.04	8.0	8.0	13.0	1.59	5.86	0.944	0.53	2.12	30.73	25.70
A11	158	0.02	0.04	8.0	8.0	13.0	1.34	4.97	0.911	0.38	1.72	31.82	34.46
A12	114	0.02	0.04	8.0	8.0	13.0	1.14	4.53	0.891	0.32	1.46	25.14	31.20

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

CAMELOT LANDFILL
1339-351-11-02
CHUTE ANALYSIS
EXAMPLE CALCULATION FOR
GABION-LINED CHUTES

Example Calculation: Calculate the normal depth for the chute for drainage area A1S.

List of Symbols

- Q_d = design flow rate for channel, cfs
- R = hydraulic radius, ft
- n = Manning's roughness coefficient
- S = channel slope, ft/ft
- b = bottom width of channel, ft
- z = z-ratio (ratio of run to rise for channel sideslope)
- A_f = flow area, sf
- g = gravitational acceleration = 32.2 ft/s²
- T = top width of flow, ft
- d = normal depth of chute, ft

The program uses an iterative process to calculate the normal depth of the chute to satisfy Manning's Equation

$$Q = \frac{1.486}{n} A R^{0.67} S^{0.5}$$

Design Inputs:

Q_d =	156	cfs (from HEC-1 analysis, Appendix IIIF-A)
S =	0.25	ft/ft
b =	13	ft
z =	4	(H) : 1 (V)
n =	0.04	

Step 1 - Based on the geometry of the chute cross-section, solve for R and A_f

$$R = \frac{bd + zd^2}{b + 2d(z^2 + 1)^{0.5}}$$

$$A_f = bd + zd^2$$

assume: $d = 0.73$ ft

$$R = 0.611 \text{ ft}$$

$$A_f = 11.64 \text{ sf}$$

solve for Q : $Q = 156$

CAMELOT LANDFILL
1339-351-11-02
CHUTE ANALYSIS
EXAMPLE CALCULATION FOR
GABION-LINED CHUTES

if Q is not equal to Q_d , select a new d and repeat calculations

Step 2 - solve for velocity, T, Froude number, velocity head, and energy head

$$Q = VA \Rightarrow V = Q/A$$

$$V = 13.40 \text{ ft/s}$$

$$T = b + 2(z \times d)$$

$$T = 18.85 \text{ ft}$$

$$F_r = \frac{V}{(gA/T)^{0.5}}$$

$$F_r = 3.005$$

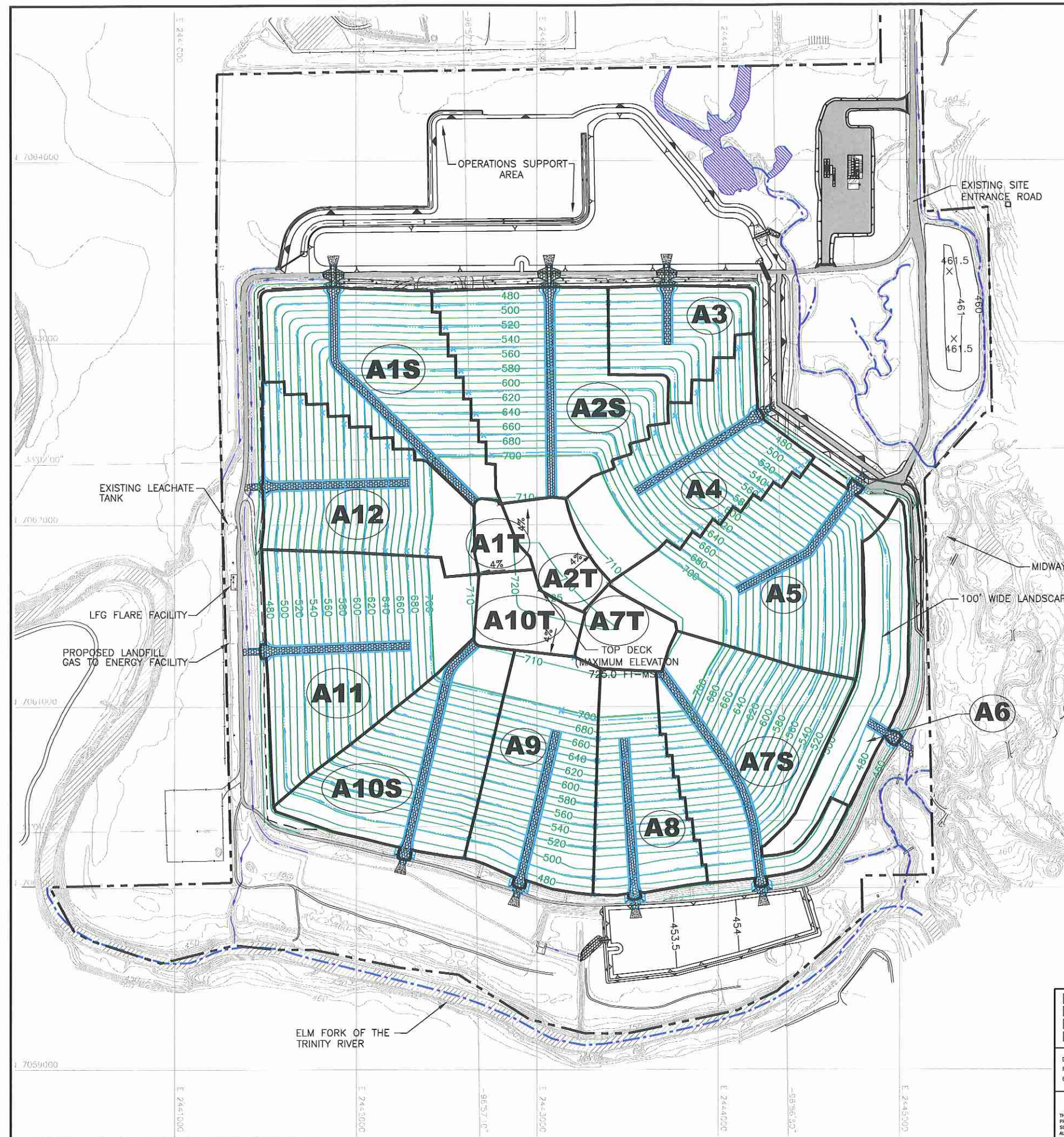
$$\text{Velocity Head} = \frac{V^2}{2g}$$

$$\text{Velocity Head} = 2.79 \text{ ft}$$

Energy Head = water elevation + velocity head

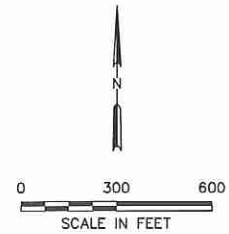
$$\text{Energy Head} = 3.52 \text{ ft}$$

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LEGEND

- PERMIT BOUNDARY
- PROPOSED LIMIT OF WASTE
- STATE PLANE COORDINATE SYSTEM
- GEODETIC COORDINATE SYSTEM
- EXISTING CONTOUR (SEE NOTE 1)
- 600 REGRADED BUFFER ZONE AREA
- 600 PROPOSED FINAL COVER CONTOUR
- PROPOSED LETDOWN STRUCTURE
- DRAINAGE SWALE
- USACE SECTION 404 JURISDICTIONAL WATERS OF THE U.S. (SEE NOTE 3)
- USACE JURISDICTIONAL WETLANDS
- DRAINAGE AREA BOUNDARY
- A3** DRAINAGE AREA DESIGNATION



DRAINAGE AREA DESIGNATION	AREA (ACRES)
A1T	2.07
A2T	4.56
A7T	4.90
A10T	4.20
A1S	20.17
A2S	23.32
A3	8.66
A4	18.25
A5	23.05
A6	10.87
A7S	22.89
A8	12.65
A9	17.25
A10S	18.55
A11	24.67
A12	18.13

NEVZAT TURAN
 84059
 LICENSED PROFESSIONAL ENGINEER

2-28-12

- NOTE:
- CONTOURS AND ELEVATIONS PROVIDED BY METROPOLITAN AERIAL SURVEYS COMPILED FROM AERIAL PHOTOGRAPHY FLOWN 8-28-2010. THE GRID SYSTEM IS TIED TO THE TEXAS STATE PLANE COORDINATE SYSTEM NORTH CENTRAL ZONE NAD 1983. ELEVATIONS ARE BASED ON NAVD 1988.
 - MAXIMUM FINAL COVER ELEVATION IS 725 FT-MSL. MAXIMUM TOP OF WASTE ELEVATION IS 721.5 FT-MSL.
 - SECTION 404 JURISDICTIONAL WATERS OF THE U.S. AND WETLANDS REPRODUCED FROM THE GOSHAWK ENVIRONMENTAL CONSULTANTS, INC. SEPTEMBER 2010 REPORT WHICH IS INCLUDED IN PARTS I/II, APPENDIX I/II.

<input type="checkbox"/> DRAFT <input checked="" type="checkbox"/> FOR PERMITTING PURPOSES ONLY <input type="checkbox"/> ISSUED FOR CONSTRUCTION <input type="checkbox"/> CLIENT APPROVAL BY:	PREPARED FOR CITY OF FARMERS BRANCH	MAJOR PERMIT AMENDMENT LETDOWN STRUCTURE DRAINAGE AREAS CAMELOT LANDFILL DENTON COUNTY, TEXAS															
DATE: 02/2012 FILE: 1339-351-11 CAD: IIF-C-13_DRAIN_AREAS.DWG	DRAWN BY: SRF DESIGN BY: CRM REVIEWED BY: JPY	<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th colspan="3">REVISIONS</th> </tr> <tr> <th>NO.</th> <th>DATE</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> </tbody> </table>	REVISIONS			NO.	DATE	DESCRIPTION									
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		SHEET IIF-C-13															

CAMELOT LANDFILL
1339-351-11-02
EROSION CONTROL STRUCTURE MODIFICATION
GABION-LINED CHUTE DESIGN
25-YEAR, 24 HOUR STORM

Required: Provide design for a gabion-lined letdown structure (or chute).

Method:

1. Design the energy dissipator system at the downstream end of the proposed "tumbling flow" chutes.
The tumbling flow regime consists of a series of hydraulic jumps and overfalls designed to maintain critical velocity in the chutes. Tumbling flow occurs only in the energy dissipators located at the downstream end of the chutes.

Assumptions:

1. The gabion-lined chute will transition to its maximum width for the energy dissipator design where maximum total flow for chute is expected to occur.
2. Concrete block will be designed for a maximum height of 3 1/2 feet.
3. Proposed chutes will convey runoff from the following chute drainage area:

Proposed Chute	Chute Drainage Areas	25-Year Total Flow (cfs) ¹
1	A1S	156
2	A2S	195
3	A3	61
4	A4	100
5	A5	134
6	A6	73
7	A7S	201
8	A8	80
9	A9	105
10	A10S	180
11	A11	158
12	A12	114

¹ From HEC-1 Analysis, Appendix III-F-A

References:

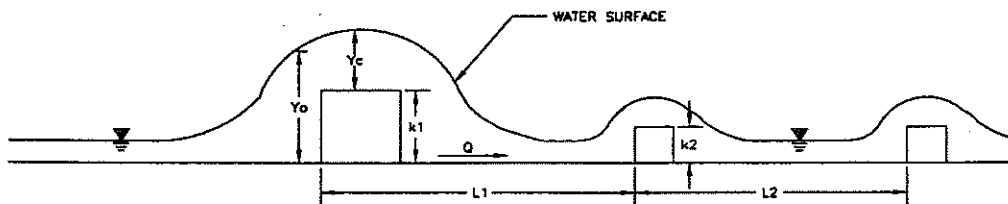
1. Gamelsky, S.G., *Innovations in Stormwater Management for Landfill Closure* Technical Paper
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3. Morris, H.M., *Hydraulics of Energy Dissipators in Steep Rough Channels*, Bulletin 19, Research Division, Virginia Polytechnic Institute, Blacksburg, Virginia.

CAMELOT LANDFILL
1339-351-11-02
EROSION CONTROL STRUCTURE MODIFICATION
GABION-LINED CHUTE DESIGN
25-YEAR, 24 HOUR STORM

Solution:

1. Energy Dissipator Design

1. Tumbling Flow Energy Dissipators



Definition of Terms/Variables:

- Q = flow rate (cfs)
- q = unit flow (cfs/ft width)
- Y_c = critical depth (ft)
- Y_o = approach depth (ft)
- k_1 = height of initial element (ft)
- k_2 = height of secondary elements (ft)
- L_1 = distance between initial and secondary elements (ft)
- L_2 = distance between secondary elements (ft)
- W = bottom width of chute (ft)
- g = acceleration due to gravity, 32.2 ft/s^2
- S = slope of channel (percent)
- x = slope of channel (degrees)
- n = Manning's Coefficient

CAMELOT LANDFILL
1339-351-11-02
EROSION CONTROL STRUCTURE MODIFICATION
GABION-LINED CHUTE DESIGN
25-YEAR, 24 HOUR STORM

Design Equations:

$$q = Q/W \quad (\text{Ref 3, page 93, Item 6})$$

$$Y_c = (q^2/g)^{1/3} \quad (\text{Ref 3, page 92, Item 3})$$

$$Y_o = (nq/(1.5 \tan(x)^{0.5}))^{3/5} \quad (\text{Ref 3, page 28, Eqn 24})$$

$$y_1 = 0.35 q^{2/3} \quad (\text{Ref 1, page 93, Item 7})$$

$$K_1 = Y_o \{ [(2/1 - 0.01S)(Y_c/Y_o)]^{0.5} - (1 - 0.01S)^2 \} \quad (\text{Ref 3, page 93, Item 5})$$

$$K_2 = \frac{Y_c}{(3-0.037S)^{2/3}} \quad (\text{Ref 1, page 92, Item 3})$$

$$L_1 = (1 + 0.01S)K_1 + Y_o(K_1/g \cos(x))^{0.5} \quad (\text{Ref 1, page 42, Eqn 31})$$

$$L_2 = 8.5 K_2$$

Note: use the greater of L_1 and L_2

Chute parameters:

Slope (S) =	25	%
Manning's coefficient (n) =	0.04	
Slope (x) =	14.04	deg
g =	32.2	ft/s ²

EROSION CONTROL STRUCTURE MODIFICATION
GABION-LINED CHUTE DESIGN
25-YEAR, 24 HOUR STORM

Chute	Q'	W	q	Y _C	Y _O	y ₁	K ₁	K ₂
1	156	14	11.14	1.57	0.73	1.75	3.45	0.96
2	195	18	10.83	1.54	0.72	1.71	3.38	0.95
3	61	13	4.69	0.88	0.44	0.98	1.87	0.54
4	100	13	7.69	1.22	0.59	1.36	2.65	0.75
5	134	13	10.31	1.49	0.70	1.66	3.26	0.92
6	73	13	5.62	0.99	0.49	1.11	2.12	0.61
7	201	18	11.17	1.57	0.73	1.75	3.45	0.97
8	80	13	6.15	1.06	0.51	1.18	2.26	0.65
9	105	13	8.08	1.27	0.60	1.41	2.74	0.78
10	180	16	11.25	1.58	0.74	1.76	3.47	0.97
11	158	15	10.53	1.51	0.71	1.68	3.31	0.93
12	114	13	8.77	1.34	0.63	1.49	2.91	0.82

Chute	L ₁	L ₂	L ₂ Used
1	4.83	8.92	8.9
2	4.73	8.75	8.8
3	2.55	5.01	5.0
4	3.67	6.96	7.0
5	4.56	8.46	8.5
6	2.91	5.65	5.6
7	4.84	8.93	8.9
8	3.11	6.00	6.0
9	3.80	7.19	7.2
10	4.86	8.97	9.0
11	4.63	8.59	8.6
12	4.04	7.60	7.6

Prep By: CRM
Date: 2/21/2012

CAMELOT LANDFILL
1339-351-11-02
EROSION CONTROL STRUCTURE MODIFICATION
GABION-LINED CHUTE DESIGN
25-YEAR, 24 HOUR STORM

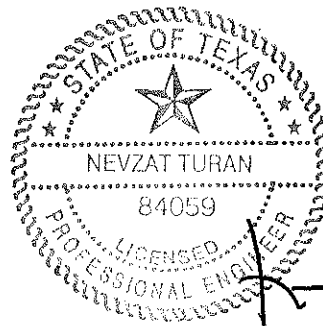
Chkd By: RCE
Date: 2-28-12

Design Summary

Chute	Height of		Length Between Weir and First Element (L ₁) (ft)	Length Between Elements (L ₂) (ft)
	Concrete Weir (K ₁) (ft)	Secondary Element (K ₂) (ft)		
1	3.5	0.96	4.83	8.9
2	3.5	0.95	4.73	8.8
3	3.0	0.75	2.55	5.0
4	3.0	0.75	3.67	7.0
5	3.5	0.92	4.56	8.5
6	3.0	0.75	2.91	5.6
7	3.5	0.97	4.84	8.9
8	3.0	0.75	3.11	6.0
9	3.0	0.78	3.80	7.2
10	3.5	0.97	4.86	9.0
11	3.5	0.93	4.63	8.6
12	3.0	0.82	4.04	7.6

APPENDIX IIIF-D

EROSION LAYER EVALUATION



2-28-12

Includes pages IIIF-D-1 through IIIF-D-37

EROSION LAYER EVALUATION

This appendix presents the supporting documentation for evaluation of the thickness of the erosion layer for the final cover system at the Camelot Landfill. The evaluation is based on the premise of adding excess soil to increase the time required before maintenance is needed as recommended in the EPA Solid Waste Disposal Facility Criteria Technical Manual (EPA 530-R-93-017, November 1993).

The design procedure is as follows:

1. Minimum thickness of the erosion layer at the end of the 30-year postclosure period is evaluated based on the depth of frost penetration or 6 inches, whichever is greater. For Denton County, the approximate depth of frost penetration is approximately 6.1 inches (see III-F-D-9). Therefore, the minimum erosion layer thickness is 6.1 inches.
2. Soil loss is calculated using the Universal Soil Loss Equation (USLE) by following SCS procedures. The soil loss is adjusted by a safety factor of 2 and is then converted to a thickness. The thickness of the soil loss over a 30-year postclosure period is added to the minimum thickness of the erosion layer (from Step 1) to yield an initial thickness to be placed at closure of the site. According to the USLE, the typical 4 percent topslope and 25 percent side slope require a minimum of 6.199 inches and 6.955 inches, respectively, for the erosion layer. These USLE requirements include the 6.1-inch minimum required by regulations. Conservatively, a 24-inch erosion layer is proposed over final cover. These calculations begin on page III-F-D-3.
3. Stormwater flows over the final cover system by (1) sheet flow over the topslope and sideslopes and (2) channelized flow in the drainage berms (or swales). As discussed in Section 2.2 and Appendix III-F-C, flow also occurs in the letdown structures. The letdown structures are lined with gabions to prevent erosion given that the velocities in the letdowns are over 5 ft/sec.

Sheet flow velocities for the topslope and sideslope cases for a 25-year storm event are calculated to be less than permissible nonerosive velocities. A permissible nonerosive velocity is defined as 5.0 ft/sec or less. Calculated sheet flow velocities range from 0.33 to 0.45 ft/sec for topslope and sideslope cases. The supporting calculations are presented on pages III-F-D-17 through III-F-D-25.

Channelized flow for drainage swales is also calculated to be less than permissible nonerosive velocities. Calculated channelized flow velocities range from 1.65 to

- 3.24 ft/sec for the drainage swales. The supporting calculations are presented on pages IIIF-C-3 through IIIF-C-7.
4. Vegetation for the site will be native and introduced grasses with root depths of 6 inches to 8 inches. The seeding is specified on the attached pages IIIF-D-26 through IIIF-D-37. The seeding included on pages IIIF-D-26 through IIIF-D-37 is specified by TxDOT for temporary and permanent erosion control for Denton County, Texas (Fort Worth District).
 5. Native and introduced grasses will be hydroseeded with fertilizer on the disked (parallel to contours) erosion layer upon final grading. Temporary cold weather vegetation will be established if needed. Irrigation will be employed for 6 to 8 weeks or until vegetation is well established. Erosion control measures such as silt fences and straw bales will be used to minimize erosion until the vegetation is established. Areas that experience erosion or do not readily vegetate after hydroseeding will be reseeded until vegetation is established or the soil will be replaced with soil that will support the grasses.
 6. Slope stability information is included in Appendix IIIJ.

Required: Determine expected soil loss and minimum thickness for the erosion layer.

Method: Expected soil loss is calculated using the Universal Soil Loss Equation. Minimum erosion layer thickness is determined by adding the minimum thickness allowed by TCEQ to the expected soil loss.

- References:**
1. SCS National Engineering Handbook, Chapter 3 - Erosion.
 2. TNRC, *Use of the USLE in Final Cover/Configuration Design*, 1993.
 3. United States Department of Agriculture, National Resource Conservation Service, Web Soil Survey for Denton County, Texas (<http://websoilsurvey.nrcs.usda.gov>).
 4. United States Environmental Protection Agency, *Solid Waste Disposal Facility Criteria Technical Manual*, 1993.

Solution: 1. Soil Loss Equation: $A=RKL_sCP$

Where:

- A= Soil loss (tons/ac/yr)
- R= Rainfall factor
- K= Soil erodibility factor
- L_s = Slope length/slope gradient factor
- C= Plant cover or cropping management factor
- P= Erosion practice factor

The rainfall factor, R, represents the average intensity for the maximum intensity, 30 minute storms over a 22 year period of record compiled by the SCS. Using Figure 1 (Ref 2), Average Annual Values of the R Factor, the R factor for Denton County is:

$$R = 275$$

The soil erodibility factor, K, factor represents the resistance of a soil surface to erosion as a function of the soil's physical and chemical properties. Assume an organic matter content of 2% to determine the K factor. The site top soil will consist of silty clay with high organic content. Clean compost as a soil amendment maybe added to final cover top soil as necessary to protect against erosion. Therefore, the following is a K value for the site.

$$K = 0.25$$

The slope length/slope gradient factor, L_s , represents the erosion of the soil due to both slope length and degree of slope. The slopes of interest are the typical side slope and top slope conditions.
See sheet HIF-D-7 for the locations of the slopes analyzed.

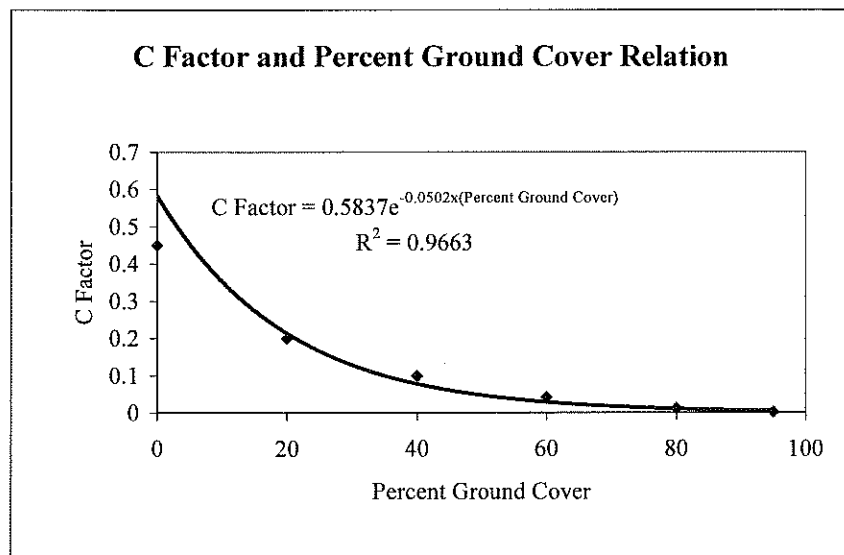
Case 1.	Typical Top Slope	Case 2.	Longest Top Slope
	slope = 4 %		slope = 4 %
	length = 500 ft		length = 600 ft
Case 3.	Typical Side Slope	Case 4.	Longest Side Slope
	25 %		25 %
	120 ft		126 ft

Using the above information and Figure 2 (Ref 2, p.9), the L_s factors are determined.

Case	Slope (%)	Slope Length (ft)	L_s
1. Typical Top Slope	4	500	0.75
2. Longest Top Slope	4	600	0.81
5. Typical Side Slope	25	120	6.50
6. Longest Side Slope	25	126	6.60

The plant cover or cropping management factor, C, represents the percentage of soil loss that would occur if the surface were partially protected by some combination of cover and management practices. C Factor for Permanent Pasture, Range, and Idle Land with No Appreciable Canopy has the following relation with percent ground cover (GC) (from Ref 2, p.7).

% GC	C Factor:
0	0.45
20	0.2
40	0.1
60	0.042
80	0.013
95	0.003



C Factor = $0.5837e^{-0.0502x90}$
C Factor = 0.0064 (for 90% ground cover)

The erosion control practice factor, P, measures the effect of control practices that reduce the erosion potential of the runoff by influencing drainage patterns, runoff concentration, and runoff velocity. Contouring for this site will be done only to establish vegetation.

$$P = 1.00$$

2. Soil loss calculations

Slope Condition	R	K	L _s	C	P	A (tons/ac/yr)
1. Typical Top Slope 4% slope 500 ft length	275	0.25	0.75	0.0064	1.00	0.33
2. Longest Top Slope 4% slope 600 ft length	275	0.25	0.81	0.0064	1.00	0.35
3. Typical Side Slope 25% slope 120 ft length	275	0.25	6.50	0.0064	1.00	2.85
4. Longest Side Slope 25% slope 126 ft length	275	0.25	6.60	0.0064	1.00	2.89

Note: Erosion layer will be maintained to provide 90% ground cover.

3. Erosion layer thickness calculations:

$$T_{el} = 6.1 \text{ in} + \frac{AYF(2000\text{lb/ton})(12\text{in/ft})}{w(43,560\text{s/ft}^2)}$$

Where: T_{el} = Erosion layer thickness
A = Soil loss (ton/ac/yr)
Y = Postclosure period (yr)
F = Factor of Safety
w = Specific weight of soil (pcf)

Y = 30 yr
F = 2
w = 110 pcf

CAMELOT LANDFILL
1339-351-11-02
EROSION LAYER EVALUATION

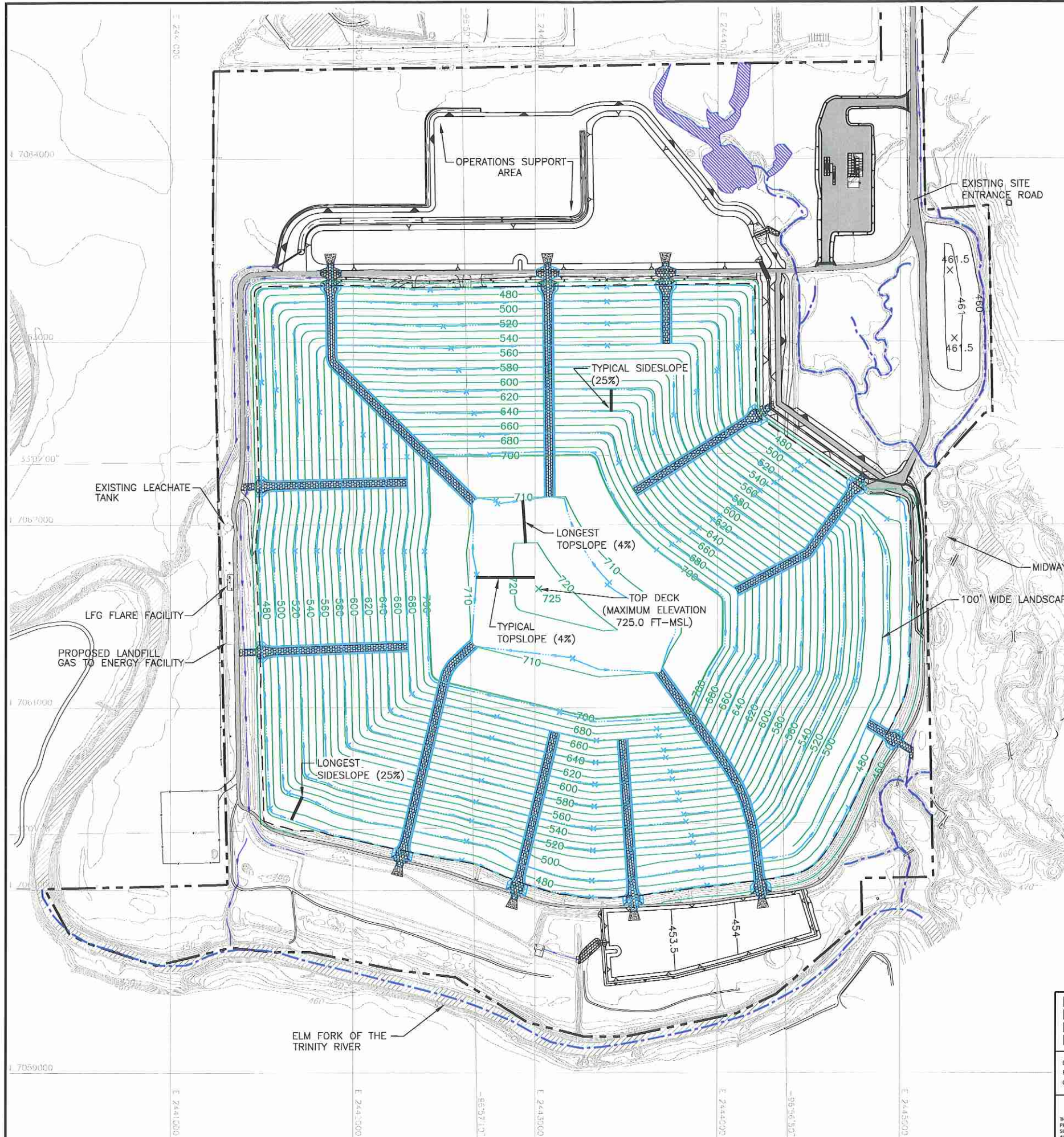
1. Typical Top Slope Thickness:		
T _{et} , Required thickness ¹ =	6.199	in
Total estimated soil loss =	0.099	in
Specified thickness =	24.000	in
2. Longest Top Slope Thickness:		
T _{et} , Required thickness ¹ =	6.207	in
Total estimated soil loss =	0.107	in
Specified thickness =	24.000	in
3. Typical Sideslope Thickness:		
T _{et} , Required thickness ¹ =	6.955	in
Total estimated soil loss =	0.855	in
Specified thickness =	24.000	in
4. Longest Sideslope Thickness:		
T _{et} , Required thickness ¹ =	6.968	in
Total estimated soil loss =	0.868	in
Specified thickness =	24.000	in

Note: ¹Required thicknesses include 6.1 inch minimum required and estimated soil loss.

4. Summary:

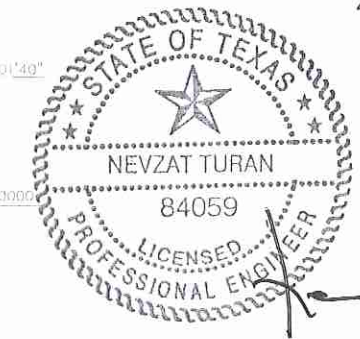
Calculated erosion losses are shown in Step 2 above.
The erosion layer will be a minimum of 24 inches thick.
As shown above, this is a conservative design considering
the maximum expected soil loss for a 30 year period is 0.900 inches.

O:\1339\351\EXPANSION 2009\PART III-SDP\III-D-7 DRAINAGE STRUCTURE PLAN.dwg, jwilson, 1:2



- LEGEND**
- PERMIT BOUNDARY
 - - - PROPOSED LIMIT OF WASTE
 - N 7064000 STATE PLANE COORDINATE SYSTEM
 - 33°02'00" GEODETIC COORDINATE SYSTEM
 - 500 EXISTING CONTOUR (SEE NOTE 1)
 - 600 REGRADED BUFFER ZONE AREA
 - 600 PROPOSED FINAL COVER CONTOUR
 - PROPOSED LETDOWN STRUCTURE
 - X DRAINAGE SWALE
 - USACE SECTION 404 JURISDICTIONAL WATERS OF THE U.S. (SEE NOTE 4)
 - USACE JURISDICTIONAL WETLANDS

- NOTE:**
1. CONTOURS AND ELEVATIONS PROVIDED BY METROPOLITAN AERIAL SURVEYS COMPILED FROM AERIAL PHOTOGRAPHY FLOWN 8-28-2010. THE GRID SYSTEM IS TIED TO THE TEXAS STATE PLANE COORDINATE SYSTEM NORTH CENTRAL ZONE NAD 1983. ELEVATIONS ARE BASED ON NAVD 1988.
 2. PERMIT BOUNDARY WAS PREPARED BY PEISER SUREYING CO. IN NOVEMBER 2010.
 3. MAXIMUM FINAL COVER ELEVATION IS 725 FT-MSL. MAXIMUM TOP OF WASTE ELEVATION IS 721.5 FT-MSL.
 4. SECTION 404 JURISDICTIONAL WATERS OF THE U.S. AND WETLANDS REPRODUCED FROM THE GOSHAWK ENVIRONMENTAL CONSULTANTS, INC. SEPTEMBER 2010 REPORT WHICH IS INCLUDED IN PARTS I/II, APPENDIX I/II.B.



2-28-12
[Signature]

<input type="checkbox"/> DRAFT <input checked="" type="checkbox"/> FOR PERMITTING PURPOSES ONLY <input type="checkbox"/> ISSUED FOR CONSTRUCTION <input type="checkbox"/> CLIENT APPROVAL BY:		PREPARED FOR CITY OF FARMERS BRANCH		MAJOR PERMIT AMENDMENT DRAINAGE STRUCTURE PLAN CAMELOT LANDFILL DENTON COUNTY, TEXAS <i>Weaver Boos Consultants</i> TBPE REGISTRATION NO. F-3727													
DATE: 02/2012 FILE: 1339-351-11 CAD: IIF-D-7-DRAINAGE PLAN.DWG		DRAWN BY: SRF DESIGN BY: CRM REVIEWED BY: JPY				REVISIONS <table border="1"> <thead> <tr> <th>NO.</th> <th>DATE</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td></tr> </tbody> </table>		NO.	DATE	DESCRIPTION							
NO.	DATE	DESCRIPTION															
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					SHEET IIF-D-7												



Solid Waste Disposal Facility Criteria

Technical Manual

Printed on Recycled Paper

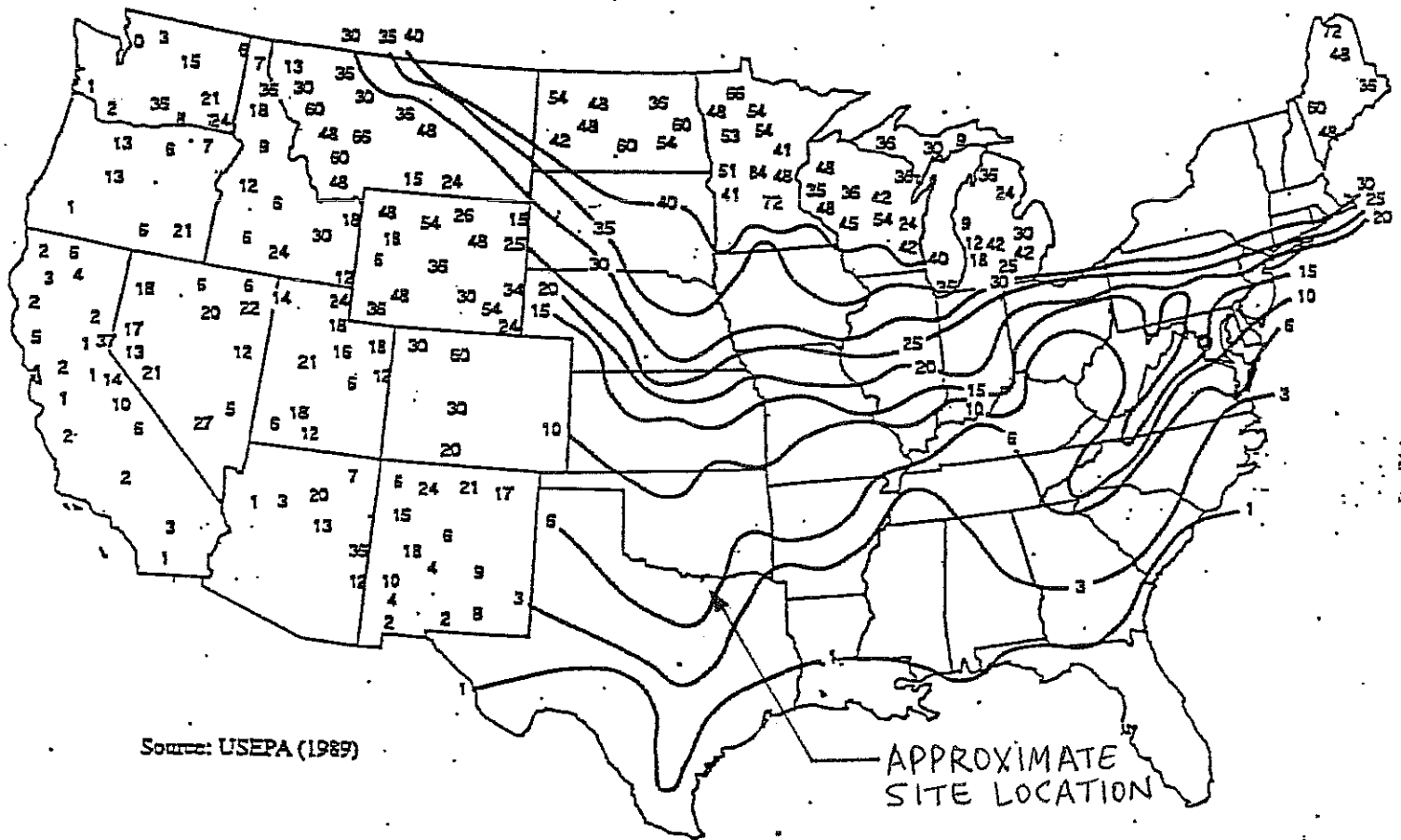
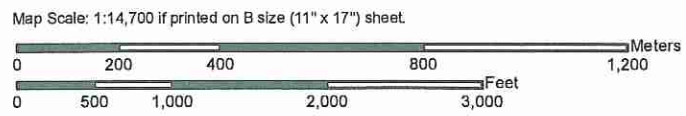
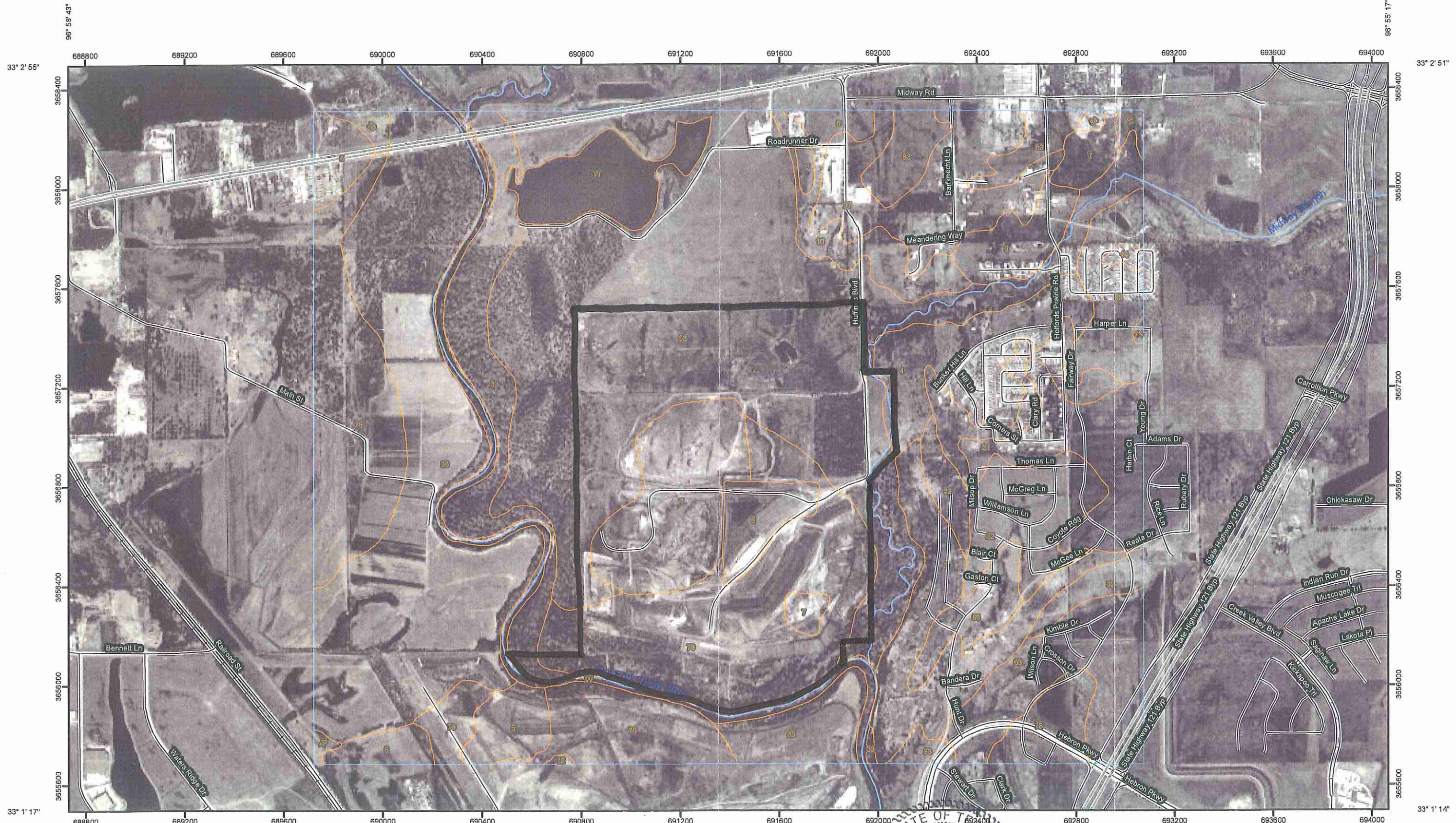


Figure 6-4
Regional Depth of Frost Penetration in Inches

Map Unit Legend

Denton County, Texas (TX121)			
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
3	Altoga silty clay, 5 to 8 percent slopes	77.8	3.6%
4	Altoga silty clay, 5 to 12 percent slopes, eroded	68.7	3.2%
5	Aquilla loamy fine sand, 2 to 5 percent slopes	37.7	1.7%
6	Arents, gently undulating	36.7	1.7%
7	Arents, hilly	102.5	4.7%
9	Bastil fine sandy loam, 1 to 3 percent slopes	35.8	1.6%
10	Bastil fine sandy loam, 3 to 5 percent slopes	32.7	1.5%
21	Burleson clay, 0 to 1 percent slopes	61.0	2.8%
22	Burleson clay, 1 to 3 percent slopes	80.7	3.7%
27	Crockett fine sandy loam, 1 to 3 percent slopes	79.8	3.7%
32	Ferris-Heiden clay, 5 to 15 percent slopes	66.5	3.1%
33	Frio silty clay, occasionally flooded	391.4	18.0%
44	Houston Black clay, 1 to 3 percent slopes	3.7	0.2%
53	Lewisville clay loam, 3 to 5 percent slopes	23.5	1.1%
63	Ovan clay, occasionally flooded	590.5	27.2%
70	Seagoville clay, occasionally flooded	54.2	2.5%
72	Silstid loamy fine sand, 1 to 5 percent slopes	0.8	0.0%
78	Trinity clay, occasionally flooded	307.4	14.1%
81	Vertel clay, 3 to 5 percent slopes	3.4	0.2%
83	Wilson clay loam, 0 to 1 percent slopes	33.0	1.5%
84	Wilson clay loam, 1 to 3 percent slopes	1.8	0.1%
W	Water	83.8	3.9%
Totals for Area of Interest		2,173.6	100.0%

Soil Map—Denton County, Texas
(CAMELOT LANDFILL)



STATE OF TEXAS
NEVZAT TURAN
84059
PROFESSIONAL ENGINEER
2-28-12
[Signature]

TEXAS NATURAL RESOURCE CONSERVATION COMMISSION

USE OF THE UNIVERSAL SOIL LOSS EQUATION
IN FINAL COVER/CONFIGURATION DESIGN

PROCEDURAL HANDBOOK

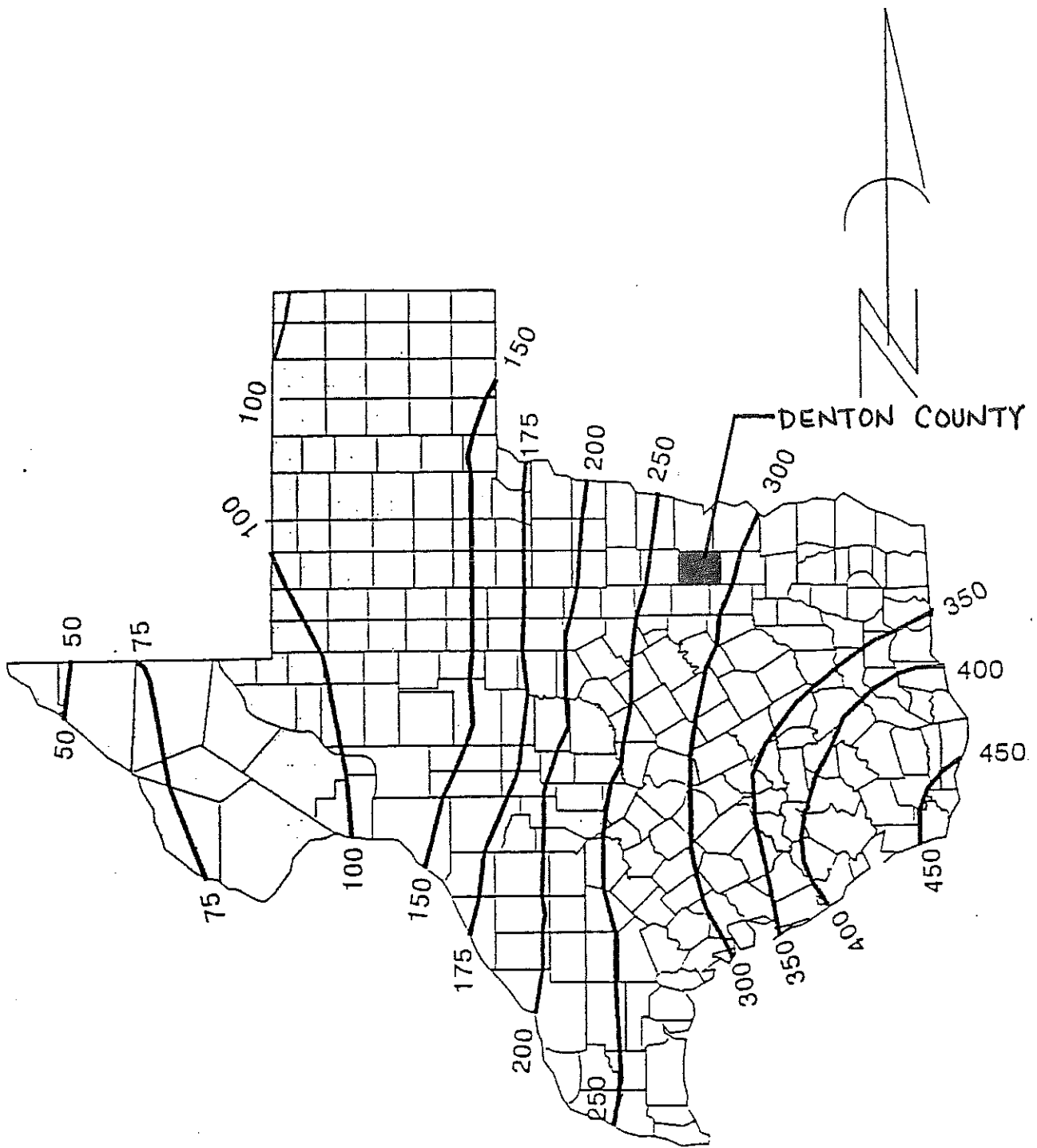
PERMITS SECTION
MUNICIPAL SOLID WASTE DIVISION

OCTOBER 1993

Table 1 Approximate Values of Factor K for USDA Textural Classes

Texture Class	Organic Matter Content		
	<0.5%	2%	4%
	K	K	K
Sand	0.05	0.03	0.02
Fine Sand	0.16	0.14	0.10
Very Fine Sand	0.42	0.36	0.28
Loamy Sand	0.12	0.10	0.08
Loamy Fine Sand	0.24	0.20	0.16
Loamy Very Fine Sand	0.44	0.38	0.30
Sandy Loam	0.27	0.24	0.19
Fine Sandy Loam	0.35	0.30	0.24
Very Fine Sandy Loam	0.47	0.41	0.33
Loam	0.38	0.32	0.29
Silt Loam	0.48	0.42	0.33
Silt	0.60	0.52	0.42
Sandy Clay Loam	0.27	0.25	0.21
Clay Loam	0.28	0.25	0.21
Silty Clay Loam	0.37	0.32	0.26
Sandy Clay	0.14	0.13	0.12
Silty Clay	0.25	0.23	0.19
Clay	0.13 - 0.29 K = 0.25		

The values shown are estimated averages of broad ranges of specific-soil values. When a texture is near the borderline of two texture classes, use the average of the two K values.



W.H. Wischmeier, SEA, 1976

FIGURE 1. - AVERAGE ANNUAL VALUES OF THE RAINFALL EROSION INDEX

Table 2 Factor C for permanent pasture, range, and idle land¹

Vegetative Canopy		Cover that contacts the soil surface					
Type and height ²	Percent cover ³	Percent ground cover					
		0	20	40	60	80	95+
No Appreciable Canopy		0.45	0.20	0.10	0.042	0.013	0.003
Tall weeds or short brush with average drop fall height of 20 in.	25	0.36	0.17	0.09	0.038	0.013	0.011
	50	0.26	0.13	0.07	0.035	0.012	0.003
	75	0.17	0.10	0.06	0.032	0.011	0.003

Extracted from:

United States Department of Agriculture, AGRICULTURE HANDBOOK NUMBER 537

- ¹ The listed C values assume that the vegetation and mulch are randomly distributed over the entire area.
- ² Canopy height is measured as the average fall height of water drops falling from the canopy to the ground. Canopy effect is inversely proportional to drop fall height and is negligible if fall height exceeds 33 ft.
- ³ Portions of total-area surface that would be hidden from view by canopy in a vertical projection (a bird's-eye view).

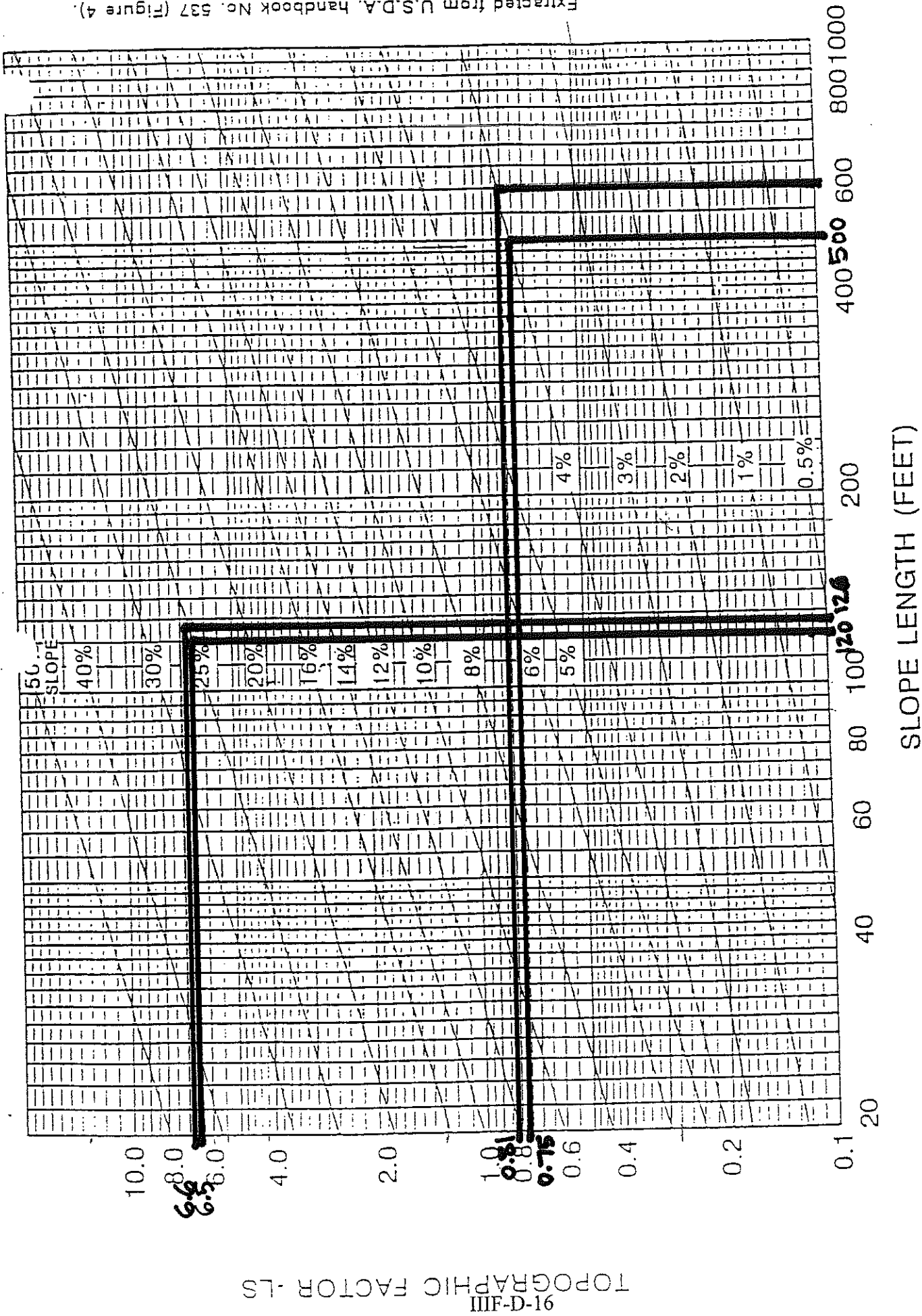


FIGURE 2.- Slope effect chart (topographic factor, LS). $LS = (\lambda/72.6)^m 65.41 \sin^2 (\theta) = 4.56 \sin (\theta) + 0.065$ where λ = slope length in feet; θ = angle of slope; and $m = 0.2$ for gradients < 1 percent, 0.3 for 1 to 3 slopes; 0.4 for 3.5 to 4.5 percent slopes, and 0.5 for slopes of 5 percent or steeper.

Required: Determine the sheet flow velocity for the final cover system design and compare to the permissible non-erodible flow velocity.

Method:

1. Determine the flow using the Rational Method.
2. Calculate flow depth using Kinematic Wave procedures.
3. Compute flow velocity and compare to permissible non-erodibility velocity.

References:

1. Raudkivi, A.J., *Hydrology - An Advanced Introduction to Hydrological Processes and Modeling*, 1979.
2. Texas Department of Transportation, *Bridge Division Hydraulic Manual*, April 2002.
3. United States Soil Conservation Service, *TR-55 Hydrology for Small Watersheds*, December 1989.

Solution: Use the typical case scenarios from the USLE calculation to determine the expected sheet flow velocity.

Case 1. Typical top slope
slope = 0.04 ft/ft
length = 500 ft

Case 2. Longest top slope
slope = 0.04 ft/ft
length = 600 ft

Case 3. Typical side slope
slope = 0.25 ft/ft
length = 120 ft

Case 4. Longest side slope
slope = 0.25 ft/ft
length = 126 ft

Time of Concentration:

$$t_c = \frac{0.007(nL)^{0.8}}{(P_{2,24})^{0.5}S^{0.4}}$$

Where:

- t_c = time of concentration (hr)
- n = Manning's roughness coefficient
- L = slope length
- $P_{2,24}$ = 2-year, 24-hour rainfall depth (in)
- S = slope (ft/ft)

United States
Department of
Agriculture

Soil
Conservation
Service

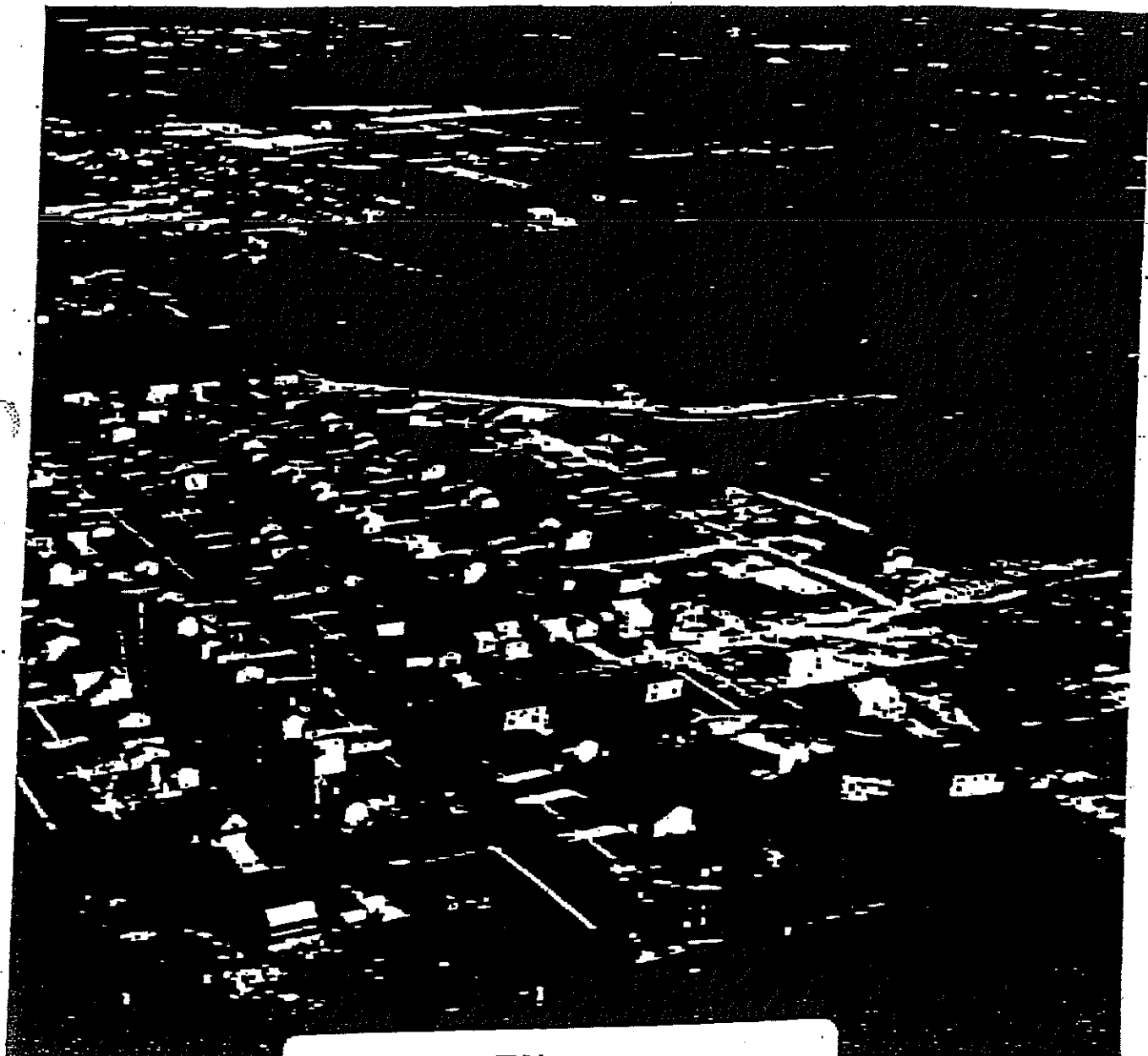
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June 1985



Urban Hydrology for Small Watersheds



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Chapter 3: Time of concentration and travel time

Travel time (T_t) is the time it takes water to travel from one location to another in a watershed. T_t is a component of time of concentration (T_c), which is the time for runoff to travel from the hydraulically most distant point of the watershed to a point of interest within the watershed. T_c is computed by summing all the travel times for consecutive components of the drainage conveyance system.

T_c influences the shape and peak of the runoff hydrograph. Urbanization usually decreases T_c , thereby increasing the peak discharge. But T_c can be increased as a result of (a) ponding behind small or inadequate drainage systems, including storm drain inlets and road culverts, or (b) reduction of land slope through grading.

Factors affecting time of concentration and travel time

Surface roughness

One of the most significant effects of urban development on flow velocity is less retardance to flow. That is, undeveloped areas with very slow and shallow overland flow through vegetation become modified by urban development: the flow is then delivered to streets, gutters, and storm sewers that transport runoff downstream more rapidly. Travel time through the watershed is generally decreased.

Channel shape and flow patterns

In small non-urban watersheds, much of the travel time results from overland flow in upstream areas. Typically, urbanization reduces overland flow lengths by conveying storm runoff into a channel as soon as possible. Since channel designs have efficient hydraulic characteristics, runoff flow velocity increases and travel time decreases.

Slope

Slopes may be increased or decreased by urbanization, depending on the extent of site grading or the extent to which storm sewers and street ditches are used in the design of the water

management system. Slope will tend to increase when channels are straightened and decrease when overland flow is directed through storm sewers, street gutters, and diversions.

Computation of travel time and time of concentration

Water moves through a watershed as sheet flow, shallow concentrated flow, open channel flow, or some combination of these. The type that occurs is a function of the conveyance system and is best determined by field inspection.

Travel time (T_t) is the ratio of flow length to flow velocity:

$$T_t = \frac{L}{3600 V} \quad [\text{Eq. 3-1}]$$

where

- T_t = travel time (hr).
- L = flow length (ft).
- V = average velocity (ft/s), and
- 3600 = conversion factor from seconds to hours.

Time of concentration (T_c) is the sum of T_t values for the various consecutive flow segments:

$$T_c = T_{t1} + T_{t2} + \dots + T_{tm} \quad [\text{Eq. 3-2}]$$

where

- T_c = time of concentration (hr) and
- m = number of flow segments.

Determine $P_{2,24}$:

$$i = \frac{b}{(t_c + d)^e}$$

Where: i = rainfall intensity (in/hr)
 b = constant for Denton County = 90
 d = constant for Denton County = 8.5
 e = constant for Denton County = 0.781
 t_d = storm duration (min) = 1440

$$i = 0.31 \text{ in/hr}$$

$$P_{2,24} = 7.34 \text{ in (Ref 2.)}$$

Calculate t_c :

Case 1:

$n = 0.24$
 $L = 500$
 $P_{2,24} = 7.3$
 $S = 0.04$

$t_c = 0.43$ hr
25.88 min

Case 2:

$n = 0.24$
 $L = 600$
 $P_{2,24} = 7.3$
 $S = 0.04$

$t_c = 0.50$ hr
29.94 min

Case 3:

$n = 0.24$
 $L = 120$
 $P_{2,24} = 7.3$
 $S = 0.25$

$t_c = 0.07$ hr
3.97 min

Case 4:

$n = 0.24$
 $L = 126$
 $P_{2,24} = 7.3$
 $S = 0.25$

$t_c = 0.07$ hr
4.13 min

Insert TR-55 reference page 3

Sheet flow

Sheet flow is flow over plane surfaces. It usually occurs in the headwater of streams. With sheet flow, the friction value (Manning's *n*) is an effective roughness coefficient that includes the effect of raindrop impact; drag over the plane surface; obstacles such as litter, crop ridges, and rocks; and erosion and transportation of sediment. These *n* values are for very shallow flow depths of about 0.1 foot or so. Table 3-1 gives Manning's *n* values for sheet flow for various surface conditions.

For sheet flow of less than 300 feet, use Manning's kinematic solution (Overton and Meadows 1975) to compute T_1 :

$$T_1 = \frac{0.007 (nL)^{0.8}}{(P_2)^{0.5} s^{0.4}} \quad [\text{Eq. 3-3}]$$

Table 3-1.—Roughness coefficients (Manning's *n*) for sheet flow

Surface description	<i>n</i> ¹
Smooth surfaces (concrete, asphalt, gravel, or bare soil)	0.011
Fallow (no residue)	0.05
Cultivated soils:	
Residue cover < 20%	0.06
Residue cover > 20%	0.17
Grass:	
Short grass prairie	0.15
Dense grasses ²	0.24
Bermudagrass	0.41
Range (natural)	0.13
Woods: ³	
Light underbrush	0.40
Dense underbrush	0.80

¹The *n* values are a composite of information compiled by Engman (1985).

²Includes species such as creeping lovegrass, bluegrass, buffalo grass, blue grama grass, and native grass mixtures.

³When selecting *n*, consider cover to a height of about 0.1 ft. This is the only part of the plant cover that will obstruct sheet flow.

where

T_1 = travel time (hr).

n = Manning's roughness coefficient (table 3-1).

L = flow length (ft).

P_2 = 2-year, 24-hour rainfall (in), and

s = slope of hydraulic grade line (land slope, ft/ft).

This simplified form of the Manning's kinematic solution is based on the following: (1) shallow steady uniform flow, (2) constant intensity of rainfall excess (that part of a rain available for runoff), (3) rainfall duration of 24 hours, and (4) minor effect of infiltration on travel time. Rainfall depth can be obtained from appendix B.

Shallow concentrated flow

After a maximum of 300 feet, sheet flow usually becomes shallow concentrated flow. The average velocity for this flow can be determined from figure 3-1, in which average velocity is a function of watercourse slope and type of channel. For slopes less than 0.005 ft/ft, use equations given in appendix F for figure 3-1. Tillage can affect the direction of shallow concentrated flow. Flow may not always be directly down the watershed slope if tillage runs across the slope.

After determining average velocity in figure 3-1, use equation 3-1 to estimate travel time for the shallow concentrated flow segment.

Open channels

Open channels are assumed to begin where surveyed cross section information has been obtained, where channels are visible on aerial photographs, or where blue lines (indicating streams) appear on United States Geological Survey (USGS) quadrangle sheets. Manning's equation or water surface profile information can be used to estimate average flow velocity. Average flow velocity is usually determined for bank-full elevation.

Rainfall Intensity-Duration-Frequency Coefficients for Texas Counties

METRIC UNITS: e is in inches, b is unitless, and d is in minutes

County name	2-year			5-year			10-year			25-year			50-year			100-year		
	e	b	d	e	b	d	e	b	d	e	b	d	e	b	d	e	b	d
Dawson	0.810	1118	10.0	0.816	1499	10.4	0.814	1727	10.4	0.807	1956	10.4	0.801	2184	10.4	0.798	2362	10.0
De Witt	0.820	1651	8.9	0.795	1905	8.7	0.758	1981	8.7	0.758	2286	8.7	0.747	2438	8.7	0.739	2591	8.9
Dear Smith	0.847	1219	10.7	0.844	1524	9.3	0.794	1549	9.3	0.831	2083	9.3	0.837	2388	9.3	0.830	2718	10.7
Delta	0.788	1372	8.2	0.783	1727	9.1	0.775	1956	9.1	0.770	2388	9.1	0.769	2388	9.1	0.753	2540	8.2
Donnell	0.789	1295	8.0	0.777	1651	8.5	0.779	1956	8.5	0.781	2286	8.5	0.780	2591	8.5	0.769	2718	8.0
Dickens	0.810	1143	9.4	0.807	1549	10.0	0.803	1803	10.0	0.808	2159	10.0	0.808	2438	10.0	0.809	2769	9.4
Dimmit	0.830	1524	9.6	0.806	1880	9.4	0.795	2083	9.4	0.783	2388	9.4	0.781	2667	9.4	0.779	2970	9.6
Donley	0.839	1321	11.0	0.832	1727	10.6	0.825	2007	10.6	0.836	2438	10.6	0.823	2616	10.6	0.845	3277	11.0
Duval	0.826	1778	8.8	0.802	2007	9.2	0.781	2134	9.2	0.772	2388	9.2	0.765	2489	9.2	0.750	2642	8.8
Eastland	0.780	1143	8.0	0.772	1473	7.8	0.771	1753	7.8	0.772	2057	7.8	0.775	2337	7.8	0.770	2565	8.0
Ector	0.812	991	9.5	0.821	1422	10.5	0.816	1651	10.5	0.789	1727	10.5	0.802	2083	10.5	0.800	2261	9.5
Edwards	0.790	1118	8.2	0.759	1372	7.5	0.759	1600	7.5	0.769	1930	7.5	0.776	2235	7.5	0.772	2540	8.2
El Paso	0.797	610	9.5	0.802	864	12.0	0.795	1067	12.0	0.843	1524	12.0	0.900	2286	12.0	0.825	1651	9.5
Ellis	0.798	1422	8.4	0.788	1803	8.8	0.777	2007	8.8	0.771	2311	8.8	0.766	2489	8.8	0.760	2667	8.4
Erali	0.780	1194	7.7	0.772	1549	8.1	0.770	1829	8.1	0.785	2261	8.1	0.772	2438	8.1	0.765	2616	7.7
Falls	0.801	1524	8.0	0.786	1829	8.5	0.771	2007	8.5	0.772	2362	8.5	0.779	2515	8.5	0.762	2616	8.3
Fannin	0.790	1372	8.3	0.778	1676	9.1	0.762	2007	9.1	0.758	2235	9.1	0.743	2388	9.1	0.740	2540	8.3
Fayette	0.805	1651	8.3	0.782	1854	8.2	0.758	1930	8.2	0.758	2235	8.2	0.743	2388	8.2	0.740	2540	8.3
Fisher	0.786	1041	8.6	0.779	1397	9.5	0.793	1778	9.5	0.790	2108	9.5	0.798	2438	9.5	0.788	2591	8.6
Floyd	0.828	1219	10.1	0.821	1600	10.0	0.821	1903	10.0	0.818	2159	10.0	0.813	2464	10.0	0.822	2794	10.1
Foard	0.810	1219	9.8	0.787	1524	9.5	0.806	1956	9.5	0.807	2311	9.5	0.817	2769	9.5	0.806	2946	9.8
Fort Bend	0.804	1776	7.9	0.760	1803	8.1	0.751	2032	8.1	0.729	2134	8.1	0.726	2311	8.1	0.710	2337	7.9
Franklin	0.780	1346	8.1	0.762	1753	8.8	0.765	1880	8.8	0.759	2134	8.8	0.751	2261	8.8	0.745	2413	8.1
Freestone	0.803	1575	8.5	0.795	1956	9.0	0.769	2032	9.0	0.775	2413	9.0	0.749	2388	9.0	0.745	2540	8.5
Frio	0.814	1549	9.3	0.789	1803	9.1	0.789	2083	9.1	0.772	2261	9.1	0.765	2438	9.1	0.769	2794	9.3
Galves	0.820	1067	10.0	0.832	1473	10.0	0.805	1600	10.0	0.797	1778	10.0	0.807	2134	10.0	0.813	2413	10.0
Galveston	0.787	1702	7.8	0.739	1676	7.6	0.742	1981	7.6	0.727	2159	7.6	0.704	2235	7.6	0.680	2159	7.8
Garza	0.812	1118	9.4	0.811	1524	10.2	0.800	1702	10.2	0.810	2108	10.2	0.799	2235	10.2	0.800	2540	9.4
Gillespie	0.787	1245	8.5	0.766	1524	8.1	0.767	1803	8.1	0.765	2083	8.1	0.764	2388	8.1	0.765	2642	8.5
Glasscock	0.801	1016	9.1	0.796	1397	10.0	0.793	1676	10.0	0.789	1880	10.0	0.789	2108	10.0	0.784	2337	9.1
Goliad	0.812	1651	9.1	0.789	1905	8.7	0.758	1956	8.7	0.755	2261	8.7	0.746	2464	8.7	0.738	2665	9.1
Gonzales	0.801	1549	8.4	0.788	1880	8.6	0.763	1956	8.6	0.760	2261	8.6	0.747	2413	8.6	0.745	2642	8.4
Gray	0.845	1372	10.8	0.837	1778	10.8	0.836	2108	10.8	0.842	2515	10.8	0.841	2896	10.8	0.846	3175	10.8
Grayson	0.790	1321	8.3	0.778	1651	8.9	0.779	1981	8.9	0.790	2413	8.9	0.781	2642	8.9	0.769	2743	8.3
Gregg	0.783	1422	8.1	0.763	1803	8.6	0.750	1829	8.6	0.753	2134	8.6	0.740	2210	8.6	0.737	2388	8.1
Gilmer	0.808	1727	8.0	0.784	1905	8.3	0.760	2057	8.3	0.744	2210	8.3	0.742	2413	8.3	0.721	2388	8.0
Guadalupe	0.796	1473	8.4	0.787	1829	8.7	0.772	1981	8.7	0.765	2261	8.7	0.750	2362	8.7	0.754	2667	8.4
Hale	0.834	1219	10.3	0.827	1549	9.9	0.815	1753	9.9	0.823	2134	9.9	0.812	2337	9.9	0.817	2642	10.3
Hall	0.829	1270	10.4	0.821	1676	10.3	0.815	1905	10.3	0.822	2337	10.3	0.819	2616	10.3	0.830	3200	10.4
Hamilton	0.779	1219	7.3	0.770	1575	8.3	0.761	1829	8.3	0.778	2261	8.3	0.766	2413	8.3	0.761	2616	7.3
Hansford	0.865	1448	10.4	0.846	1854	11.3	0.842	2134	11.3	0.862	2642	11.3	0.867	3150	11.3	0.839	2946	10.4
Hardeman	0.815	1245	10.0	0.794	1549	9.5	0.810	1981	9.5	0.816	2413	9.5	0.817	2794	9.5	0.810	3048	10.0
Hardin	0.788	1727	8.4	0.738	1651	7.5	0.740	1880	7.5	0.720	2032	7.5	0.718	2210	7.5	0.700	2210	8.4
Harris	0.800	1727	7.9	0.749	1778	7.7	0.753	2057	7.7	0.724	2057	7.7	0.728	2311	7.7	0.708	2311	7.9
Harrison	0.771	1346	8.0	0.773	1753	8.4	0.750	1778	8.4	0.747	2032	8.4	0.730	2093	8.4	0.732	2286	8.0
Hartley	0.858	1295	10.8	0.855	1702	10.2	0.840	2159	10.2	0.863	2692	10.2	0.863	2692	10.2	0.832	2718	10.8
Haskell	0.790	1143	8.9	0.779	1448	9.2	0.798	1880	9.2	0.787	2159	9.2	0.805	2616	9.2	0.788	2692	8.9
Hays	0.796	1422	10.6	0.783	1753	8.6	0.776	1981	8.6	0.765	2210	8.6	0.747	2286	8.6	0.755	2642	8.2
Hemphill	0.845	1422	10.6	0.851	1930	10.7	0.842	2210	10.7	0.843	2616	10.7	0.840	2921	10.7	0.847	3353	10.6
Henderson	0.800	1524	9.6	0.796	1956	9.0	0.770	2007	9.0	0.773	2362	9.0	0.752	2362	9.0	0.749	2591	8.7
Hidalgo	0.831	1800	9.6	0.795	2032	9.2	0.778	2210	9.2	0.771	2489	9.2	0.749	2515	9.2	0.740	2616	9.6
Hill	0.799	1448	8.2	0.780	1829	8.8	0.777	1981	8.8	0.773	2311	8.8	0.764	2489	8.8	0.759	2667	8.2
Hockley	0.832	1168	9.9	0.832	1524	10.0	0.807	1826	10.0	0.812	1981	10.0	0.810	2210	10.0	0.817	2565	9.9
Hood	0.782	1219	7.7	0.773	1600	8.3	0.773	1905	8.3	0.782	2286	8.3	0.773	2489	8.3	0.766	2667	7.7
Hopkins	0.786	1372	8.3	0.783	1778	9.1	0.775	1956	9.1	0.767	2235	9.1	0.754	2362	9.1	0.750	2540	8.3
Houston	0.797	1600	9.2	0.780	1854	8.3	0.757	1981	8.3	0.748	2184	8.3	0.740	2362	8.3	0.727	2388	8.2
Howard	0.805	1067	9.2	0.800	1422	10.1	0.802	1651	10.1	0.786	1930	10.1	0.791	2184	10.1	0.788	2413	9.2
Hudspeth	0.800	686	9.4	0.840	1118	11.4	0.827	1270	11.4	0.819	1524	11.4	0.856	1981	11.4	0.833	1956	9.4
Hunt	0.793	1397	8.4	0.785	1753	9.2	0.776	2032	9.2	0.776	2362	9.2	0.776	2616	9.2	0.758	2642	8.4
Hutchinson	0.860	1422	10.4	0.844	1778	11.0	0.837	2032	11.0	0.851	2540	11.0	0.853	3073	11.0	0.837	2921	10.4

CAMELOT LANDFILL
1339-351-11-02
SHEET FLOW VELOCITY

Calculate the design 25-year frequency for each condition:

$$Q = CiA$$

Where: Q = flow rate (cfs)
C = runoff coefficient
i = rainfall intensity (in/hr)
A = drainage area (ac)

$$i = b/(t_c+d)^e$$

Where: i = rainfall intensity (in/hr)
b = constant for Denton County = 90
d = constant for Denton County = 8.5
e = constant for Denton County = 0.781
t_c = time of concentration (min)

For a unit width of final cover, the flow lengths shown on sheet III-F-D-7 for each case is used.

$$A = [\text{Length (ft)} \times \text{Width (ft)}] / 43560 = \text{acres}$$

Case 1:
C = 0.7
t_c = 25.88 min
i = 5.68 in/hr
Length: 500.00 ft
A = 0.0115 ac
Q = 0.046 cfs

Case 2:
C = 0.7
t_c = 29.94 min
i = 5.21 in/hr
Length: 600.00 ft
A = 0.0138 ac
Q = 0.050 cfs

Case 3:
C = 0.7
t_c = 3.97 min
i = 12.54 in/hr
Length: 120.00 ft
A = 0.0028 ac
Q = 0.024 cfs

Case 4:
C = 0.7
t_c = 4.13 min
i = 12.42 in/hr
Length: 126.00 ft
A = 0.0029 ac
Q = 0.025 cfs

Approximate depth of flow:

Using Manning's Equation

$$V = 1.49/n y^{0.67} S^{0.5}$$

$$Q = VA \Rightarrow V = Q/A$$

$$A = y \times 1 \text{ (assuming unit width of flow)}$$

substituting for V

$$Q/y = 1.49/n y^{0.67} S^{0.5}$$

$$Q = 1.49/n y^{1.67} S^{0.5}$$

solve for y

$$y = (Qn/1.49 S^{0.5})^{1/1.67}$$

$$y = (Qn/1.49S^{0.5})^{0.6}$$

Case 1:

$$Q = 0.046 \text{ cfs}$$

$$n = 0.24$$

$$S = 0.04 \text{ ft/ft}$$

$$y = 0.138 \text{ ft}$$

Case 2:

$$Q = 0.050 \text{ cfs}$$

$$n = 0.24$$

$$S = 0.04 \text{ ft/ft}$$

$$y = 0.146 \text{ ft}$$

Case 3:

$$Q = 0.024 \text{ cfs}$$

$$n = 0.24$$

$$S = 0.25 \text{ ft/ft}$$

$$y = 0.054 \text{ ft}$$

Case 4:

$$Q = 0.025 \text{ cfs}$$

$$n = 0.24$$

$$S = 0.25 \text{ ft/ft}$$

$$y = 0.056 \text{ ft}$$

CAMELOT LANDFILL
1339-351-11-02
SHEET FLOW VELOCITY

Determine sheet flow velocity:

$$V = Q/A \quad (\text{assume unit flow width for the flow area, A})$$

Case 1:

$$Q = 0.046 \text{ cfs}$$
$$A = 0.138 \text{ sf}$$

V = 0.33 ft/s

Case 2:

$$Q = 0.050 \text{ cfs}$$
$$A = 0.146 \text{ sf}$$

V = 0.34 ft/s

Case 3:

$$Q = 0.024 \text{ cfs}$$
$$A = 0.054 \text{ sf}$$

V = 0.45 ft/s

Case 4:

$$Q = 0.025 \text{ cfs}$$
$$A = 0.056 \text{ sf}$$

V = 0.45 ft/s

Permissible non-erodible velocity is 5.0 ft/s. Therefore, expected sheet flow velocity is acceptable on the final cover system top and side slopes.



**STANDARD
SPECIFICATIONS
FOR CONSTRUCTION
AND MAINTENANCE OF
HIGHWAYS, STREETS,
AND BRIDGES**

**Adopted by the
Texas Department of Transportation**

June 1, 2004

Add or reshape the mulch sod to meet the requirements of Section 162.3.B, "Finishing."

- B. Finishing.** Smooth and shape the area after planting to conform to the desired cross sections. Spread any excess soil uniformly over adjacent areas or dispose of the excess soil as directed.
- C. Straw or Hay Mulch.** Apply straw or hay mulch for "Spot Sodding" and "Mulch Sodding" uniformly over the area as shown on the plans. Apply straw mulch at 2 to 2-1/2 tons per acre. Apply hay mulch at 1-1/2 to 2 tons per acre. Use a tacking method over the mulched area.

162.4. Measurement. "Spot Sodding," "Block Sodding," and "Straw or Hay Mulch" will be measured by the square yard in its final position. "Mulch Sodding" will be measured by the square yard in its final position or by the cubic yard in vehicles as delivered to the planting site.

162.5. Payment. The work performed and materials furnished in accordance with this Item and measured as provided under "Measurement" will be paid for at the unit price bid for "Spot Sodding," "Block Sodding," "Straw or Hay Mulch," or "Mulch Sodding." This price is full compensation for securing a source, excavation, loading, hauling, placing, rolling, finishing, furnishing materials, equipment, labor, tools, supplies, and incidentals. Fertilizer will not be paid for directly but will be subsidiary to this Item.

Unless otherwise specified on the plans, water, except for that used for maintaining and preparing the sod before planting, will be measured and paid for in accordance with Item 168, "Vegetative Watering."

ITEM 164

SEEDING FOR EROSION CONTROL

164.1. Description. Provide and install temporary or permanent seeding for erosion control as shown on the plans or as directed.

164.2. Materials.

- A. Seed.** Provide seed from the previous season's crop meeting the requirements of the Texas Seed Law, including the testing and labeling for pure live seed (PLS = Purity x Germination). Furnish seed of the designated species, in labeled unopened bags or containers to the Engineer before planting. Use within 12 mo. From the date of the

164.2 to 164.2

analysis. When Buffalograss is specified, use seed that is treated with KNO_3 (potassium nitrate) to overcome dormancy.

Use Tables 1 through 4 to determine the appropriate seed mix and rates as specified on the plans.

Table 1
Permanent Rural Seed Mix

District and Planting Dates	Clay Soils		Sandy Soils	
	Species and Rates (lb. PLS/ac.)		Species and Rates (lb. PLS/ac.)	
1 (Paris) Feb. 1 – May 15	Green Sprangletop	0.3	Green Sprangletop	0.3
	Sideoats Grama (Haskell)	3.2	Bermudagrass	1.5
	Bermudagrass	1.8	Bahiagrass (Pensacola)	6.0
	Little Bluestem (Native)	1.7	Sand Lovegrass	0.6
	Illinois Bundleflower	1.0	Weeping Lovegrass (Ermelo)	0.8
			Partridge Pea	1.0
2 (Ft. Worth) Feb. 1 – May 15	Green Sprangletop	0.3	Green Sprangletop	0.3
	Sideoats Grama (El Reno)	2.7	Sand Lovegrass	0.5
	Bermudagrass	0.9	Bermudagrass	1.8
	Little Bluestem (Native)	1.0	Weeping Lovegrass (Ermelo)	0.8
	Blue Grama (Hachita)	0.9	Sand Dropseed	0.4
	Illinois Bundleflower	1.0	Partridge Pearl	1.0
3 (Wichita Falls) Feb. 1 – May 15	Green Sprangletop	0.3	Green Sprangletop	0.3
	Sideoats Grama (El Reno)	2.7	Bermudagrass	1.2
	Bermudagrass	0.9	Sand Dropseed	0.4
	Buffalograss (Texoka)	1.6	Sand Bluestem	2.4
	Western Wheatgrass	2.1	Sand Lovegrass	0.3
	Blue Grama (Hachita)	0.6	Weeping Lovegrass (Ermelo)	0.6
	Illinois Bundleflower	1.0	Purple Prairieclover	0.5
4 (Amarillo) Feb. 15 – May 15	Green Sprangletop	0.3	Green Sprangletop	0.3
	Sideoats Grama (El Reno)	3.6	Weeping Lovegrass (Ermelo)	0.8
	Blue Grama (Hachita)	1.2	Blue Grama (Hachita)	1.0
	Buffalograss (Texoka)	1.6	Sand Dropseed	0.3
	Illinois Bundleflower	1.0	Sand Bluestem	1.8
			Purple Prairieclover	0.5
5 (Lubbock) Feb. 15 – May 15	Green Sprangletop	0.3	Green Sprangletop	0.3
	Sideoats Grama (El Reno)	3.6	Weeping Lovegrass (Ermelo)	0.8
	Blue Grama (Hachita)	1.2	Blue Grama (Hachita)	1.0
	Buffalograss (Texoka)	1.6	Sand Dropseed	0.3
	Illinois Bundleflower	1.0	Sand Bluestem	1.8
			Purple Prairieclover	0.5

Table 1 (continued)
Permanent Rural Seed Mix

District and Planting Dates	Clay Soils		Sandy Soils	
	Species and Rates (lb. PLS/ac.)		Species and Rates (lb. PLS/ac.)	
6 (Odessa) Feb. 1 – May 15	Green Sprangletop	0.3	Green Sprangletop	0.3
	Sideoats Grama (Haskell)	2.3	Blue Grama	0.8
	Blue Grama (Hachita)	0.8	Sand Dropseed	0.4
	Alkali Sacaton	0.4	Weeping Lovegrass (Ermelo)	0.6
	Galleta	2.1	Indian Ricegrass	3.0
	Illinois Bundleflower	1.0	Purple Prairieclover	0.5
7 (San Angelo) Feb. 1 – May 1	Green Sprangletop	0.3	Green Sprangletop	0.3
	Sideoats Grama (Haskell)	2.7	Sideoats Grama (Haskell)	2.7
	Buffalograss (Texoka)	1.6	Weeping Lovegrass (Ermelo)	0.6
	Little Bluestem (Native)	1.7	Sand Dropseed	0.4
	Blue Grama (Hachita)	0.9	Purple Prairieclover	0.5
	Galleta	1.6		
8 (Abilene) Feb. 1 – May 15	Green Sprangletop	0.3	Green Sprangletop	0.3
	Sideoats Grama (Haskell)	2.7	Sand Bluestem	3.0
	Blue Grama (Hachita)	0.9	Weeping Lovegrass (Ermelo)	1.2
	Galleta	1.6	Sand Dropseed	0.5
	Buffalograss (Texoka)	1.6	Purple Prairieclover	0.5
	Little Bluestem (Native)	1.7		
9 (Waco) Feb. 1 – May 15	Green Sprangletop	0.3	Green Sprangletop	0.3
	Bermudagrass	1.2	Bermudagrass	2.4
	Sideoats Grama (Haskell)	3.6	Sand Dropseed	0.5
	Little Bluestem (Native)	2.0	Weeping Lovegrass (Ermelo)	0.8
	Illinois Bundleflower	1.0	Partridge Pea	1.0
10 (Tyler) Feb. 1 – May 15	Green Sprangletop	0.3	Green Sprangletop	0.3
	Bermudagrass	1.8	Bermudagrass	1.8
	Bahiagrass (Pensacola)	9.0	Bahiagrass (Pensacola)	9.0
	Sideoats Grama (Haskell)	2.7	Weeping Lovegrass (Ermelo)	0.5
	Illinois Bundleflower	1.0	Sand Lovegrass	0.5
			Lance-Leaf Coreopsis	1.0

Table 1 (continued)
Permanent Rural Seed Mix

District and Planting Dates	Clay Soils		Sandy Soils	
	Species and Rates (lb. PLS/ac.)		Species and Rates (lb. PLS/ac.)	
11 (Lufkin) Feb. 1 – May 15	Green Sprangletop	0.3	Green Sprangletop	0.3
	Bermudagrass	1.8	Bermudagrass	2.1
	Bahiagrass (Pensacola)	9.0	Bahiagrass (Pensacola)	9.0
	Sideoats Grama (Haskell)	2.7	Sand Lovegrass	0.5
	Illinois Bundleflower	1.0	Lance-Leaf Coreopsis	1.0
12 (Houston) Jan. 15 – May 15	Green Sprangletop	0.3	Green Sprangletop	0.3
	Bermudagrass	2.1	Bermudagrass	2.4
	Sideoats Grama (Haskell)	3.2	Bahiagrass (Pensacola)	10.5
	Little Bluestem (Native)	1.4	Weeping Lovegrass (Ermelo)	0.5
	Illinois Bundleflower	1.0	Lance-Leaf Coreopsis	1.0
13 (Yoakum) Jan. 15 – May 15	Green Sprangletop	0.3	Green Sprangletop	0.3
	Sideoats Grama (Haskell)	3.6	Bermudagrass	1.8
	Bermudagrass	1.8	Bahiagrass (Pensacola)	6.0
	Little Bluestem (Native)	1.4	Sand Lovegrass	0.6
	Illinois Bundleflower	1.0	Weeping Lovegrass (Ermelo)	0.6
14 (Austin) Feb. 1 – May 15	Green Sprangletop	0.3	Green Sprangletop	0.3
	Bermudagrass	0.9	Bermudagrass	2.4
	Sideoats Grama (Haskell)	2.7	Weeping Lovegrass (Ermelo)	0.8
	Little Bluestem (Native)	1.0	Sand Lovegrass	0.8
	Blue Grama (Hachita)	0.9	Partridge Pea	1.0
	Illinois Bundleflower	1.0		
15 (San Antonio) Feb. 1 – May 1	Green Sprangletop	0.3	Green Sprangletop	0.3
	Bermudagrass	1.2	Bermudagrass	1.8
	Sideoats Grama (Haskell)	2.7	Lehmans Lovegrass	0.6
	Little Bluestem (Native)	1.4	Sand Lovegrass	0.6
	Plains Bristlegrass	1.2	Buffelgrass (Common)	0.4
	Illinois Bundleflower	1.0	Partridge Pea	1.0
16 (Corpus Christi) Jan. 1 – May 1	Green Sprangletop	0.3	Green Sprangletop	0.3
	Sideoats Grama (Haskell)	2.7	Bermudagrass	1.8
	Bermudagrass	1.8	Buffelgrass (Common)	0.4
	Buffalograss (Texoka)	1.6	Sand Lovegrass	0.6
	Plains Bristlegrass	1.2	Lehmans Lovegrass	0.6
	Illinois Bundleflower	1.0	Purple Prairieclover	0.5

Table 1 (continued)
Permanent Rural Seed Mix

District and Planting Dates	Clay Soils		Sandy Soils	
	Species and Rates (lb. PLS/ac.)		Species and Rates (lb. PLS/ac.)	
17 (Bryan) Feb. 1 – May 15	Green Sprangletop	0.3	Green Sprangletop	0.3
	Bermudagrass	1.5	Bermudagrass	1.5
	Sideoats Grama (Haskell)	3.6	Bahiagrass (Pensacola)	7.5
	Little Bluestem (Native)	1.7	Weeping Lovegrass (Ermelo)	0.6
	Illinois Bundleflower	1.0	Sand Lovegrass	0.6
			Lance-Leaf Coreopsis	1.0
18 (Dallas) Feb. 1 – May 15	Green Sprangletop	0.3	Green Sprangletop	0.3
	Bermudagrass	1.2	Bermudagrass	1.8
	Sideoats Grama (El Reno)	2.7	Weeping Lovegrass (Ermelo)	0.6
	Little Bluestem (Native)	2.0	Sand Lovegrass	0.6
	Buffalograss (Texoka)	1.6	Sand Dropseed	0.4
	Illinois Bundleflower	1.0	Partridge Pea	1.0
19 (Atlanta) Feb. 1 – May 15	Green Sprangletop	0.3	Green Sprangletop	0.3
	Bermudagrass	2.4	Bermudagrass	2.1
	Sideoats Grama (Haskell)	4.5	Bahiagrass (Pensacola)	7.5
	Illinois Bundleflower	1.0	Sand Lovegrass	0.6
			Lance-Leaf Coreopsis	1.0
20 (Beaumont) Jan. 15 – May 15	Green Sprangletop	0.3	Green Sprangletop	0.3
	Bermudagrass	2.7	Bermudagrass	2.1
	Sideoats Grama (Haskell)	4.1	Bahiagrass (Pensacola)	7.5
	Illinois Bundleflower	1.0	Sand Lovegrass	0.6
			Lance-Leaf Coreopsis	1.0
21 (Pharr) Jan. 15 – May 15	Green Sprangletop	0.3	Green Sprangletop	0.3
	Sideoats Grama (Haskell)	3.6	Bermudagrass	1.8
	Plains Bristlegrass	1.2	Buffelgrass (Common)	0.4
	Buffalograss (Texoka)	1.6	Sand Dropseed	0.4
	Bermudagrass	1.2	Lehmans Lovegrass	0.6
	Illinois Bundleflower	1.0	Purple Prairieclover	0.5
22 (Laredo) Jan. 15 – May 1	Green Sprangletop	0.3	Green Sprangletop	0.3
	Sideoats Grama (Haskell)	3.6	Bermudagrass	1.8
	Bermudagrass	1.2	Buffelgrass (Common)	0.4
	Buffalograss (Texoka)	1.6	Sand Dropseed	0.4
	Plains Bristlegrass	1.2	Lehmans Lovegrass	0.6
	Illinois Bundleflower	1.0	Purple Prairieclover	0.5

Table 1 (continued)
Permanent Rural Seed Mix

District and Planting Dates	Clay Soils		Sandy Soils	
	Species and Rates (lb. PLS/ac.)		Species and Rates (lb. PLS/ac.)	
23 (Brownwood) Feb. 1 – May 15	Green Sprangletop	0.3	Green Sprangletop	0.3
	Sideoats Grama (Haskell)	2.7	Bermudagrass	1.8
	Bermudagrass	0.6	Weeping Lovegrass (Ermelo)	0.6
	Blue Grama (Hachita)	0.9	Sand Lovegrass	0.6
	Galleta	2.1	Sand Dropseed	0.4
	Illinois Bundleflower	1.0	Purple Prairieclover	0.5
24 (El Paso) Feb. 1 – May 15	Green Sprangletop	0.3	Green Sprangletop	0.3
	Sideoats Grama (Butte)	2.7	Sand Dropseed	0.4
	Blue Grama (Hachita)	0.9	Lehmans Lovegrass	0.9
	Galleta	2.1	Blue Grama (Hachita)	1.0
	Alkali Sacaton	0.4	Indian Ricegrass	1.6
	Illinois Bundleflower	1.0	Purple Prairieclover	0.5
25 (Childress) Feb. 1 – May 15	Green Sprangletop	0.3	Green Sprangletop	0.3
	Sideoats Grama (El Reno)	2.7	Weeping Lovegrass (Ermelo)	1.2
	Blue Grama (Hachita)	0.9	Sand Dropseed	0.5
	Western Wheatgrass	2.1	Sand Lovegrass	0.8
	Galleta	1.6	Purple Prairieclover	0.5
	Illinois Bundleflower	1.0		

Table 2
Permanent Urban Seed Mix

District and Planting Dates	Clay Soils Species and Rates (lb. PLS/ac.)		Sandy Soils Species and Rates (lb. PLS/ac.)	
1 (Paris) Feb. 1 – May 15	Green Sprangletop Bermudagrass Sideoats Grama (Haskell)	0.3 2.4 4.5	Green Sprangletop Bermudagrass	0.3 5.4
2 (Ft. Worth) Feb. 1 – May 15	Green Sprangletop Sideoats Grama (El Reno) Bermudagrass Buffalograss (Texoka)	0.3 3.6 2.4 1.6	Green Sprangletop Sideoats Grama (El Reno) Bermudagrass Sand Dropseed	0.3 3.6 2.1 0.3
3 (Wichita Falls) Feb. 1 – May 15	Green Sprangletop Sideoats Grama (El Reno) Bermudagrass Buffalograss (Texoka)	0.3 4.5 1.8 1.6	Green Sprangletop Sideoats Grama (El Reno) Bermudagrass Sand Dropseed	0.3 3.6 1.8 0.4
4 (Amarillo) Feb. 15 – May 15	Green Sprangletop Sideoats Grama (El Reno) Blue Grama (Hachita) Buffalograss (Texoka)	0.3 3.6 1.2 1.6	Green Sprangletop Sideoats Grama (El Reno) Blue Grama (Hachita) Sand Dropseed Buffalograss (Texoka)	0.3 2.7 0.9 0.4 1.6
5 (Lubbock) Feb. 15 – May 15	Green Sprangletop Sideoats Grama (El Reno) Blue Grama (Hachita) Buffalograss (Texoka)	0.3 3.6 1.2 1.6	Green Sprangletop Sideoats Grama (El Reno) Blue Grama (Hachita) Sand Dropseed Buffalograss (Texoka)	0.3 2.7 0.9 0.4 1.6
6 (Odessa) Feb. 1 – May 15	Green Sprangletop Sideoats Grama (Haskell) Blue Grama (Hachita) Buffalograss (Texoka)	0.3 3.6 1.2 1.6	Green Sprangletop Sideoats Grama (Haskell) Sand Dropseed Blue Grama (Hachita) Buffalograss (Texoka)	0.3 2.7 0.4 0.9 1.6
7 (San Angelo) Feb. 1 – May 1	Green Sprangletop Sideoats Grama (Haskell) Buffalograss (Texoka)	0.3 7.2 1.6	Green Sprangletop Sideoats Grama (Haskell) Sand Dropseed Blue Grama (Hachita) Buffalograss (Texoka)	0.3 3.2 0.3 0.9 1.6

Table 2 (continued)
Permanent Urban Seed Mix

District and Planting Dates	Clay Soils Species and Rates (lb. PLS/ac.)	Sandy Soils Species and Rates (lb. PLS/ac.)
8 (Abilene) Feb. 1 – May 15	Green Sprangletop 0.3 Sideoats Grama (Haskell) 3.6 Blue Grama (Hachita) 1.2 Buffalograss (Texoka) 1.6	Green Sprangletop 0.3 Sand Dropseed 0.3 Sideoats Grama (Haskell) 3.6 Blue Grama (Hachita) 0.8 Buffalograss (Texoka) 1.6
9 (Waco) Feb. 1 – May 15	Green Sprangletop 0.3 Bermudagrass 1.8 Buffalograss (Texoka) 1.6 Sideoats Grama (Haskell) 4.5	Green Sprangletop 0.3 Buffalograss (Texoka) 1.6 Bermudagrass 3.6 Sand Dropseed 0.4
10 (Tyler) Feb. 1 – May 15	Green Sprangletop 0.3 Bermudagrass 2.4 Sideoats Grama (Haskell) 4.5	Green Sprangletop 0.3 Bermudagrass 5.4
11 (Lufkin) Feb. 1 – May 15	Green Sprangletop 0.3 Bermudagrass 2.4 Sideoats Grama (Haskell) 4.5	Green Sprangletop 0.3 Bermudagrass 5.4
12 (Houston) Jan. 15 – May 15	Green Sprangletop 0.3 Sideoats Grama (Haskell) 4.5 Bermudagrass 2.4	Green Sprangletop 0.3 Bermudagrass 5.4
13 (Yoakum) Jan. 15 – May 15	Green Sprangletop 0.3 Sideoats Grama (Haskell) 4.5 Bermudagrass 2.4	Green Sprangletop 0.3 Bermudagrass 5.4
14 (Austin) Feb. 1 – May 15	Green Sprangletop 0.3 Bermudagrass 2.4 Sideoats Grama (Haskell) 3.6 Buffalograss (Texoka) 1.6	Green Sprangletop 0.3 Bermudagrass 4.8 Buffalograss (Texoka) 1.6
15 (San Antonio) Feb. 1 – May 1	Green Sprangletop 0.3 Sideoats Grama (Haskell) 3.6 Bermudagrass 2.4 Buffalograss (Texoka) 1.6	Green Sprangletop 0.3 Bermudagrass 4.8 Buffalograss (Texoka) 1.6
16 (Corpus Christi) Jan. 1 – May 1	Green Sprangletop 0.3 Sideoats Grama (Haskell) 3.6 Bermudagrass 2.4 Buffalograss (Texoka) 1.6	Green Sprangletop 0.3 Bermudagrass 4.8 Buffalograss (Texoka) 1.6

Table 2 (continued)
Permanent Urban Seed Mix

District and Planting Dates	Clay Soils Species and Rates (lb. PLS/ac.)	Sandy Soils Species and Rates (lb. PLS/ac.)
17 (Bryan) Feb. 1 – May 15	Green Sprangletop 0.3 Bermudagrass 2.4 Sideoats Grama (Haskell) 4.5	Green Sprangletop 0.3 Bermudagrass 5.4
18 (Dallas) Feb. 1 – May 15	Green Sprangletop 0.3 Sideoats Grama (El Reno) 3.6 Buffalograss (Texoka) 1.6 Bermudagrass 2.4	Green Sprangletop 0.3 Buffalograss (Texoka) 1.6 Bermudagrass 3.6 Sand Dropseed 0.4
19 (Atlanta) Feb. 1 – May 15	Green Sprangletop 0.3 Bermudagrass 2.4 Sideoats Grama (Haskell) 4.5	Green Sprangletop 0.3 Bermudagrass 5.4
20 (Beaumont) Jan. 15 – May 15	Green Sprangletop 0.3 Bermudagrass 2.4 Sideoats Grama (Haskell) 4.5	Green Sprangletop 0.3 Bermudagrass 5.4
21 (Pharr) Jan. 15 – May 15	Green Sprangletop 0.3 Sideoats Grama (Haskell) 3.6 Buffalograss (Texoka) 1.6 Bermudagrass 2.4	Green Sprangletop 0.3 Buffalograss (Texoka) 1.6 Bermudagrass 3.6 Sand Dropseed 0.4
22 (Laredo) Jan. 15 – May 1	Green Sprangletop 0.3 Sideoats Grama (Haskell) 4.5 Buffalograss (Texoka) 1.6 Bermudagrass 1.8	Green Sprangletop 0.3 Buffalograss (Texoka) 1.6 Bermudagrass 3.6 Sand Dropseed 0.4
23 (Brownwood) Feb. 1 – May 15	Green Sprangletop 0.3 Sideoats Grama (Haskell) 3.6 Bermudagrass 1.2 Blue Grama (Hachita) 0.9	Green Sprangletop 0.3 Buffalograss (Texoka) 1.6 Bermudagrass 3.6 Sand Dropseed 0.4
24 (El Paso) Feb. 1 – May 15	Green Sprangletop 0.3 Sideoats Grama (Butte) 3.6 Blue Grama (Hachita) 1.2 Buffalograss (Texoka) 1.6	Green Sprangletop 0.3 Buffalograss (Texoka) 1.6 Sand Dropseed 0.4 Blue Grama (Hachita) 1.8
25 (Childress) Feb. 1 – May 15	Green Sprangletop 0.3 Sideoats Grama (El Reno) 3.6 Blue Grama (Hachita) 1.2 Buffalograss (Texoka) 1.6	Green Sprangletop 0.3 Sand Dropseed 0.4 Buffalograss (Texoka) 1.6 Bermudagrass 1.8

Table 3
Temporary Cool Season Seeding

Districts	Dates	Seed Mix and Rates (lb./ac.)
Paris (1), Amarillo (4), Lubbock (5), Dallas (18)	September 1 – November 30	Tall Fescue 4.5 Western Wheatgrass 5.6 Wheat (Red, Winter) 34
Odessa (6), San Angelo (7), El Paso (24)	September 1 – November 30	Western Wheatgrass 8.4 Wheat (Red, Winter) 50
Waco (9), Tyler (10), Lufkin (11), Austin (14), San Antonio (15), Bryan (17), Atlanta (19)	September 1 – November 30	Tall Fescue 4.5 Oats 24 Wheat 34
Houston (12), Yoakum (13), Corpus Christi (16), Beaumont (20), Pharr (21), Laredo (22)	September 1 – November 30	Oats 72
Ft. Worth (2), Wichita Falls (3), Abilene (8), Brownwood (23), Childress (25)	September 1 – November 30	Tall Fescue 4.5 Western Wheatgrass 5.6 Cereal Rye 34

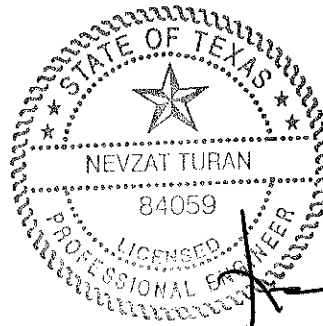
Table 4
Temporary Warm Season Seeding

Districts	Dates	Seed Mix and Rates (lb./ac.)
All	May 1 – August 31	Foxtail Millet 34

- B. Fertilizer.** Use fertilizer in conformance with Article 166.2, "Materials."
- C. Vegetative Watering.** Use water that is clean and free of industrial wastes and other substances harmful to the growth of vegetation.
- D. Mulch.**
1. **Straw or Hay Mulch.** Use straw or hay mulch in conformance with Article 162.2.E, "Mulch."
 2. **Cellulose Fiber Mulch.** Use only cellulose fiber mulches that are on the approved list published in "Field Performance of Erosion Control Products," available from the Maintenance Division. Submit 1 full set of manufacturer's literature for the selected material. Keep mulch dry until applied. Do not use molded or rotted material.
- E. Tacking Methods.** Use a tacking agent applied in accordance with the manufacturer's recommendations or a crimping method on all straw or

APPENDIX III-F-E

**PERMITTED LANDFILL CONDITION
HYDROLOGIC CALCULATIONS**



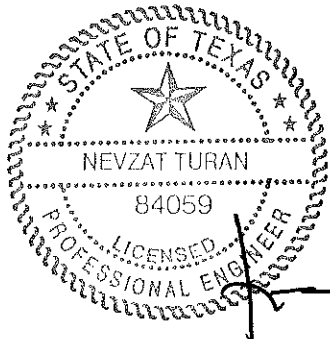
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Includes pages III-F-E-1 through III-F-E-120

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Permitted Condition Hydrologic Calculations	IIIF-E-1
Hypothetical Storm Data	IIIF-E-2
Precipitation Loss Data	IIIF-E-4
Hydrograph Development Information	IIIF-E-10
HEC-1 Output – Updated Permitted 25-Year, 24-Hour Storm Event	IIIF-E-20
Volume Calculations	IIIF-E-110
Velocity Calculations	IIIF-E-115



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PERMITTED CONDITION HYDROLOGIC CALCULATIONS

Appendix IIIF-E presents the hydrologic calculations for the updated permitted conditions summarized on the Sheet IIIF-E-16 and Sheet IIIF-E-17 drawings. The following summarizes the content of this appendix:

- Precipitation data are provided on page IIIF-E-3.
- Precipitation loss information is included on pages IIIF-E-4 through IIIF-E-9.
- Hydrograph development information is presented on IIIF-E-10 through IIIF-E-19.
- A comparison between the existing permitted, updated permitted, and proposed drainage conditions is presented in Section 4 of Appendix IIIF – Drainage Design Report.
- The HEC-1 output for the 25-year storm event for the updated permitted conditions is presented on IIIF-E-20 through IIIF-E-109.

HYPOTHETICAL STORM DATA

Hypothetical Storm Data

Precipitation data taken from TP-40 and Hydro 35 rainfall data.

Time	5 min	15 min	60 min	2 hr	3 hr	6 hr	12 hr	24 hr
25-Year Event	0.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44
100-Year Event	0.88	1.87	4.30	5.45	5.75	6.80	8.30	9.45

TP-40 (*U.S. Department of Commerce, May 1961*) was used to identify precipitation values for storm durations ranging from 60 minutes to 24 hours.

Hydro 35 (*National Oceanic and Atmospheric Administration, June 1977*) was used to estimate precipitation for the 5 minute and 15 minute duration storm events.

PRECIPITATION LOSS DATA

CAMELOT LANDFILL
1339-351-11-02
PRECIPITATION LOSS DATA

Required: Determine the SCS curve numbers for both on-site and off-site drainage areas for use in the HEC-1 analysis.

- References:**
1. Dodson's and Associates, Inc., *ProHec-1 Plus Program Documentation*, 1995.
 2. United States Department of Agriculture, National Resource Conservation Service, Web Soil Survey for Hill County, Texas (<http://websoilsurvey.nrcs.usda.gov>).
 3. The Hydrologic Evaluation of Landfill Performance (HELP) Model - Engineering Documentation for version 3. EPA/600/R-94/168b, September 1994.

Note: Approximate non landfill areas within the permit boundary on SCS map (page IIIF-A-5).

Solution: Based on the soil survey information found in Ref. 2, hydrologic group D soils predominate the soils within the permit boundary drainage area (see pages IIIF-A-5 through IIIF-A-7).

Offsite areas O3, O4, and O5 and several onsite areas (CH2, CH3, CH4, CH4A, CH5, CH6, CH7A, CH7B, CH9, CH10, CH11, N1, N12, N13, N14, N15, N16, N17, N18, N19, S1, S2, S3, S4, and S5) were considered pasture land or range in fair condition. A curve number was selected using the table on page IIIF-E-6.

Use:	CN = 84
------	---------

Curve numbers for offsite areas O1, O1A, and O2 were calculated using an area-weighted average of rural and urban land uses, including pasture or range in fair condition, 1/4 acre average residential lots, and industrial districts. The calculated composite curve numbers are shown below.

Use:	CN = 87	for area O1
Use:	CN = 85	for area O1A
Use:	CN = 85	for area O2

The final cover system was assumed to be in place and the erosion layer will control precipitation loss. A curve number that is corrected for the surface slope of the erosion layer may be computed first using the chart on page IIIF-E-7 to select an un-adjusted curve number. Calculate the adjusted curve number using equation 34 from Ref. 3 (see page IIIF-E-7).

$$CN_{II} = 100 - (100 - CN_{IIo}) * (L^* / S^*) ^ (CN_{IIo}^{-0.81})$$

Use:	$CN_{IIo} = 84, L^* = (500/500), S^* = (.02/.04)$	for top dome surfaces
Use:	$CN_{IIo} = 84, L^* = (120/500), S^* = (.20/.04)$	for side slopes

Calculate:	CN = 84	for top dome surfaces
Calculate:	CN = 86	for side slopes

The pond areas are assumed to collect all precipitation for their areas:

Use:	CN = 100
------	----------

**TABLE 5.3 Values of SCS
Curve Number for Rural Areas**

Source: [McCuen, 1982]

Land Use Description	Hydrologic Soil Group			
	A	B	C	D
Fallow:				
Straight Row	77	86	91	94
Row Crops:				
Straight Row, Poor Condition	72	81	88	91
Straight Row, Good Condition	67	78	85	89
Contoured, Poor Condition	70	79	84	88
Contoured, Good Condition	65	75	82	86
Contoured and Terraced, Poor Condition	66	74	80	82
Contoured and Terraced, Good Condition	62	71	78	81
Small Grain:				
Straight Row, Poor Condition	65	76	84	88
Straight Row, Good Condition	63	75	83	87
Contoured, Poor Condition	63	74	82	85
Contoured, Good Condition	61	73	81	84
Contoured and Terraced, Poor Condition	61	72	79	82
Contoured and Terraced, Good Condition	59	70	78	81
Close-Seeded Legumes or Rotation Meadow				
Straight Row, Poor Condition	66	77	85	89
Straight Row, Good Condition	58	72	81	85
Contoured, Poor Condition	64	75	83	85
Contoured, Good Condition	55	69	78	83
Contoured and Terraced, Poor Condition	63	73	80	83
Contoured and Terraced, Good Condition	51	67	76	80
Pasture or Range:				
Poor Condition	68	79	86	89
Fair Condition	49	69	79	84
Good Condition	39	61	74	80
Contoured, Poor Condition	47	67	81	88
Contoured, Fair Condition	25	59	75	83
Contoured, Good Condition	6	35	70	79
Meadow, Good Condition	30	58	71	78
Woods or Forest Land:				
Poor Condition	45	66	77	83
Fair Condition	36	60	73	79
Good Condition	25	55	70	77
Farmsteads:	59	74	82	86

Initial and Uniform Loss Rate

An initial loss in inches (*STRIL*) and a constant loss rate (*CNSTL*) in inches per hour are specified for this method. All rainfall is lost until the volume of initial loss is satisfied. After the initial loss is satisfied, rainfall is lost at the constant rate.

This section provides guidance in selecting the values used for the initial loss and uniform loss rate in two ways:

1. By consulting previous studies of actual rainfall events for a particular watershed or region.
2. By relating the parameters to the SCS Curve Number, which can be estimated using the information presented earlier in this chapter.

Previous studies by the U.S. Army Corps of Engineers or other public agencies may provide guidance on selecting appropriate values for the initial loss and uniform loss rate for a particular location. Tables 5.4 through 5.6 list the values of initial and

loam, and clayey loam as specified by saturated hydraulic conductivity, capillary drive, porosity, and maximum relative saturation. Two levels of vegetation were described--a good stand of grass (bluegrass sod) and a poor stand of grass (clipped range). Slopes of 0.04, 0.10, 0.20, 0.35, and 0.50 ft/ft and slope lengths of 50, 100, 250, and 500 ft were used. Rainfalls of 1.1 inches, 1-hour duration and 2nd quartile Huff distribution and of 3.8 inches, 6-hour duration and balanced distribution were modeled.

The resulting regression equation used for adjusting the AMC-II curve number computed for default soils and vegetation placed at mild slopes, CN_{II_0} , is:

$$CN_{II} = 100 - (100 - CN_{II_0}) \cdot \left(\frac{L^{*2}}{S^*} \right) CN_{II_0}^{-0.81} \quad (34)$$

where

L^* = standardized dimensionless length, (L/500 ft)

S^* = standardized dimensionless slope, (S/0.04)

This same equation is used to adjust user-specified AMC-II curve numbers for surface slope conditions by substituting the user value for CN_{II_0} in Equation 34.

4.2.4 Adjustment of Curve Number for Frozen Soil

When the HELP program predicts frozen conditions to exist, the value of CN_{II} is increased, resulting in a higher calculated runoff. Knisel et al. (1985) found that this type of curve number adjustment in the CREAMS model resulted in improved predictions of annual runoff for several test watersheds. If the CN_{II} for unfrozen soil is less than or equal to 80, the CN_{II} for frozen soil conditions is set at 95. When the unfrozen soil CN_{II} is greater than 80, the CN_{II} is reset to be 98 on days when the program has determined the soil to be frozen. This adjustment results in an increase in CN_I and consequently a decrease in S_{mx} and S' (Equations 19, 26, and 30).

From Equations 19 and 21, it is apparent that as S' approaches zero, Q approaches P . In other words, as S' decreases, the calculated runoff becomes closer to being equal to the net rainfall which is most often, when frozen soil conditions exist, predominantly snowmelt. This will result in a decrease in infiltration under frozen soil conditions, which has been observed in numerous studies.

4.2.5 Summary of Daily Runoff Computation

The HELP model determines daily runoff by the following procedure:

where

- CN_{II} = AMC-II curve number for mild slope (unadjusted for slope)
- C_0 = regression constant for a given level of vegetation
- C_1 = regression constant for a given level of vegetation
- C_2 = regression constant for a given level of vegetation
- IR = infiltration correlation parameter for given soil type

The relationship between CN_{II} , the vegetative cover and default soil texture is shown graphically in Figure 8. Table 7 gives values of C_0 , C_1 , and C_2 for the five types of vegetative cover built into the HELP program.

4.2.3 Adjustment of Curve Number for Surface Slope

A regression equation was developed to adjust the AMC-II curve number for surface slope conditions. The regression was developed based on kinematic wave theory where

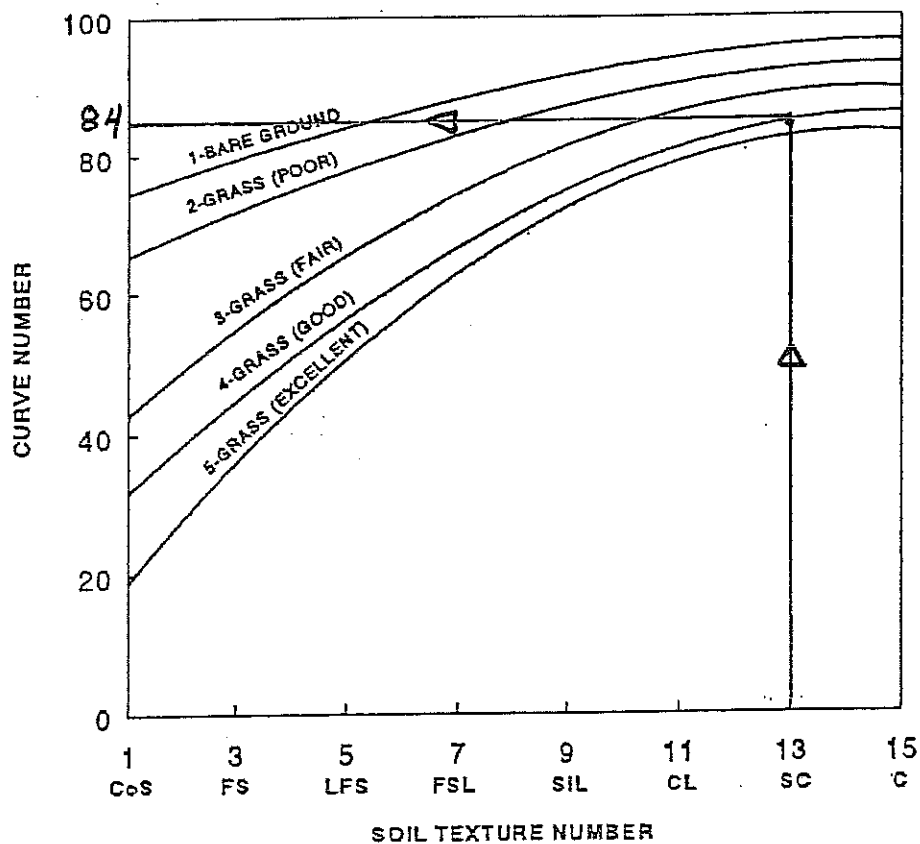


Figure 8. Relation between SCS Curve Number and Default Soil Texture Number for Various Levels of Vegetation

TABLE 7. CONSTANTS FOR USE IN EQUATION 32

Vegetative Cover	C_0	C_1	C_2
Bare Ground	96.77	-20.80	-54.94
Poor Grass	93.51	-24.85	-71.92
Fair Grass	90.09	-23.73	-158.4
Good Grass	86.72	-43.38	-151.2
Excellent Grass	83.83	-26.91	-229.4

the travel time of runoff from the top of a slope to the bottom of the slope is computed as follows:

$$t_{run} = \frac{1.5}{(i - I)^{1/3}} \left(\frac{L^2}{S} \right)^{1/3} \left(\frac{1.49}{n} \right)^{-2/3} \quad (33)$$

where

- t_{run} = runoff travel time (time of concentration), minutes
- i = steady-state rainfall intensity (rate), inches/hour
- I = steady-state infiltration rate, inches/hour
- L = slope length, feet
- S = surface slope, dimensionless
- n = Manning's roughness coefficient, dimensionless

A decrease in travel time results in less infiltration because less time is available for infiltration to occur.

Using the KINEROS kinematic runoff and erosion model (Woolhiser, Smith, and Goodrich, 1990), hundreds of runoff estimates were generated using different combinations of soil texture class, level of vegetation, slope, slope length, and rainfall depth, duration and temporal distribution. Using these estimates, the curve number that would yield the estimated runoff was calculated from the rainfall depth and the runoff estimate. These curve numbers were regressed with the slope length, surface slope and the curve number that would be generated for the soil texture and level of vegetation placed at a mild slope. The four soil textures used included loamy sand, sandy loam,

HYDROGRAPH DEVELOPMENT INFORMATION

HYDROGRAPH DEVELOPMENT INFORMATION

Landfill Areas

Direct runoff methods (i.e., kinematic wave) have been used for the landfill final cover areas. The kinematic wave method has been used to model the four percent slope top dome areas before flow is intercepted by top dome swales. The kinematic wave method is a physically based method using slope, surface roughness, catchment lengths and areas. This method does not consider attenuation for flood wave; as a consequence, this method provides for a conservative analysis. The following typical parameters for the direct runoff method have been developed for the landfill areas consistent with the parameters used in the currently approved hydrologic analysis (HEC-1 output file included in pages III-F-E-20 through III-F-E-109).

Kinematic wave parameters for overland flow:

- Slope: Varies from 0.02 to 0.20 ft/ft landfill slopes
- N: 0.35 Manning's friction coefficient for sheet flow
- L: Represents a typical distance between swales for overland flow.

Percentage of drainage area represented by this element is 100 percent.

Muskingum-Cunge routing is used along with the kinematic wave method to estimate hydrographs at the outfall of each separate drainage area analyzed using the direct runoff method.

Muskingum-Cunge routing data for swale:

- Swale length (ft): Typical swale lengths for each drainage area were used.
- Swale bottom slope (ft/ft): 0.005 ft/ft
- Swale roughness coefficient: 0.03
- Swale type: A trapezoidal channel was used with no bottom width to simulate a triangular channel.

Muskingum-Cunge routing data for channels:

- Channel length (ft): The length of the channel section.

- Channel slope (ft/ft): Varies from 0.001 to 0.011.
- Channel roughness coefficient: 0.03 for grass lined.
- Channel type: A trapezoidal channel was used with varying bottom width and 3:1 side slopes.

Non-Landfill Final Cover Areas

Hydrographs for a portion of the non-landfill final cover areas within the permit boundary (e.g., pond areas) and all off-site areas were developed using the Snyder unit hydrograph method. Espey "10-Minute" method has been used to estimate Snyder parameters. Snyder parameter estimations are provided on the pages IIF-E-14 and IIF-E-15.

As discussed in Section 2 of Appendix IIF, hydrographs for the areas outside of the permit boundary (O1, O1A, O2, O3, O4, and O5), and larger areas inside the permit boundary (S1, S2, S3, S4, S5, N1, N12, N13, N14, N15, 16, N17, N18, and N19) were developed using the Snyder unit hydrograph method. The percent imperviousness ranges from 2 percent to 23 percent for the non-landfill on-site and off-site areas, which represents the majority of the watersheds as undeveloped. Pond areas are assumed to be 100 percent impervious, and areas with significant channel surface or paved surfaces were assigned higher percentages of impervious area, as shown on IIF-E-14.

Drainage Areas

The drainage areas used for this analysis are shown on Sheet IIF-E-16 and Sheet IIF-E-17. The routing scheme for the updated permitted condition is shown in the HEC-1 output file presented on pages IIF-E-20 through IIF-E-109.

ESPEY 10-MINUTE METHOD PARAMETERS

Snyder's Hydrograph Coefficients (Espey's 10 Minute Method)

Updated Permitted Conditions

Area No.	Area (acres)	Max. Flow Length (L) (ft)	S (ft/ft)	I (%)	Manning "n"	Φ^1	T_r^2 (min)	T_{lag}^3 (min)	T_{lag} (hr)	Area ⁴ (sq mi)	q_p^5 (cfs/sq mi)	C_p^6
O1	87.47	3,380	0.0101	23	0.04	0.80	25.7	23.2	0.39	0.1367	1059.5	0.64
O1A	23.42	2,285	0.0132	4	0.04	0.85	32.7	30.2	0.50	0.0366	864.1	0.68
O2	1008.38	14,770	0.0050	18	0.04	0.81	45.3	42.8	0.71	1.5756	524.7	0.58
O3	16.18	835	0.0611	2	0.04	0.86	20.4	17.9	0.30	0.0253	1452.4	0.68
O4	86.04	3,840	0.0180	10	0.04	0.84	28.4	25.9	0.43	0.1344	954.1	0.64
O5	116.47	2,140	0.0121	2	0.04	0.86	38.0	35.5	0.59	0.1820	690.4	0.64
S1	10.40	908	0.0022	2	0.04	0.86	47.7	45.2	0.75	0.0163	595.4	0.70
S2	31.53	1,538	0.0040	2	0.04	0.86	46.4	43.9	0.73	0.0493	586.8	0.67
S3	20.21	1,076	0.0019	2	0.04	0.86	51.8	49.3	0.82	0.0316	531.3	0.68
S4	57.41	2,475	0.0024	2	0.04	0.86	58.7	56.2	0.94	0.0897	445.7	0.65
S5	0.67	165	0.0363	2	0.04	0.86	16.0	13.5	0.23	0.0010	2137.5	0.75
N1	11.26	880	0.0273	2	0.04	0.86	25.3	22.8	0.38	0.0176	1172.1	0.70
N12	7.96	700	0.0214	2	0.04	0.86	25.5	23.0	0.38	0.0124	1179.0	0.71
N13	18.73	1,368	0.0117	2	0.04	0.86	34.6	32.1	0.53	0.0293	821.8	0.69
N14	26.06	861	0.0279	2	0.04	0.86	25.0	22.5	0.38	0.0407	1146.5	0.67
N15	19.93	1,078	0.0148	2	0.04	0.86	30.8	28.3	0.47	0.0311	926.1	0.68
N16	2.72	351	0.0627	2	0.04	0.86	16.6	14.1	0.24	0.0042	1943.8	0.71
N17	4.32	60	0.1000	2	0.04	0.86	9.8	7.3	0.12	0.0068	3339.4	0.64

¹ Conveyance efficiency coefficient from Dodson & Associates Inc., *ProHec-1 Program Documentation*, 1995, pages 6-19 and 6-20.

² $T_r = 3.1(L^{0.23})(S^{0.25})(\Phi^{0.18})(\Phi^{1.57})$

³ $T_{lag} = T_r - \Delta t/2$

⁴ From area summary sheet

⁵ $q_p = 31600(A^{0.06})(T_r^{-1.07})$

⁶ $C_p = 49.375(A^{-0.06})(T_r^{-1.07})(T_{lag})$

T_r = surface runoff to unit hydrograph peak (min)

L_c = distance along main channel from study point to watershed boundary (ft)

S = main channel slope (ft/ft)

I = impervious cover within the watershed (%)

T_{lag} = watershed lag time (min)

Δt = computation interval (minutes)

q_p = unit hydrograph peak discharge (cfs/sq mi)

C_p = Snyder's peaking coefficient

Snyder Unit Hydrograph uses lag time (T_{lag}) and peaking coefficient accounting for flood wave and watershed storage conditions.

Drainage area "O1" is used in this example.

Estimated Watershed specific parameters

A =	87.47	acres	watershed area
L =	3580	feet	maximum flow length with this watershed
S =	0.0101	feet/feet	watershed slope
I =	23	percent (%)	watershed imperviousness
n =	0.04		Manning's coefficient

Calculate T_r : time beginning of surface runoff to the unit hydrograph peak in minutes

$$T_r = 3.1(L^{0.23})(S^{-0.25})(I^{-0.18})(\Phi^{1.57})$$

Estimate : conveyance efficiency coefficient

See figure 6.12 on page IIIF-E-18 for estimating

Φ = for 23 percent impervious cover and $n = 0.04$

$$\Phi = 0.8$$

$$T_r = 3.1(3580^{0.23})(.0101^{-0.25})(23^{-0.18})(0.8^{1.57})$$

$$T_r = 25.7 \quad \text{min}$$

Calculate T_{lag} : watershed lag time

$$T_{lag} = T_r - (\Delta t/2)$$

$$T_{lag} = 23.2 \quad \text{minutes}$$

$$T_{lag} = 0.39 \quad \text{hours}$$

Δt is calculation interval, and 5 minutes is used in the HEC - 1 modeling in this project

$$A = A/640$$

$$A = 0.1367 \quad \text{square miles}$$

Calculate q_p : peak discharge of unit hydrograph per unit area (cfs/sq. mi).

$$q_p = 31600(A^{-0.04})(T_r^{-1.07})$$

$$q_p = 31600(0.1367^{-0.04})(25.7^{-1.07})$$

$$q_p = 1059.5 \quad \text{cfs/sq. mi}$$

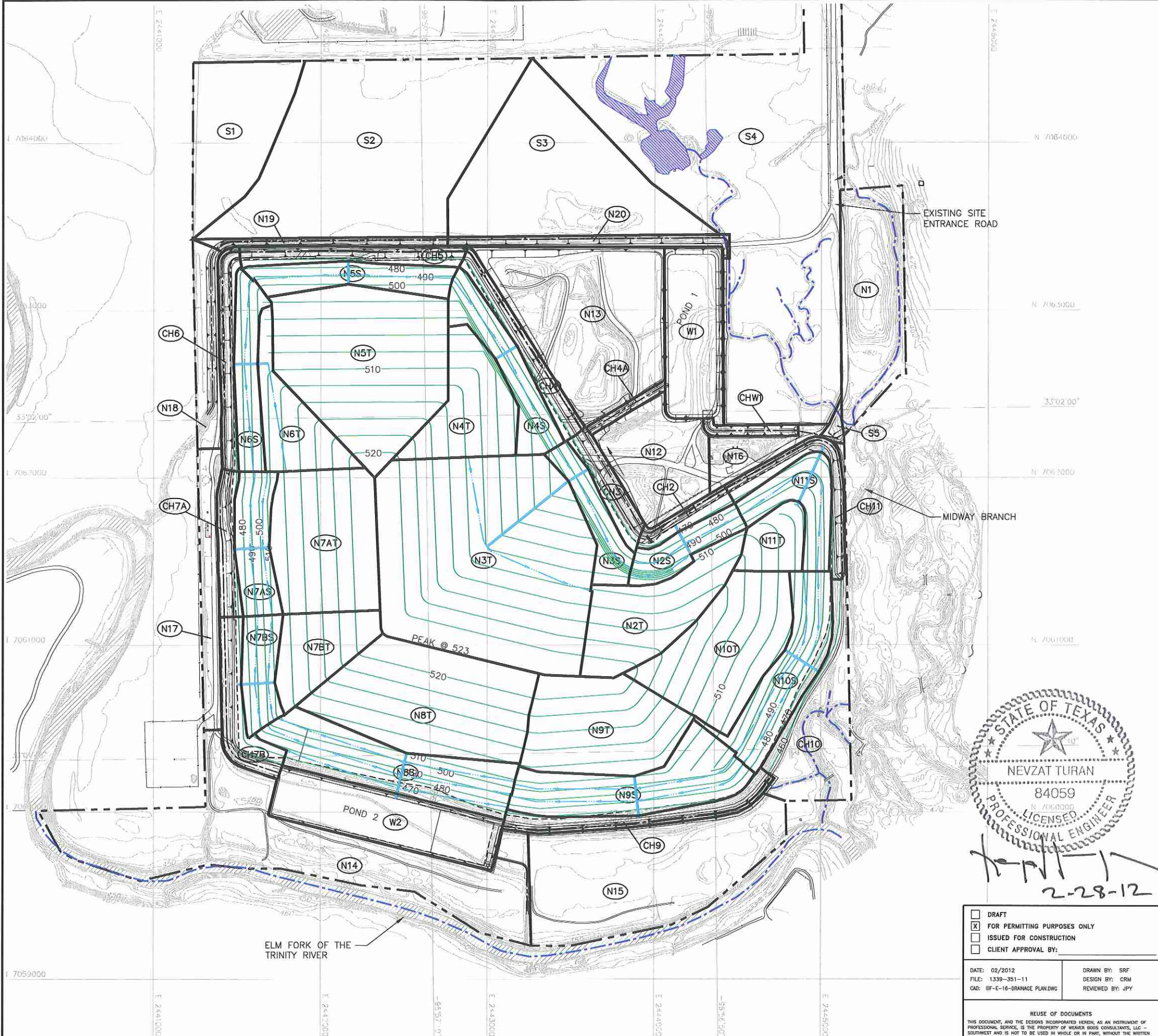
Calculate Peaking coefficient C_p :

$$C_p = 49.375(A^{-0.04})(T_r^{-1.07})(T_{lag})$$

$$C_p = 49.375(0.1367^{-0.04})(25.7^{-1.07})(0.39)$$

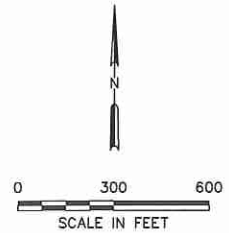
$$C_p = 0.64$$

O:\1339\151\EXPANSION 2009\PART III-SDP\III-E-16-EXISTING PERMITTED.dwg, jwilson, 1:2



LEGEND

- PERMIT BOUNDARY
- AUTHORIZED LIMIT OF WASTE
- STATE PLANE COORDINATE SYSTEM
- GEODETIC COORDINATE SYSTEM
- 600 PERMITTED FINAL COVER CONTOUR
- 500 EXISTING CONTOUR (SEE NOTE 1)
- PERMITTED DRAINAGE SWALE
- PERMITTED LETDOWN STRUCTURE
- USACE SECTION 404 JURISDICTIONAL WATERS OF THE U.S. (SEE NOTE 3)
- USACE JURISDICTIONAL WETLANDS
- DRAINAGE AREA BOUNDARY
- S3 DRAINAGE AREA DESIGNATION



- NOTE:**
1. CONTOURS AND ELEVATIONS PROVIDED BY METROPOLITAN AERIAL SURVEYS COMPILED FROM AERIAL PHOTOGRAPHY FLOWN 8-28-2010. THE GRID SYSTEM IS TIED TO THE TEXAS STATE PLANE COORDINATE SYSTEM NORTH CENTRAL ZONE NAD 1983. ELEVATIONS ARE BASED ON NAVD 1988.
 2. PERMIT BOUNDARY WAS PREPARED BY PEISER SUREYING CO. IN NOVEMBER 2010.
 3. SECTION 404 JURISDICTIONAL WATERS OF THE U.S. AND WETLANDS REPRODUCED FROM THE GOSHAWK ENVIRONMENTAL CONSULTANTS, INC. SEPTEMBER 2010 REPORT WHICH IS INCLUDED IN PARTS I/II, APPENDIX I/II.B.
 4. REFER TO DRAWING IIIIF-E-17 FOR OFFSITE DRAINAGE AREAS.

DRAINAGE AREA NO.	AREA (ACRES)	DRAINAGE AREA NO.	AREA (ACRES)	DRAINAGE AREA NO.	AREA (ACRES)
S1	10.40	N7AS	4.36	N18	4.12
S2	31.53	N7BT	5.45	N19	1.82
S3	20.21	N7BS	3.34	N20	2.62
S4	57.41	N8T	16.52	CH2	1.56
S5	0.67	NBS	10.27	CH3	2.39
N1	11.26	N9T	11.35	CH4	3.11
N2T	9.05	N9S	9.50	CH4A	0.68
N2S	3.16	N10T	11.93	CH5	3.26
N3T	34.01	N10S	7.39	CH6	2.95
N3S	3.47	N11T	3.03	CH7A	2.30
N4T	7.45	N11S	4.40	CH7B	3.66
N4S	5.05	N12	7.96	CH9	3.48
N5T	20.18	N13	18.73	CH10	8.41
N5S	4.50	N14	26.06	CH11	2.97
N6T	5.48	N15	19.93	CHW1	0.89
N6S	4.10	N16	2.72	W1	8.30
N7AT	12.08	N17	4.32	W2	9.83
TOTAL OF ALL DRAINAGE AREAS LISTED = 469.62 ACRES					



<input type="checkbox"/> DRAFT <input checked="" type="checkbox"/> FOR PERMITTING PURPOSES ONLY <input type="checkbox"/> ISSUED FOR CONSTRUCTION <input type="checkbox"/> CLIENT APPROVAL BY:	
DATE: 02/2012 FILE: 1339-351-11 CAD: IIIIF-E-16-DRAINAGE PLAN.DWG	DRAWN BY: SRF DESIGN BY: CRM REVIEWED BY: JPY
REUSE OF DOCUMENTS <small>THIS DOCUMENT, AND THE DESIGNS INCORPORATED HEREIN, AS AN INSTRUMENT OF PROFESSIONAL SERVICE, IS THE PROPERTY OF WEAVER BOOS CONSULTANTS, LLC - SOUTHWEST AND IS NOT TO BE USED IN WHOLE OR IN PART, WITHOUT THE WRITTEN AUTHORIZATION OF WEAVER BOOS CONSULTANTS, LLC - SOUTHWEST.</small>	

PREPARED FOR CITY OF FARMERS BRANCH		
REVISIONS		
NO.	DATE	DESCRIPTION

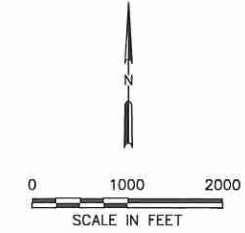
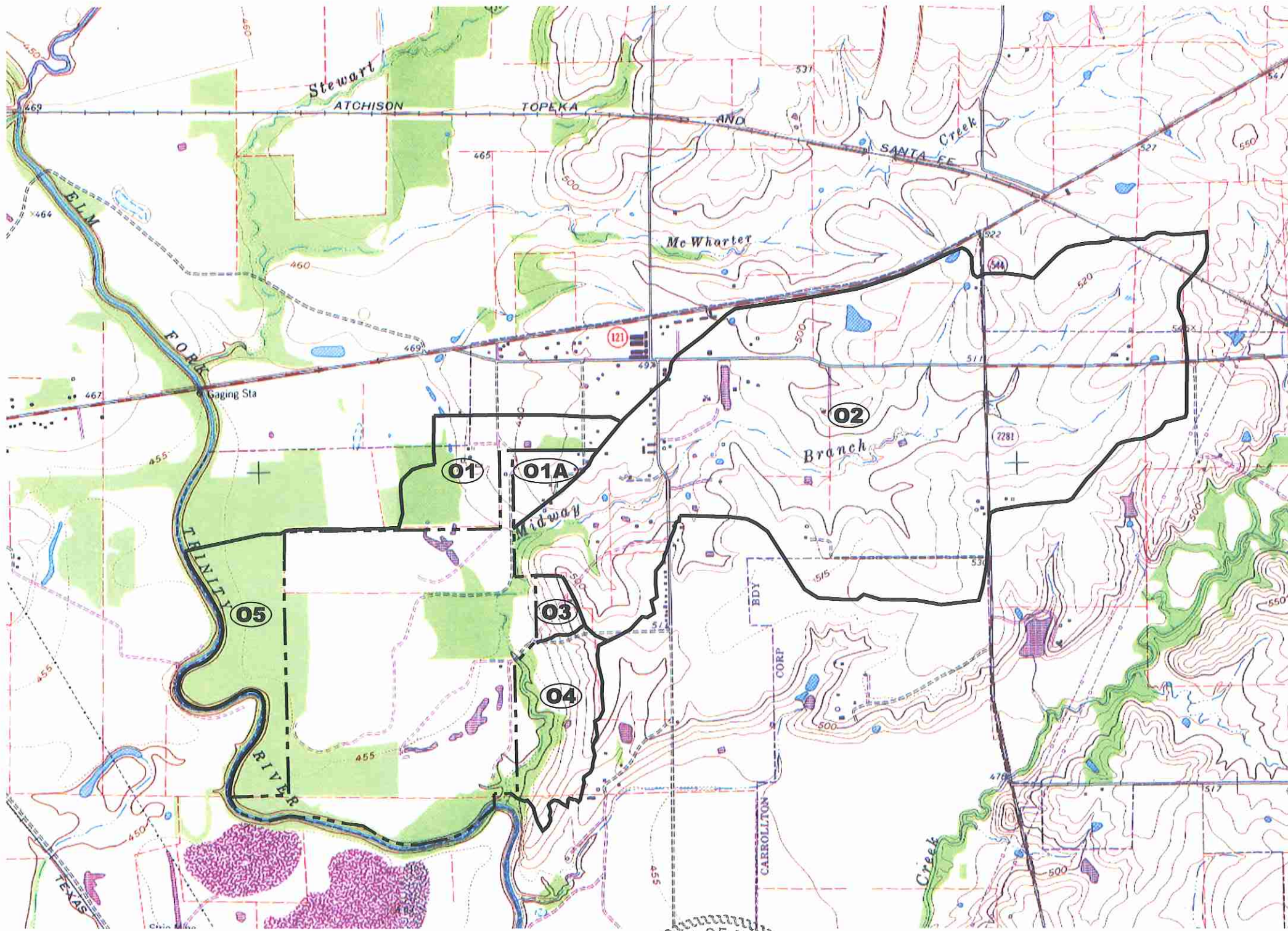
**MAJOR PERMIT AMENDMENT
UPDATED PERMITTED CONDITION
DRAINAGE AREA PLAN
CAMELOT LANDFILL
DENTON COUNTY, TEXAS**

Weaver Boos Consultants
 TBPE REGISTRATION NO. F-3727

CHICAGO, IL	FORT WORTH, TX	GRIFFITH, IN
NAPERVILLE, IL	SOUTH BEND, IN	SOUTH BEND, IN
COLUMBUS, OH	SPRINGFIELD, IL	SPRINGFIELD, IL
DENVER, CO	ST. LOUIS, MO	ST. LOUIS, MO

SHEET IIIIF-E-16

O:\1339\351\EXPANSION 2009\PART III-SUP\IIF-E-17 OFFSITE DRAINAGE.dwg, jwilson, 1:2



LEGEND

--- PERMIT BOUNDARY

— DRAINAGE AREA BOUNDARY

02 DRAINAGE AREA LABEL

DRAINAGE AREA NO.	AREA (ACRES)
01	87.5
01A	23.4
02	1,008.4
03	16.2
04	86.0
05	116.5
PB	462.6
TOTAL	1,807.6

ROAD CLASSIFICATION

Heavy-duty ——— Light-duty ———

Medium-duty ——— Unimproved dirt ———

○ Interstate Route ○ U.S. Route ○ State Route

LEWISVILLE EAST, TEX.
 SW/4 FRISCO 15' QUADRANGLE
 N3300-W9652.5/7.5
 1960
 PHOTOREVISED 1968
 AMS 6650 III SW-SERIES V882

- NOTES:**
1. DRAINAGE AREA DELINEATION WITHIN THE PERMIT BOUNDARY IS SHOWN ON DRAWING IIF-E-16.
 2. TOPOGRAPHY REPRODUCED FROM USGS 7.5 MINUTE QUADRANGLE TOPOGRAPHIC MAP (LEWISVILLE EAST, TX, PHOTO REVISED 1981).

NEVZAT TURAN
 84059
 LICENSED PROFESSIONAL ENGINEER
 2-28-12

<input type="checkbox"/> DRAFT <input checked="" type="checkbox"/> FOR PERMITTING PURPOSES ONLY <input type="checkbox"/> ISSUED FOR CONSTRUCTION <input type="checkbox"/> CLIENT APPROVAL BY:	PREPARED FOR CITY OF FARMERS BRANCH	MAJOR PERMIT AMENDMENT UPDATED PERMITTED OFFSITE DRAINAGE AREAS CAMELOT LANDFILL DENTON COUNTY, TEXAS <i>Weaver Boos Consultants</i> TBPE REGISTRATION NO. F-3727															
DATE: 02/2012 FILE: 1339-351-11 CAD: IIF-E-17 OFFSITE DRAINAGE.DWG	DRAWN BY: SRF DESIGN BY: CRM REVIEWED BY: JPY	<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th colspan="3">REVISIONS</th> </tr> <tr> <th>NO.</th> <th>DATE</th> <th>DESCRIPTION</th> </tr> </thead> <tbody> <tr> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> </tr> </tbody> </table>	REVISIONS			NO.	DATE	DESCRIPTION									
REVISIONS																	
NO.	DATE	DESCRIPTION															
REUSE OF DOCUMENTS THIS DOCUMENT, AND THE DESIGNS INCORPORATED HEREIN, AS AN INSTRUMENT OF PROFESSIONAL SERVICE, IS THE PROPERTY OF WEAVER BOOS CONSULTANTS, LLC - SOUTHWEST AND IS NOT TO BE USED IN WHOLE OR IN PART, WITHOUT THE WRITTEN AUTHORIZATION OF WEAVER BOOS CONSULTANTS, LLC - SOUTHWEST.																	
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compute the value of Snyder's peaking coefficient C_p for use in HEC-1 analyses. First, the watershed lag time T_L is determined by subtracting one-half of the computation interval from the time to rise ($T_L = T_r - \Delta t/2$). Then, C_p may be computed by substituting the known values of T_L and q_p into Snyder's equation for peak unit hydrograph flow rate and solving for C_p .

$$C_p = \frac{q_p \times T_L}{640} \tag{6.30}$$

In another study, Espey [1977] derived the following equation for computing the time from the beginning of surface runoff to the unit hydrograph peak:

$$T_r = 3.10 L^{0.23} S^{-0.25} I^{-0.18} \Phi^{1.57} \tag{6.31}$$

Espey "10-Minute" Method for Estimating Snyder Parameters

in which:

T_r = time from beginning of surface runoff to unit hydrograph peak (minutes)

L = total distance along main channel from study point to watershed boundary (feet)

S = main channel slope between the reference point and a point 0.2L downstream from the upstream watershed boundary (feet per foot)

I = impervious cover within the watershed (percent)

Φ = description of conveyance efficiency of the watershed drainage system.

The conveyance efficiency coefficient Φ is determined using the relationships illustrated on Figure 6.12.

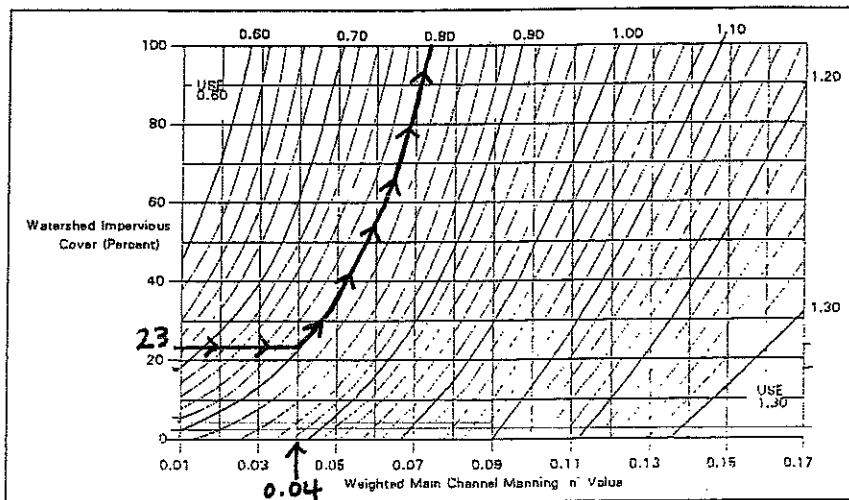


FIGURE 6.12 Determination of Conveyance Efficiency Coefficient Φ

This equation was derived from records for 41 watersheds in Texas, Tennessee, Mississippi, Pennsylvania, North Carolina, Colorado, Kentucky, and Indiana. The range in the watershed characteristics used to develop the equations for urban areas were:

Area : From 0.0128 square miles to 15.00 square miles

L : From 555 feet to 35,600 feet

S : From 0.0005 ft. per ft. to 0.0295 ft. per ft.

I : From 2% to 100%

Φ : From 0.60 to 1.30

Again, note that the time to rise T_r is not the same as the watershed lag time T_L . The difference between the two is that T_r is defined as the time from the beginning of effective rainfall to the peak of the unit hydrograph, while T_L is the time from the centroid of the effective rainfall to the peak of the unit hydrograph. For the purposes of HEC-1 analyses, however, T_L may be determined simply by subtracting one-half the computation time interval from the computed value of T_r ($T_r - \Delta t/2$).

The relationship developed by Espey to compute the peak flow rate of the unit hydrograph is as follows:

$$6.32 \quad Q_u = 31600 A^{0.96} T_r^{-1.07}$$

in which:

Q_u = unit hydrograph peak discharge (cfs)

A = drainage area (square miles)

T_r = time of rise from beginning of surface runoff to unit hydrograph peak (minutes)

Riverside County Method for Estimating Snyder Parameters

Three watershed lag equations have been derived for use in rural areas of Riverside County, California by the Riverside County Flood Control and Water Conservation District [Anonymous, 1963]. These equations differ slightly from those developed at the Tulsa District of the U.S. Army Corps of Engineers in that lag is defined as the time from the beginning of rainfall to the point on the unit hydrograph corresponding to one-half of the total runoff volume.

Each equation is applicable to a different topographic region:

$$6.33 \quad T_L = 120 \left(\frac{L \times L_{ca}}{\sqrt{S}} \right)^{0.38} \quad \text{(Mountain Areas)}$$

$$6.34 \quad T_L = 0.72 \left(\frac{L \times L_{ca}}{\sqrt{S}} \right)^{0.38} \quad \text{(Foothill Areas)}$$

$$6.35 \quad T_L = 0.38 \left(\frac{L \times L_{ca}}{\sqrt{S}} \right)^{0.38} \quad \text{(Valley Areas)}$$

in which:

T_L = watershed lag in hours

L = watershed length in miles

L_{ca} = length to centroid in miles

S = watershed slope in feet per mile.

The sizes of the watersheds studied in developing these equations ranged from 2.3 square miles to 645 square miles.

**HEC-1 OUTPUT – UPDATED PERMITTED
25-YEAR, 24-HOUR STORM EVENT**


```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*   JUN 1998
*   VERSION 4.1
*
* RUN DATE 13JUN11 TIME 13:37:12
*
*****

```

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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

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X X XXXXXXX XXXXX X
X X X X X XX
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XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
*DIAGRAM
1         ID          CAMELOT LANDFILL
2         ID          MAJOR PERMIT AMENDMENT APPLICATION
3         ID          UPDATED PERMITTED CONDITION
4         ID          25-YEAR, 24-HOUR STORM EVENT
5         IT          5          0          2400          416          0          0
6         IO          3          0          0
*         *          NORTHEAST AREA
7         KK          01
8         KM          OFFSITE AREA 01
9         KO          0          0          0          7          21
10        BA          .1367
11        PH          4          .74          1.57          3.19          4.18          4.52          5.47          6.43          7.44
12        LS          .87
13        US          .39          .64
*         *
14        KK          01A
15        KM          OFFSITE AREA 01A
16        KO          0          0          0          7          21
17        BA          .0366
18        LS          .85
19        US          .50          .68
*         *
20        KK          02
21        KM          OFFSITE AREA 02
22        KO          0          0          0          7          21
23        BA          1.5756
24        LS          .85
25        US          .71          .58
*         *
26        KK          S4
27        KM          RUNOFF AREA S4
28        KO          0          0          0          7          21
29        BA          .0897
30        LS          .84
31        US          .94          .65
*         *
32        KK          CS4
33        KM          COMBINE AREAS PRIOR TO POND P1 OUTLET
34        KO          0          0          0          7          21
35        HC          3
*         *
36        KK          N1
37        KM          RUNOFF AREA N1
38        KO          0          0          0          7          21
39        BA          .0176
40        LS          .84
41        US          .38          .70
*         *

```

LINE	ID	1	2	3	4	5	6	7	8	9	10
42	KK	O3									
43	KM	OFFSITE AREA O3									
44	KO	0	0	0	7	21					
45	BA	.0253									
46	LS		84								
47	US	.30	.68								
	*										
48	KK	C1MWT									
49	KM	COMBINE AREAS N1, O1, O2, O3, AND S4									
50	KO	0	0	0	7	21					
51	HC	3									
	*										
52	KK	S3									
53	KM	RUNOFF AREA S3									
54	KO	0	0	0	7	21					
55	BA	.0316									
56	LS		84								
57	US	.82	.68								
	*										
58	KK	N20									
59	KM	RUNOFF AREA N20									
60	KO	0	0	0	7	21					
61	BA	.0041									
62	LS		84								
63	UK	31.95	.188	.35	100						
64	RD	1832.1	.0018	.03			TRAP	6	3	YES	
	*										
65	KK	C2MWT									
66	KM	COMBINE AREAS O1, O2, O3, N1, S4, S3, AND N20									
67	KO	0	0	0	7	21					
68	HC	2									
	*										
	*	NORTH CENTRAL AREA OF LANDFILL TO POND 1 (UPPER POND)									
	*										
69	KK	N11T									
70	KM	RUNOFF AREA N11T									
71	KO	0	0	0	7	21					
72	BA	.0047									
73	LS		84								
74	UK	415.07	.02	.35	100						
75	RD	427.05	.003	.03			TRAP	0	4	NO	
	*										
76	KK	N11S									
77	KM	RUNOFF AREA N11S									
78	KO	0	0	0	7	21					
79	BA	.0069									
80	LS		86								
81	UK	73.21	.20	.35	100						

LINE	ID	1	2	3	4	5	6	7	8	9	10
82	RD	733.86	.007	.03			TRAP	0	4	NO	
	*										
83	KK	CN11									
84	KM	COMBINE N11 AREAS									
85	KO	0	0	0	7	21					
86	HC	2									
	*										
87	KK	CH11									
88	KM	RUNOFF AREA CH11									
89	KO	0	0	0	7	21					
90	BA	.0046									
91	LS		84								
92	UK	84.04	.33	.35	100						
93	RD	1487	.001	.03			TRAP	10	3	YES	
	*										
94	KK	N2T									
95	KM	RUNOFF AREA N2T									
96	KO	0	0	0	7	21					
97	BA	.0141									
98	LS		84								
99	UK	553.17	.02	.35	100						
100	RD	644.44	.003	.03			TRAP	0	4	NO	
	*										
101	KK	N2S									
102	KM	RUNOFF AREA N2S									
103	KO	0	0	0	7	21					

104	BA	.0049								
105	LS		86							
106	UK	80.24	.20	.35	100					
107	RD	379.06	.01	.03		TRAP	0	4	NO	
	*									
108	KK	CN2								
109	KM	COMBINE N2 AREAS								
110	KO	0	0	0	7	21				
111	HC	2								
	*									
112	KK	CCH2								
113	KM	COMBINE AREAS UPSTREAM OF CH2								
114	KO	0	0	0	7	21				
115	HC	2								
	*									
116	KK	CH2								
117	KM	RUNOFF AREA CH2								
118	KO	0	0	0	7	21				
119	BA	.0024								
120	LS		84							
121	UK	102.63	.18	.35	100					
122	RD	576.18	.001	.03		TRAP	10	3	YES	
	*									

1

HEC-1 INPUT

PAGE 4

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

123	KK	N12								
124	KM	RUNOFF AREA N12								
125	KO	0	0	0	7	21				
126	BA	.0124								
127	LS		84							
128	US	.38	.71							
	*									
129	KK	N3T								
130	KM	RUNOFF AREA N3T								
131	KO	0	0	0	7	21				
132	BA	.0531								
133	LS		84							
134	UK	512.17	.02	.35	100					
135	RD	691.59	.003	.03		TRAP	0	4	NO	
	*									
136	KK	N3S								
137	KM	RUNOFF AREA N3S								
138	KO	0	0	0	7	21				
139	BA	.0054								
140	LS		86							
141	UK	89.87	.20	.35	100					
142	RD	581.49	.003	.03		TRAP	0	4	NO	
	*									
143	KK	CN3								
144	KM	COMBINE N3S, N3T, N12								
145	KO	0	0	0	7	21				
146	HC	3								
	*									
147	KK	CCH3								
148	KM	COMBINE AREAS N11, N2, N12, N3 AT CH3								
149	KO	0	0	0	7	21				
150	HC	2								
	*									
151	KK	CH3								
152	KM	RUNOFF AREA CH3								
153	KO	0	0	0	7	21				
154	BA	.0037								
155	LS		84							
156	UK	152.72	.275	.35	100					
157	RD	697.69	.001	.03		TRAP	20	3	YES	
	*									
158	KK	N4T								
159	KM	RUNOFF AREA N4T								
160	KO	0	0	0	7	21				
161	BA	.0116								
162	LS		84							
163	UK	746.35	.02	.35	100					
164	RD	608.13	.01	.03		TRAP	0	4	NO	
	*									

1

HEC-1 INPUT

PAGE 5

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

165	KK	N4S								
166	KM	RUNOFF AREA N4S								

167	KO	0	0	0	7	21							
168	BA	.0079											
169	LS		86										
170	UK	77.51	.20	.35	100								
171	RD	640.53	.003	.03			TRAP	0	4	NO			
	*												
172	KK	CN4											
173	KM	COMBINE N4 AREAS											
174	KO	0	0	0	7	21							
175	HC	2											
	*												
176	KK	CH4											
177	KM	RUNOFF AREA CH4											
178	KO	0	0	0	7	21							
179	BA	.0049											
180	LS		84										
181	UK	100.82	.198	.35	100								
182	RD	1278.5	.005	.03			TRAP	10	4	YES			
	*												
183	KK	CLCH4A											
184	KM	COMBINE AREAS N11, N2, N3, N4 AT CHANNEL CH4A											
185	KO	0	0	0	7	21							
186	HC	2											
	*												
187	KK	CH4A											
188	KM	RUNOFF AREA CH4A											
189	KO	0	0	0	7	21							
190	BA	.0011											
191	LS		84										
192	UK	40.38	.33	.35	100								
193	RD	519.75	.0035	.03			TRAP	20	3	YES			
	*												
194	KK	N13											
195	KM	RUNOFF AREA N13											
196	KO	0	0	0	7	21							
197	BA	.0293											
198	LS		84										
199	US	.53	.69										
	*												
200	KK	W1											
201	KM	RUNOFF AREA W1 (POND 1)											
202	KO	0	0	0	7	21							
203	BA	.0130											
204	LS		100										
205	UD	0											
	*												

1

HEC-1 INPUT

PAGE 6

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

206	KK	PNDLIN											
207	KM	COMBINE ALL FLOWS INTO POND 1											
208	KO	0	0	0	7	21							
209	HC	3											
	*												
210	KK	PNDIOUT											
211	KM	ROUTE THROUGH UPPER DET. POND (POND 1) 3-42" AT 451											
212	KO	0	0	0	7	21							
213	RS	1	ELEV	455.2									
214	SA	0	7.7727	7.9131	8.0441	8.1759							
215	SE	455.2	455.5	456	456.5	457							
216	SS	456	25	2.6	1.5								
217	SL	452.77	19.6350	.8	.5								
	*												
218	KK	N16											
219	KM	RUNOFF AREA N16											
220	KO	0	0	0	7	21							
221	BA	.0042											
222	LS		84										
223	US	.24	.71										
	*												
224	KK	CHW1											
225	KM	RUNOFF AREA CHW1											
226	KO	0	0	0	7	21							
227	BA	.0014											
228	LS		84										
229	UK	41.87	.33	.35	100								
230	RD	551.13	.001	.03			TRAP	20	3	YES			
	*												
231	KK	MIDRD											
232	KM	COMBINE ALL FLOWS U/S OF ENTRANCE ROAD											
233	KO	0	0	0	7	21							

234 HC 3
*
235 KK S5
236 KM RUNOFF AREA S5
237 KO 0 0 0 7 21
238 BA .0010
239 LS 84
240 US .23 .75
*
241 KK CS5
242 KM COMBINE ALL FLOWS U/S OF ENTRANCE ROAD WITH S5
243 KO 0 0 0 7 21
244 HC 2
*

1

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PAGE 7

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

245 KK O4
246 KM OFFSITE AREA O4
247 KO 0 0 0 7 21
248 BA .1344
249 LS 84
250 US .43 .64
*
251 KK C4MWY
252 KM COMBINE ALL FLOWS UPSTREAM OF N10
253 KO 0 0 0 7 21
254 HC 2
* EAST AND SOUTHSIDE TO MIDWAY BRANCH
255 KK N10T
256 KM RUNOFF AREA N10T
257 KO 0 0 0 7 21
258 BA .0186
259 LS 84
260 UK 733.01 .02 .35 100
261 RK 618.87 .002 .03 TRAP 0 4 NO
*

262 KK N10S
263 KM RUNOFF AREA N10S
264 KO 0 0 0 7 21
265 BA .0115
266 LS 86
267 UK 99.77 .20 .35 100
268 RK 717.21 .013 .03 TRAP 0 4 NO
*

269 KK CN10
270 KM COMBINE N10 AREAS
271 KO 0 0 0 7 21
272 HC 2
*

273 KK CH10
274 KM RUNOFF AREA CH10
275 KO 0 0 0 7 21
276 BA .0131
277 LS 84
278 UK 88.40 .015 .35 100
279 RD 1453.8 .011 .03 TRAP 10 3 YES
*

280 KK CABELM
281 KM COMBINE AREAS UPSTREAM OF ELM FORK
282 KO 0 0 0 7 21
283 HC 2
* SOUTHEAST CORNER INTO POND 2

1

HEC-1 INPUT

PAGE 8

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

284 KK N9T
285 KM RUNOFF AREA N9T
286 KO 0 0 0 7 21
287 BA .0177
288 LS 84
289 UK 566.18 .02 .35 100
290 RK 696.09 .003 .03 TRAP 0 4 NO
*

291 KK N9S
292 KM RUNOFF AREA N9S
293 KO 0 0 0 7 21
294 BA .0148
295 LS 86
296 UK 83.55 .2 .35 100

297	RK	791.65	.014	.03		TRAP	0	4	NO
	*								
298	KK	CN9							
299	KM	COMBINE N9 AREAS							
300	KO	0	0	0	7	21			
301	HC	2							
	*								
302	KK	CH9							
303	KM	RUNOFF AREA CH9							
304	KO	0	0	0	7	21			
305	BA	.0054							
306	LS	84							
307	UK	84.85	.157	.35	100				
308	RD	1689.3	.001	.03		TRAP	10	3	YES
	*	NORTHWEST CORNER TO POND 2							
309	KK	N5T							
310	KM	RUNOFF AREA N5T							
311	KO	0	0	0	7	21			
312	BA	.0315							
313	LS	84							
314	UK	1133.6	.02	.35	100				
315	RK	154.15	.002	.03		TRAP	0	4	NO
	*								
316	KK	N5S							
317	KM	RUNOFF AREA N5S							
318	KO	0	0	0	7	21			
319	BA	.007							
320	LS	86							
321	UK	126.10	.140	.35	100				
322	RK	628.8	.01	.03		TRAP	0	4	NO
	*								

1

HEC-1 INPUT

PAGE 9

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

323	KK	CN5							
324	KM	COMBINE N5 AREAS							
325	KO	0	0	0	7	21			
326	HC	2							
	*								
327	KK	CH5							
328	KM	RUNOFF AREA CH5							
329	KO	0	0	0	7	21			
330	BA	.0051							
331	LS	84							
332	UK	100.8	.198	.35	100				
333	RD	1358.6	.001	.03		TRAP	10	3	YES
	*								
334	KK	N6T							
335	KM	RUNOFF AREA N6T							
336	KO	0	0	0	7	21			
337	BA	.0086							
338	LS	84							
339	UK	476.08	.02	.35	100				
340	RK	652.91	.005	.03		TRAP	0	4	NO
	*								
341	KK	N6S							
342	KM	RUNOFF AREA N6S							
343	KO	0	0	0	7	21			
344	BA	.0064							
345	LS	86							
346	UK	85.77	.20	.35	100				
347	RK	641.29	.005	.03		TRAP	0	4	NO
	*								
348	KK	CN6							
349	KM	COMBINE N6 AREAS							
350	KO	0	0	0	7	21			
351	HC	2							
	*								
352	KK	CCH6							
353	KM	COMBINE AREAS N5 AND N6 AT CH6							
354	KO	0	0	0	7	21			
355	HC	2							
	*								
356	KK	CH6							
357	KM	RUNOFF AREA CH6							
358	KO	0	0	0	7	21			
359	BA	.0046							
360	LS	84							
361	UK	101.19	.17	.35	100				
362	RD	1371.2	.001	.03		TRAP	20	3	YES
	*								

LINE	ID	1	2	3	4	5	6	7	8	9	10
363	KK	N7AT									
364	KM	RUNOFF AREA N7AT									
365	KO	0	0	0	7	21					
366	BA	.0189									
367	LS		84								
368	UK	582.87	.02	.35	100						
369	RK	408.17	.003	.03		TRAP	0	4	NO		
	*										
370	KK	N7AS									
371	KM	RUNOFF AREA N7AS									
372	KO	0	0	0	7	21					
373	BA	.0068									
374	LS		86								
375	UK	91.73	.20	.35	100						
376	RK	467.36	.011	.03		TRAP	0	4	NO		
	*										
377	KK	CN7A									
378	KM	COMBINE N7A AREAS									
379	KO	0	0	0	7	21					
380	HC	2									
	*										
381	KK	CCH7A									
382	KM	COMBINE AREAS N5, N6, N7A AT CH7A									
383	KO	0	0	0	7	21					
384	HC	2									
	*										
385	KK	CH7A									
386	KM	RUNOFF AREA CH7A									
387	KO	0	0	0	7	21					
388	BA	.0036									
389	LS		84								
390	UK	78.31	.203	.35	100						
391	RD	885.29	.001	.03		TRAP	40	3	YES		
	*										
392	KK	N7BT									
393	KM	RUNOFF AREA N7BT									
394	KO	0	0	0	7	21					
395	BA	.0085									
396	LS		84								
397	UK	562.87	.02	.35	100						
398	RK	410.19	.003	.03		TRAP	0	4	NO		
	*										
399	KK	N7BS									
400	KM	RUNOFF AREA N7BS									
401	KO	0	0	0	7	21					
402	BA	.0052									
403	LS		86								
404	UK	86.46	.20	.35	100						

LINE	ID	1	2	3	4	5	6	7	8	9	10
405	RK	405.33	.014	.03		TRAP	0	4	NO		
	*										
406	KK	CN7B									
407	KM	COMBINE N7B AREAS									
408	KO	0	0	0	7	21					
409	HC	2									
	*										
410	KK	CCH7B									
411	KM	COMBINE AREAS N5, N6, N7A, N7B AT CH7B									
412	KO	0	0	0	7	21					
413	HC	2									
	*										
414	KK	CH7B									
415	KM	RUNOFF AREA CH7A									
416	KO	0	0	0	7	21					
417	BA	.0057									
418	LS		84								
419	UK	109.04	.177	.35	100						
420	RD	1127	.001	.03		TRAP	40	3	YES		
	*										
421	KK	N8T									
422	KM	RUNOFF AREA N8T									
423	KO	0	0	0	7	21					
424	BA	.0258									
425	LS		84								
426	UK	551.92	.02	.35	100						

427	RK	667.70	.003	.03		TRAP	0	4	NO
	*								
428	KK	N8S							
429	KM	RUNOFF AREA N8S							
430	KO	0	0	0	7	21			
431	BA	.0160							
432	LS		86						
433	UK	91.71	.20	.35	100				
434	RK	924.50	.018	.03		TRAP	0	4	NO
	*								
435	KK	CN8							
436	KM	COMBINE N8 AREAS							
437	KO	0	0	0	7	21			
438	HC	2							
	*								
439	KK	C2W2							
440	KM	COMBINE AREAS N5-N9 INTO POND 2							
441	KO	0	0	0	7	21			
442	HC	3							
	*								

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PAGE 12

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

443	KK	W2																	
444	KM	RUNOFF WITHIN POND 2																	
445	KO	0	0	0	7	21													
446	BA	.0154																	
447	LS		100																
448	UD	0																	
	*																		
449	KK	PND2IN																	
450	KM	COMBINE AREAS INTO POND 2																	
451	KO	0	0	0	7	21													
452	HC	2																	
	*																		
453	KK	PD2OUT																	
454	KM	ROUTE THROUGH POND W2																	
455	KO	0	0	0	7	21													
456	RS	1	ELEV	454															
457	SA	0	4.4466	6.7860	8.2567	8.3782	8.5005	8.6236	8.8721	9.1240									
458	SE	454	454.5	455	455.5	456	456.5	457	458	459									
459	SS	458	25	2.6	1.5														
460	SL	456	28.2743	.8	.5														
	*																		
461	KK	N14																	
462	KM	RUNOFF AREA N14																	
463	KO	0	0	0	7	21													
464	BA	.0407																	
465	LS		84																
466	US	.38	.67																
	*																		
467	KK	N15																	
468	KM	RUNOFF AREA N15																	
469	KO	0	0	0	7	21													
470	BA	.0311																	
471	LS		84																
472	US	.47	.68																
	*																		
473	KK	C1N14																	
474	KM	COMBINE AREAS N14, N15 & POND 2																	
475	KO	0	0	0	7	21													
476	HC	3																	
	*																		
477	KK	S2																	
478	KM	RUNOFF AREA S2																	
479	KO	0	0	0	7	21													
480	BA	.0493																	
481	LS		84																
482	US	.73	.67																
	*																		

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PAGE 13

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

483	KK	N19																	
484	KM	RUNOFF AREA N19																	
485	KO	0	0	0	7	21													
486	BA	.0028																	
487	LS		84																
488	UK	43.65	.33	.35	100														
489	RD	1305	.0016	.03		TRAP	10	3	YES										


```

*
490      KK      N18
491      KM      RUNOFF AREA N18
492      KO      0      0      0      7      21
493      BA      .0064
494      LS      84
495      UK      41.18      .33      .35      100
496      RD      1123.4      .0016      .03      TRAP      15      3      YES
*

497      KK      05
498      KM      OFFSITE AREA 05
499      KO      0      0      0      7      21
500      BA      .1820
501      LS      84
502      US      .59      .64
*

503      KK      S1
504      KM      RUNOFF AREA S1
505      KO      0      0      0      7      21
506      BA      .0163
507      LS      84
508      US      .75      .70
*

509      KK      N17
510      KM      RUNOFF AREA N17
511      KO      0      0      0      7      21
512      BA      .0068
513      LS      84
514      US      .12      .64
*

515      KK      C107
516      KM      COMBINE AREAS S1, 06, AND N17-19
517      KO      0      0      0      7      21
518      HC      4
*
519      ZZ

```

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT LINE (V) ROUTING (---->) DIVERSION OR PUMP FLOW
NO. (.) CONNECTOR (<----) RETURN OF DIVERTED OR PUMPED FLOW

7      O1
.
.
14     .      O1A
.
.
20     .      .      O2
.
.
26     .      .      .      S4
.
.
32     .      .      .      .
.      CS4.....
.
.
36     .      .      .      N1
.
.
42     .      .      .      .      O3
.
.
48     .      .      .      .
.      C1MWY.....
.
.
52     .      .      .      S3
.      .      .      V
.      .      .      V
58     .      .      .      N20 ***
.
.
65     .      .      .      .
.      C2MWY.....
.
.
69     .      .      .      N11T
.
.
76     .      .      .      .      N11S
.
.
83     .      .      .      .      .
.      .      .      CN11.....
.      .      .      V
.      .      .      V
87     .      .      .      CH11 ***
.
.

```

```

94      .      .      .      .      N2T
      .      .      .      .      .
101     .      .      .      .      .      N2S
      .      .      .      .      .      .
108     .      .      .      .      CN2.....
      .      .      .      .      .
112     .      .      .      .      CCH2.....
      .      .      .      .      V
116     .      .      .      .      V
      .      .      .      .      CH2 ***
      .      .      .      .      .
123     .      .      .      .      N12
      .      .      .      .      .
129     .      .      .      .      .      N3T
      .      .      .      .      .      .
136     .      .      .      .      .      .      N3S
      .      .      .      .      .      .      .
143     .      .      .      .      CN3.....
      .      .      .      .      .
147     .      .      .      .      CCH3.....
      .      .      .      .      V
151     .      .      .      .      V
      .      .      .      .      CH3 ***
      .      .      .      .      .
158     .      .      .      .      N4T
      .      .      .      .      .
165     .      .      .      .      .      N4S
      .      .      .      .      .      .
172     .      .      .      .      .      CN4.....
      .      .      .      .      V
176     .      .      .      .      V
      .      .      .      .      CH4 ***
      .      .      .      .      .
183     .      .      .      .      C1CH4A.....
      .      .      .      .      V
187     .      .      .      .      V
      .      .      .      .      CH4A ***
      .      .      .      .      .
194     .      .      .      .      N13
      .      .      .      .      .
200     .      .      .      .      .      W1
      .      .      .      .      .
206     .      .      .      .      PND1IN.....
      .      .      .      .      V
210     .      .      .      .      V
      .      .      .      .      PND1OU
      .      .      .      .      .
218     .      .      .      .      N16
      .      .      .      .      V
224     .      .      .      .      V
      .      .      .      .      CHW1 ***
      .      .      .      .      .
231     .      .      .      .      MIDRD.....
      .      .      .      .      .
235     .      .      .      .      S5
      .      .      .      .      .
241     .      .      .      .      CS5.....
      .      .      .      .      .
245     .      .      .      .      O4
      .      .      .      .      .
251     .      .      .      .      C4MWY.....
      .      .      .      .      .
255     .      .      .      .      N10T
      .      .      .      .      .
262     .      .      .      .      .      N10S
      .      .      .      .      .
269     .      .      .      .      CN10.....
      .      .      .      .      V
      .      .      .      .      V

```

```

273 . . . . . CH10 ***
280 . . . . . CABELM.....
284 . . . . . N9T
291 . . . . . N9S
298 . . . . . CN9.....
    . . . . . V
    . . . . . V
302 . . . . . CH9 ***
309 . . . . . N5T
316 . . . . . N5S
323 . . . . . CN5.....
    . . . . . V
    . . . . . V
327 . . . . . CH5 ***
334 . . . . . N6T
341 . . . . . N6S
348 . . . . . CN6.....
352 . . . . . CCH6.....
    . . . . . V
    . . . . . V
356 . . . . . CH6 ***
363 . . . . . N7AT
370 . . . . . N7AS
377 . . . . . CN7A.....
381 . . . . . CCH7A.....
    . . . . . V
    . . . . . V
385 . . . . . CH7A ***
392 . . . . . N7BT
399 . . . . . N7BS
406 . . . . . CN7B.....
410 . . . . . CCH7B.....
    . . . . . V
    . . . . . V
414 . . . . . CH7B ***
421 . . . . . N8T
428 . . . . . N8S
435 . . . . . CN8.....
439 . . . . . C2W2.....
443 . . . . . W2
449 . . . . . FND2IN.....
    . . . . . V
    . . . . . V

```

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453 . . . PD2OUT
. . . .
461 . . . N14
. . . .
467 . . . N15
. . . .
473 . . . C1N14.....
. . . .
477 . . . S2
. . . V
. . . V
483 . . . N19 ***
. . . V
. . . V
490 . . . N18 ***
. . . .
497 . . . O5
. . . .
503 . . . S1
. . . .
509 . . . N17
. . . .
515 . . . C1O7.....

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(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

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1*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 13JUN11 TIME 13:37:12 *
*****

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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

```

CAMELOT LANDFILL
MAJOR PERMIT AMENDMENT APPLICATION
UPDATED PERMITTED CONDITION
25-YEAR, 24-HOUR STORM EVENT

```

6 IO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

```

```

IF HYDROGRAPH TIME DATA
NMIN 5 MINUTES IN COMPUTATION INTERVAL
IDATE 1 0 STARTING DATE
ITIME 0000 STARTING TIME
NQ 416 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 3 0 ENDING DATE
NDTIME 1035 ENDING TIME
ICENT 19 CENTURY MARK

```

COMPUTATION INTERVAL .08 HOURS
TOTAL TIME BASE 34.56 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

*** **

```

*****
* 7 KK *
* O1 *
* *
*****

```

OFFSITE AREA 01

```

9 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL

```

QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

10 BA SUBBASIN CHARACTERISTICS
 TAREA .14 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
 STORM AREA = .14

12 LS SCS LOSS RATE
 STRTL .30 INITIAL ABSTRACTION
 CRVNBR 87.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

13 US SNYDER UNITGRAPH
 TP .39 LAG
 CP .64 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS
 CLARK TC= .45 HR, R= .34 HR
 SNYDER TP= .39 HR, CP= .65

UNIT HYDROGRAPH
 25 END-OF-PERIOD ORDINATES
 13. 46. 89. 127. 144. 135. 110. 86. 67. 53.
 41. 32. 25. 20. 15. 12. 9. 7. 6. 5.
 4. 3. 2. 2. 1.

*** **

HYDROGRAPH AT STATION 01

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.53, TOTAL EXCESS = 5.90

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
 + (CFS) (HR) 6-HR 24-HR 72-HR 34.58-HR
 + 298. 12.42 (CFS) 70. 22. 15. 15.
 (INCHES) 4.730 5.877 5.877 5.877
 (AC-FT) 34. 43. 43. 43.
 CUMULATIVE AREA = .14 SQ MI

*** **

 * *
 14 KK * O1A *
 * *

OFFSITE AREA O1A

16 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

17 BA SUBBASIN CHARACTERISTICS
 TAREA .04 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

.....	HYDRO-35	TP-40	TP-49			
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .04

18 LS SCS LOSS RATE
 STRTL .35 INITIAL ABSTRACTION
 CRVNBR 85.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

19 US SNYDER UNITGRAPH
 TP .50 LAG
 CP .68 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS

CLARK TC= .58 HR, R= .39 HR
 SNYDER TP= .50 HR, CP= .67

UNIT HYDROGRAPH

29 END-OF-PERIOD ORDINATES

2.	8.	15.	23.	29.	32.	32.	28.	22.	18.
15.	12.	9.	8.	6.	5.	4.	3.	3.	2.
2.	1.	1.	1.	1.	1.	0.	0.	0.	

HYDROGRAPH AT STATION O1A

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.77, TOTAL EXCESS = 5.67

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	34.58-HR
+	(CFS)	(HR)	(CFS)			
+	70.	12.58	18.	6.	4.	4.
			(INCHES)	4.570	5.648	5.648
			(AC-FT)	9.	11.	11.

CUMULATIVE AREA = .04 SQ MI

*** **

 * *
 20 KK * O2 *
 * *

OFFSITE AREA O2

22 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

23 BA SUBBASIN CHARACTERISTICS
 TAREA 1.58 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

.....	HYDRO-35	TP-40	TP-49			
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = 1.58

24 LS SCS LOSS RATE
 STRTL .35 INITIAL ABSTRACTION
 CRVNBR 85.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

25 US SNYDER UNITGRAPH
 TP .71 LAG
 CP .58 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS
CLARK TC= .79 HR, R= .76 HR
SNYDER TP= .71 HR, CP= .58

UNIT HYDROGRAPH
54 END-OF-PERIOD ORDINATES

31.	115.	232.	367.	512.	648.	752.	817.	841.	808.
733.	657.	589.	528.	473.	424.	380.	341.	306.	274.
246.	220.	197.	177.	159.	142.	127.	114.	102.	92.
82.	74.	66.	59.	53.	48.	43.	38.	34.	31.
28.	25.	22.	20.	18.	16.	14.	13.	11.	10.
9.	8.	7.	7.						

*** *** *** *** ***

HYDROGRAPH AT STATION O2

TOTAL RAINFALL = 7.42, TOTAL LOSS = 1.77, TOTAL EXCESS = 5.66

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	34.58-HR
2171.	12.75	767.	239.	166.	166.
		(INCHES)	4.524	5.632	5.632
		(AC-FT)	380.	473.	473.

CUMULATIVE AREA = 1.58 SQ MI

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* *
26 KK * S4 *
* *

RUNOFF AREA S4

28 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLST	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

29 BA SUBBASIN CHARACTERISTICS

TAREA	.09	SUBBASIN AREA
-------	-----	---------------

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40					TP-49			
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .09

30 LS SCS LOSS RATE

STRTL	.38	INITIAL ABSTRACTION
CRVNER	84.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

31 US SNYDER UNITGRAPH

TP	.94	LAG
CP	.65	PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS
CLARK TC= 1.04 HR, R= .82 HR
SNYDER TP= .93 HR, CP= .65

UNIT HYDROGRAPH
59 END-OF-PERIOD ORDINATES

1.	4.	8.	13.	18.	24.	29.	34.	37.	40.
41.	41.	39.	35.	32.	29.	26.	24.	21.	19.
17.	16.	14.	13.	12.	10.	9.	8.	8.	7.
6.	6.	5.	5.	4.	4.	3.	3.	3.	2.

2. 2. 2. 2. 1. 1. 1. 1. 1.
 1. 1. 1. 1. 1. 0. 0. 0. 0.

*** *** *** *** ***

HYDROGRAPH AT STATION 54

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
113.	13.00	43.	13.	9.	9.
		(INCHES) 4.456	5.532	5.532	5.532
		(AC-FT) 21.	26.	26.	26.

CUMULATIVE AREA = .09 SQ MI

*** **

 * *
 32 KK * CS4 *
 * *

COMBINE AREAS PRIOR TO POND P1 OUTLET

34 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

35 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

*** *** *** *** ***

HYDROGRAPH AT STATION 54

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
2337.	12.75	828.	258.	179.	179.
		(INCHES) 4.521	5.627	5.627	5.627
		(AC-FT) 410.	511.	511.	511.

CUMULATIVE AREA = 1.70 SQ MI

*** **

 * *
 36 KK * N1 *
 * *

RUNOFF AREA N1

38 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

39 BA SUBBASIN CHARACTERISTICS
 TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .02

40 LS SCS LOSS RATE
 STRL .38 INITIAL ABSTRACTION
 CRVNBR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

41 US SNYDER UNITGRAPH
 TP .38 LAG
 CP .70 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS
 CLARK TC= .46 HR, R= .28 HR
 SNYDER TP= .38 HR, CP= .70

UNIT HYDROGRAPH
 21 END-OF-PERIOD ORDINATES
 2. 7. 13. 18. 21. 19. 15. 11. 8. 6.
 4. 3. 2. 2. 1. 1. 1. 1. 0. 0.
 0.

*** **

HYDROGRAPH AT STATION N1

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
39.	12.42	9.	3.	2.	2.
		(CFS)			
		4.495	5.535	5.535	5.535
		(AC-FT)	4.	5.	5.

CUMULATIVE AREA = .02 SQ MI

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 * *
 42 KK * O3 *
 * *

OFFSITE AREA O3

44 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

45 BA SUBBASIN CHARACTERISTICS
 TAREA .03 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .03

46 LS SCS LOSS RATE
 STRL .38 INITIAL ABSTRACTION
 CRVNBR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

47 US SNYDER UNITGRAPH
 TP .30 LAG
 CP .68 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS
 CLARK TC= .35 HR, R= .23 HR
 SNYDER TP= .30 HR, CP= .68

UNIT HYDROGRAPH
 18 END-OF-PERIOD ORDINATES

5. 17. 30. 36. 32. 23. 16. 11. 8. 5.
 4. 3. 2. 1. 1. 1. 0. 0.

*** *** *** *** ***

HYDROGRAPH AT STATION O3

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
62.	12.33	12.	4.	3.	3.
		(INCHES) 4.500	5.539	5.539	5.539
		(AC-FT) 6.	7.	7.	7.

CUMULATIVE AREA = .03 SQ MI

*** **

 * *
 48 KK * CIMWY *
 * *

COMBINE AREAS N1, O1, O2, O3, AND S4

50 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

51 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

*** *** *** *** ***

HYDROGRAPH AT STATION CIMWY

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
2396.	12.75	848.	264.	183.	183.
		(INCHES) 4.520	5.625	5.625	5.625
		(AC-FT) 421.	523.	523.	523.

CUMULATIVE AREA = 1.74 SQ MI

*** **

 * *
 52 KK * S3 *
 * *

RUNOFF AREA S3

54 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED

TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

55 BA SUBBASIN CHARACTERISTICS
TAREA .03 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
..... HYDRO-35 TP-40 TP-49
5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
.74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .03

56 LS SCS LOSS RATE
STRTL .38 INITIAL ABSTRACTION
CRVNR 84.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

57 US SNYDER UNITGRAPH
TP .82 LAG
CP .68 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS
CLARK TC= .94 HR, R= .65 HR
SNYDER TP= .82 HR, CP= .68

UNIT HYDROGRAPH
48 END-OF-PERIOD ORDINATES

1. 2. 4. 6. 9. 12. 14. 16. 17. 17.
17. 16. 14. 12. 11. 9. 8. 7. 6. 6.
5. 4. 4. 3. 3. 3. 2. 2. 2. 2.
1. 1. 1. 1. 1. 1. 1. 1. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0. 0. 0.

*** **

HYDROGRAPH AT STATION S3

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
(CFS) (HR) 6-HR 24-HR 72-HR 34.58-HR
+ 45. 12.83 (CFS) 15. 5. 3. 3.
(INCHES) 4.472 5.533 5.533 5.533
(AC-FT) 8. 9. 9. 9.

CUMULATIVE AREA = .03 SQ MI

*** **

* *
58 KK * N20 *
* *

RUNOFF AREA N20

60 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLST 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

61 BA SUBBASIN CHARACTERISTICS
TAREA .00 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
..... HYDRO-35 TP-40 TP-49
5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
.74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .00

62 LS SCS LOSS RATE
STRTL .38 INITIAL ABSTRACTION
CRVNBR 84.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

63 UK KINEMATIC WAVE
OVERLAND-FLOW ELEMENT NO. 1
L 32. OVERLAND FLOW LENGTH
S .1880 SLOPE
N .350 ROUGHNESS COEFFICIENT
PA 100.0 PERCENT OF SUBBASIN
DKMIN 5 MINIMUM NUMBER OF DX INTERVALS

64 RD MUSKINGUM-CUNGE
MAIN CHANNEL
L 1832. CHANNEL LENGTH
S .0018 SLOPE
N .030 CHANNEL ROUGHNESS COEFFICIENT
CA .00 CONTRIBUTING AREA
SHAPE TRAP CHANNEL SHAPE
WD 6.00 BOTTOM WIDTH OR DIAMETER
Z 3.00 SIDE SLOPE
RUPSTQ YES ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS
COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	1.85	1.67	.42	6.39	20.57	724.93	5.56	.33
MAIN	.70	1.38	5.00	610.70	46.52	780.00	5.53	2.57

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9325E+01 EXCESS= .1215E+01 OUTFLOW= .1052E+02 BASIN STORAGE= .2178E-02 PERCENT ERROR= .1

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN .70 1.38 5.00 46.52 780.00 5.53

*** *** *** *** ***

HYDROGRAPH AT STATION N20

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

BEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR (CFS)	24-HR	72-HR	34.58-HR
+ 47.	13.00	17.	5.	4.	4.
		(INCHES) 4.468	5.527	5.527	5.527
		(AC-FT) 9.	11.	11.	11.

CUMULATIVE AREA = .04 SQ MI

*** **

* *
65 KK * C2MWY *
* *

COMBINE AREAS O1, O2, O3, N1, S4, S3, AND N20

67 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

68 HC HYDROGRAPH COMBINATION
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** *** *** *** ***

HYDROGRAPH AT STATION C2MWY

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
2437.	12.75	865.	269.	187.	187.
		(INCHES) 4.519	5.623	5.623	5.623
		(AC-FT) 429.	534.	534.	534.

CUMULATIVE AREA = 1.78 SQ MI

*** **

 * *
 69 KK * N11T *
 * *

 RUNOFF AREA N11T

71 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

72 BA SUBBASIN CHARACTERISTICS
 TAREA .00 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .00

73 LS SCS LOSS RATE

STRTL	.38	INITIAL ABSTRACTION
CRVNR	84.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

74 UK KINEMATIC WAVE
 OVERLAND-FLOW ELEMENT NO. 1

L	415.	OVERLAND FLOW LENGTH
S	.0200	SLOPE
N	.350	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

75 RD MUSKINGUM-CUNGE
 MAIN CHANNEL

L	427.	CHANNEL LENGTH
S	.0030	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.00	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	.00	BOTTOM WIDTH OR DIAMETER
Z	4.00	SIDE SLOPE
RUPSTQ	NO	ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS
 COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	.60	1.67	4.05	83.01	12.12	734.95	5.54	.35
MAIN	1.06	1.33	3.26	213.52	11.91	733.23	5.53	2.18

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .1393E+01 OUTFLOW= .1385E+01 BASIN STORAGE= .1876E-02 PERCENT ERROR= .4

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	1.06	1.33	5.00	11.86	735.00	5.53
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HYDROGRAPH AT STATION N11T

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
12.	12.25	2.	1.	0.	0.
		(INCHES) 4.492	5.521	5.528	5.528
		(AC-FT) 1.	1.	1.	1.

CUMULATIVE AREA = .00 SQ MI

*** **

76 KK *****
* N11S *

RUNOFF AREA N11S

78 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLST	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

79 BA SUBBASIN CHARACTERISTICS
TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35				TP-40				TP-49			
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .01

80 LS SCS LOSS RATE

STRTL	.33	INITIAL ABSTRACTION
CRVNR	86.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

81 UK OVERLAND-FLOW ELEMENT NO. 1

L	73.	OVERLAND FLOW LENGTH
S	.2000	SLOPE
N	.350	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

MUSKINGUM-CUNGE

82 RD MAIN CHANNEL

L	734.	CHANNEL LENGTH
S	.0070	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.01	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	.00	BOTTOM WIDTH OR DIAMETER
Z	4.00	SIDE SLOPE
RUPSTQ	NO	ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)				
PLANE1	1.90	1.67	.65	14.64	35.28	724.53	.48
MAIN	1.62	1.33	3.12	366.93	34.59	724.20	3.92

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2130E+01 OUTFLOW= .2077E+01 BASIN STORAGE= .4285E-03 PERCENT ERROR= 2.5

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	1.62	1.33	5.00	32.23	725.00	5.64
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***          ***          ***          ***          ***
          HYDROGRAPH AT STATION      N11S
TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79
PEAK FLOW      TIME                MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)                6-HR      24-HR      72-HR      34.58-HR
+ 32.          12.08                (CFS)
          (INCHES) 4.623            3.        1.        1.        1.
          (AC-FT)  2.              4.623    5.639    5.639    5.639
          CUMULATIVE AREA = .01 SQ MI

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*****
*          *
83 KK      *      CN11 *
*          *
*****
          COMBINE N11 AREAS
85 KO      OUTPUT CONTROL VARIABLES
          IPRNT      3 PRINT CONTROL
          IPLOT      0 PLOT CONTROL
          QSCAL      0. HYDROGRAPH PLOT SCALE
          IPNCH      7 PUNCH COMPUTED HYDROGRAPH
          IOUT       21 SAVE HYDROGRAPH ON THIS UNIT
          ISAV1      1 FIRST ORDINATE PUNCHED OR SAVED
          ISAV2      416 LAST ORDINATE PUNCHED OR SAVED
          TIMINT     .083 TIME INTERVAL IN HOURS

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86 HC      HYDROGRAPH COMBINATION
          ICOMP      2 NUMBER OF HYDROGRAPHS TO COMBINE

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***          ***          ***          ***          ***
          HYDROGRAPH AT STATION      CN11
PEAK FLOW      TIME                MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)                6-HR      24-HR      72-HR      34.58-HR
+ 41.          12.08                (CFS)
          (INCHES) 4.559            6.        2.        1.        1.
          (AC-FT)  3.              4.559    5.589    5.594    5.594
          CUMULATIVE AREA = .01 SQ MI

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*****
*          *
87 KK      *      CH11 *
*          *
*****
          RUNOFF AREA CH11
89 KO      OUTPUT CONTROL VARIABLES
          IPRNT      3 PRINT CONTROL
          IPLOT      0 PLOT CONTROL
          QSCAL      0. HYDROGRAPH PLOT SCALE
          IPNCH      7 PUNCH COMPUTED HYDROGRAPH
          IOUT       21 SAVE HYDROGRAPH ON THIS UNIT
          ISAV1      1 FIRST ORDINATE PUNCHED OR SAVED
          ISAV2      416 LAST ORDINATE PUNCHED OR SAVED
          TIMINT     .083 TIME INTERVAL IN HOURS

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SUBBASIN RUNOFF DATA

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90 BA      SUBBASIN CHARACTERISTICS
          TAREA      .00 SUBBASIN AREA

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PRECIPITATION DATA

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11 PH      DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
          ..... HYDRO-35 ..... TP-40 ..... TP-49 .....

```

5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .00

91 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

92 UK KINEMATIC WAVE
 OVERLAND-FLOW ELEMENT NO. 1
 L 84. OVERLAND FLOW LENGTH
 S .3300 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

93 RD MUSKINGUM-CUNGE
 MAIN CHANNEL
 L 1487. CHANNEL LENGTH
 S .0010 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 10.00 BOTTOM WIDTH OR DIAMETER
 Z 3.00 SIDE SLOPE
 RUPSTQ YES ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS
 COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	2.45	1.67	.49	16.81	22.92	724.87	5.56	.58
MAIN	.44	1.42	5.00	743.50	40.46	735.00	5.42	2.19

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3461E+01 EXCESS= .1364E+01 OUTFLOW= .4683E+01 BASIN STORAGE= .2406E-02 PERCENT ERROR= 2.9

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN .44 1.42 5.00 40.46 735.00 5.42

*** **

HYDROGRAPH AT STATION CH11

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
40.	12.25	8.	2.	2.	2.
		(INCHES) 4.475	5.417	5.421	5.421
		(AC-FT) 4.	5.	5.	5.

CUMULATIVE AREA = .02 SQ MI

*** **

 * *
 94 KK * N2T *
 * *

RUNOFF AREA N2T

96 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

97 BA SUBBASIN CHARACTERISTICS
 TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40					TP-49			
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .01

98 LS SCS LOSS RATE

STRTL	.38	INITIAL ABSTRACTION
CRVNBR	84.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

99 UK KINEMATIC WAVE OVERLAND-FLOW ELEMENT NO. 1

L	553.	OVERLAND FLOW LENGTH
S	.0200	SLOPE
N	.350	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

100 RD MUSKINGUM-CUNGE MAIN CHANNEL

L	644.	CHANNEL LENGTH
S	.0030	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.01	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	.00	BOTTOM WIDTH OR DIAMETER
Z	4.00	SIDE SLOPE
RUPSTQ	NO	ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS
COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANEL	.60	1.67	4.23	92.19	32.17	737.61	5.54	.37
MAIN	1.06	1.33	3.86	322.22	31.70	737.41	5.49	2.78

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .4180E+01 OUTFLOW= .4128E+01 BASIN STORAGE= .7392E-02 PERCENT ERROR= 1.1

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	1.06	1.33	5.00	31.34	735.00	5.49
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HYDROGRAPH AT STATION N2T

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (INCHES)	72-HR (AC-FT)	34.58-HR (CFS)
31.	12.25	7.	4.483	3.	1.
			5.486	4.	5.492
				4.	4.

CUMULATIVE AREA = .01 SQ MI

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* *
101 KK * N2S *
* *

RUNOFF AREA N2S

103 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

104 BA SUBBASIN CHARACTERISTICS

TAREA .00 SUBBASIN AREA

PRECIPITATION DATA

11 PH

DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .00

105 LS

SCS LOSS RATE

STRFL	.33	INITIAL ABSTRACTION
CRVNBR	86.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

106 UK

KINEMATIC WAVE

OVERLAND-FLOW ELEMENT NO. 1

L	80.	OVERLAND FLOW LENGTH
S	.2000	SLOPE
N	.350	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

107 RD

MUSKINGUM-CUNGE

MAIN CHANNEL

L	379.	CHANNEL LENGTH
S	.0100	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.00	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	.00	BOTTOM WIDTH OR DIAMETER
Z	4.00	SIDE SLOPE
RUPSTQ	NO	ROUTE UPSTREAM HYDROGRAPH

*** FDKRUT - NEWTON RAPHSON FAILEDFIXED POINT ITERATION USED - ITERATION= 1

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)	DX (FT)				
PLANE1	1.90	1.67	.56	16.05	24.97	724.49	.49	
MAIN	1.93	1.33	1.54	189.53	24.45	723.94	4.11	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .1513E+01 OUTFLOW= .1483E+01 BASIN STORAGE= .2001E-03 PERCENT ERROR= 2.0

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	1.93	1.33	5.00	23.72	725.00	5.69
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HYDROGRAPH AT STATION N2S

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	34.58-HR	
24.	12.08	2.	1.	1.	1.	
		(INCHES)	4.647	5.686	5.687	5.687
		(AC-FT)	1.	1.	1.	1.

CUMULATIVE AREA = .00 SQ MI

*** **

108 KK

COMBINE N2 AREAS

110 KO

OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT

ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

111 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

 HYDROGRAPH AT STATION CN2
 PEAK FLOW TIME MAXIMUM AVERAGE FLOW
 + (CFS) (HR) 6-HR 24-HR 72-HR 34.58-HR
 + 47. 12.08 (CFS)
 (INCHES) 9. 3. 2. 2.
 (AC-FT) 4.513 5.535 5.542 5.542
 5. 6. 6. 6.
 CUMULATIVE AREA = .02 SQ MI

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 * *
 112 KK * CCH2 *
 * *

 COMBINE AREAS UPSTREAM OF CH2

114 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

115 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

 HYDROGRAPH AT STATION CCH2
 PEAK FLOW TIME MAXIMUM AVERAGE FLOW
 + (CFS) (HR) 6-HR 24-HR 72-HR 34.58-HR
 + 82. 12.17 (CFS)
 (INCHES) 17. 5. 4. 4.
 (AC-FT) 4.494 5.481 5.486 5.486
 8. 10. 10. 10.
 CUMULATIVE AREA = .04 SQ MI

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 * *
 116 KK * CH2 *
 * *

 RUNOFF AREA CH2

118 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

119 BA SUBBASIN CHARACTERISTICS
TAREA .00 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .00

120 LS SCS LOSS RATE
 STRFL .38 INITIAL ABSTRACTION
 CRVNR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

121 UK OVERLAND-FLOW ELEMENT NO. 1
 L 103. OVERLAND FLOW LENGTH
 S .1800 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

122 RD MUSKINGUM-CUNGE
 MAIN CHANNEL
 L 576. CHANNEL LENGTH
 S .0010 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 10.00 BOTTOM WIDTH OR DIAMETER
 Z 3.00 SIDE SLOPE
 RUPSTQ YES ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELERITY
		M	DT	DX				
			(MIN)	(FT)	(CFS)	(MIN)	(IN)	(FPS)
PLANE1	1.81	1.67	.80	20.53	11.58	724.49	5.56	.51
MAIN	.44	1.42	3.94	576.18	84.60	733.28	5.48	2.44

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1030E+02 EXCESS= .7115E+00 OUTFLOW= .1099E+02 BASIN STORAGE= .1160E-02 PERCENT ERROR= .2

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN .44 1.42 5.00 84.05 735.00 5.48

*** **

HYDROGRAPH AT STATION CH2

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
+ 84.	12.25	(CFS)			
		18.	6.	4.	4.
		(INCHES) 4.495	5.477	5.482	5.482
		(AC-FT) 9.	11.	11.	11.

CUMULATIVE AREA = .04 SQ MI

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 * *
 123 KK * N12 *
 * *

RUNOFF AREA N12

125 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

126 BA SUBBASIN CHARACTERISTICS
TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
..... HYDRO-35 TP-40 TP-49
5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
.74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .01

127 LS SCS LOSS RATE
STRFL .38 INITIAL ABSTRACTION
CRVNBR 84.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

128 US SNYDER UNITGRAPH
TP .38 LAG
CP .71 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS

CLARK TC= .46 HR, R= .27 HR
SNYDER TP= .38 HR, CP= .70

UNIT HYDROGRAPH

21 END-OF-PERIOD ORDINATES

1.	5.	9.	13.	15.	13.	10.	8.	6.	4.
0.	2.	2.	1.	1.	1.	0.	0.	0.	0.

*** *** *** *** ***

HYDROGRAPH AT STATION N12

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
28.	12.42	6.	2.	1.	1.
		(INCHES) 4.498	5.538	5.538	5.538
		(AC-FT) 3.	4.	4.	4.

CUMULATIVE AREA = .01 SQ MI

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* *
129 KK * N3T *
* *

RUNOFF AREA N3T

131 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

132 BA SUBBASIN CHARACTERISTICS
TAREA .05 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
..... HYDRO-35 TP-40 TP-49
5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
.74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .05

133 LS SCS LOSS RATE

STRTL .38 INITIAL ABSTRACTION
 CRVNB 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

134 UK KINEMATIC WAVE
 OVERLAND-FLOW ELEMENT NO. 1
 L 512. OVERLAND FLOW LENGTH
 S .0200 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

135 RD MUSKINGUM-CUNGE
 MAIN CHANNEL
 L 692. CHANNEL LENGTH
 S .0030 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .05 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER
 Z 4.00 SIDE SLOPE
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS
 COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	.60	1.67	4.73	102.43	124.46	733.59	5.54	.36
MAIN	1.06	1.33	2.95	691.59	122.61	737.11	5.07	3.91

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .1574E+02 OUTFLOW= .1436E+02 BASIN STORAGE= .2430E-01 PERCENT ERROR= 8.6

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1.06 1.33 5.00 122.18 735.00 5.07

*** **

HYDROGRAPH AT STATION N3T

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
122.	12.25	25. (INCHES)	7. (INCHES)	5. (INCHES)	5. (INCHES)
		4.309 (AC-FT)	5.069 (AC-FT)	5.073 (AC-FT)	5.073 (AC-FT)
		12.	14.	14.	14.

CUMULATIVE AREA = .05 SQ MI

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 * *
 136 KK * N3S *
 * *

RUNOFF AREA N3S

138 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

139 BA SUBBASIN CHARACTERISTICS
 TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40					TP-49			
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .01

140 LS SCS LOSS RATE
STRTL .33 INITIAL ABSTRACTION
CRVNR 86.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

141 UK KINEMATIC WAVE
OVERLAND-FLOW ELEMENT NO. 1
L 90. OVERLAND FLOW LENGTH
S .2000 SLOPE
N .350 ROUGHNESS COEFFICIENT
PA 100.0 PERCENT OF SUBBASIN
DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

142 RD MUSKINGUM-CUNGE
MAIN CHANNEL
L 581. CHANNEL LENGTH
S .0030 SLOPE
N .030 CHANNEL ROUGHNESS COEFFICIENT
CA .01 CONTRIBUTING AREA
SHAPE TRAP CHANNEL SHAPE
WD .00 BOTTOM WIDTH OR DIAMETER
Z 4.00 SIDE SLOPE
RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS
COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	1.90	1.67	.60	17.97	27.38	724.55	5.79	.51
MAIN	1.06	1.33	3.63	290.74	25.94	725.04	5.73	2.67

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .1667E+01 OUTFLOW= .1650E+01 BASIN STORAGE= .4547E-03 PERCENT ERROR= 1.0

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1.06 1.33 5.00 25.88 725.00 5.78

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HYDROGRAPH AT STATION N3S

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (INCHES)	72-HR (AC-FT)	34.58-HR (CFS)
+	26.	12.08	3.	1.	1.
+			4.711	5.775	5.775
			1.	2.	2.

CUMULATIVE AREA = .01 SQ MI

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* *
143 KK * CN3 *
* *

COMBINE N3S, N3T, N12

145 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

146 HC HYDROGRAPH COMBINATION
ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION CN3

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
156.	12.25	33.	10.	7.	7.
		(INCHES) 4.368	5.203	5.208	5.208
		(AC-FT) 17.	20.	20.	20.

CUMULATIVE AREA = .07 SQ MI

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 * *
 147 KK * CCH3 *
 * *

COMBINE AREAS N11, N2, N12, N3 AT CH3

149 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

150 HC HYDROGRAPH COMBINATION

ICOMP	2	NUMBER OF HYDROGRAPHS TO COMBINE
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HYDROGRAPH AT STATION CCH3

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
240.	12.25	51.	15.	11.	11.
		(INCHES) 4.412	5.298	5.303	5.303
		(AC-FT) 26.	31.	31.	31.

CUMULATIVE AREA = .11 SQ MI

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 151 KK * CH3 *
 * *

RUNOFF AREA CH3

153 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

154 BA SUBBASIN CHARACTERISTICS

TAREA	.00	SUBBASIN AREA
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PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .00

155 LS SCS LOSS RATE

STRTL	.38	INITIAL ABSTRACTION
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CRVNBR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

156 UK KINEMATIC WAVE
 OVERLAND-FLOW ELEMENT NO. 1
 L 153. OVERLAND FLOW LENGTH
 S .2750 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

157 RD MUSKINGUM-CUNGE
 MAIN CHANNEL
 L 698. CHANNEL LENGTH
 S .0010 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 20.00 BOTTOM WIDTH OR DIAMETER
 Z 3.00 SIDE SLOPE
 RUPSTQ YES ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)				
PLANE1	2.23	1.67	.90	30.54	17.58	725.17	.67
MAIN	.30	1.48	3.74	697.69	238.09	737.52	5.30

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3069E+02 EXCESS= .1097E+01 OUTFLOW= .3170E+02 BASIN STORAGE= .3574E-02 PERCENT ERROR= .2

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

*** MAIN .30 1.48 5.00 237.19 740.00 5.30 ***

HYDROGRAPH AT STATION CH3

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR (CFS)	24-HR (INCHES)	72-HR (AC-FT)	34.58-HR (CFS)
+ 237.	12.33	53.	16.	11.	11.
		4.407	5.294	5.299	5.299
		26.	32.	32.	32.

CUMULATIVE AREA = .11 SQ MI

158 KK *****
 * N4T *
 * *

RUNOFF AREA N4T

160 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

161 BA SUBBASIN CHARACTERISTICS
 TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35					TP-40					TP-49			
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY		
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00		

STORM AREA = .01

162 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNER 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE
 163 UK OVERLAND-FLOW ELEMENT NO. 1
 L 746. OVERLAND FLOW LENGTH
 S .0200 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

MUSKINGUM-CUNGE
 164 RD MAIN CHANNEL
 L 608. CHANNEL LENGTH
 S .0100 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .01 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER
 Z 4.00 SIDE SLOPE
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS
 COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	.60	1.67	4.67	106.62	22.94	743.34	5.54	.39
MAIN	1.93	1.33	2.52	304.07	22.88	740.50	5.47	4.02

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .3439E+01 OUTFLOW= .3387E+01 BASIN STORAGE= .8891E-02 PERCENT ERROR= 1.3

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	1.93	1.33	5.00	22.84	740.00	5.47
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HYDROGRAPH AT STATION N4T

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
+	23.	12.33			
		(CFS)	6.	2.	1.
		(INCHES)	4.467	5.466	5.474
		(AC-FT)	3.	3.	3.

CUMULATIVE AREA = .01 SQ MI

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 165 KK * N4S *
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RUNOFF AREA N4S

167 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

168 BA SUBBASIN CHARACTERISTICS
 TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN .60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY

.74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .01

169 LS SCS LOSS RATE
STRTL .33 INITIAL ABSTRACTION
CRVNR 86.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

170 UK KINEMATIC WAVE
OVERLAND-FLOW ELEMENT NO. 1
L 78. OVERLAND FLOW LENGTH
S .2000 SLOPE
N .350 ROUGHNESS COEFFICIENT
PA 100.0 PERCENT OF SUBBASIN
DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

171 RD MUSKINGUM-CUNGE
MAIN CHANNEL
L 641. CHANNEL LENGTH
S .0030 SLOPE
N .030 CHANNEL ROUGHNESS COEFFICIENT
CA .01 CONTRIBUTING AREA
SHAPE TRAP CHANNEL SHAPE
WD .00 BOTTOM WIDTH OR DIAMETER
Z 4.00 SIDE SLOPE
RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)	DX (FT)				
PLANE1	1.90	1.67	.57	15.50	40.56	724.99	.48	
MAIN	1.06	1.33	3.62	320.27	35.90	723.22	2.95	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2439E+01 OUTFLOW= .2392E+01 BASIN STORAGE= .5147E-03 PERCENT ERROR= 1.9

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1.06 1.33 5.00 33.64 725.00 5.65

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HYDROGRAPH AT STATION N4S

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
+	34.	12.08	4.	1.	1.
		(CFS)	(INCHES)	(AC-FT)	
		4.607	5.649	5.649	5.649
		2.	2.	2.	2.

CUMULATIVE AREA = .01 SQ MI

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* *
172 KK CN4 *
* *

COMBINE N4 AREAS

174 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

175 HC HYDROGRAPH COMBINATION
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION CN4

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	34.58-HR	
50.	12.08	9.	3.	2.	2.	
		(INCHES)	4.500	5.536	5.545	5.545
		(AC-FT)	5.	6.	6.	6.

CUMULATIVE AREA = .02 SQ MI

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176 KK * CH4 *
* *

RUNOFF AREA CH4

178 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TTMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

179 BA SUBBASIN CHARACTERISTICS

TAREA	.00	SUBBASIN AREA
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PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .00

180 LS SCS LOSS RATE

STRTL	.38	INITIAL ABSTRACTION
CRVNR	84.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

181 UK OVERLAND-FLOW ELEMENT NO. 1

L	101.	OVERLAND FLOW LENGTH
S	.1900	SLOPE
N	.350	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

MUSKINGUM-CUNGE

182 RD MAIN CHANNEL

L	1279.	CHANNEL LENGTH
S	.6050	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.00	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	10.00	BOTTOM WIDTH OR DIAMETER
Z	4.00	SIDE SLOPE
RUPSTQ	YES	ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)	DK (FT)				
PLANE1	1.89	1.67	.69	20.16	23.91	724.62	.52	
MAIN	.97	1.40	5.00	639.25	62.27	730.00	3.83	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5767E+01 EXCESS= .1453E+01 OUTFLOW= .7200E+01 BASIN STORAGE= .1358E-02 PERCENT ERROR= .3

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.97	1.40	5.00	62.27	730.00	5.53
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HYDROGRAPH AT STATION CH4

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
62.	12.17	12.	4.	3.	3.
		(INCHES) 4.503	5.526	5.533	5.533
		(AC-FT) 6.	7.	7.	7.

CUMULATIVE AREA = .02 SQ MI

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183 KK * C1CH4A *
* *

COMBINE AREAS N11, N2, N3, N4 AT CHANNEL CH4A

185 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

186 HC HYDROGRAPH COMBINATION
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION C1CH4A

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
288.	12.25	65.	20.	14.	14.
		(INCHES) 4.424	5.335	5.340	5.340
		(AC-FT) 32.	39.	39.	39.

CUMULATIVE AREA = .14 SQ MI

*** **

* *
187 KK * CH4A *
* *

RUNOFF AREA CH4A

189 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

190 BA SUBBASIN CHARACTERISTICS
TAREA .00 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35					TP-40					TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY			
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00			

STORM AREA = .00

191 LS SCS LOSS RATE
STRTL .38 INITIAL ABSTRACTION
CRVNR 84.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

192 UK KINEMATIC WAVE
OVERLAND-FLOW ELEMENT NO. 1
L 40. OVERLAND FLOW LENGTH
S .3300 SLOPE
N .350 ROUGHNESS COEFFICIENT
PA 100.0 PERCENT OF SUBBASIN
DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

193 RD MUSKINGUM-CUNGE
MAIN CHANNEL
L 520. CHANNEL LENGTH
S .0035 SLOPE
N .030 CHANNEL ROUGHNESS COEFFICIENT
CA .00 CONTRIBUTING AREA
SHAPE TRAP CHANNEL SHAPE
WD 20.00 BOTTOM WIDTH OR DIAMETER
Z 3.00 SIDE SLOPE
RUPSTQ YES ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)				
PLANE1	2.45	1.67	.34	8.08	5.52	724.98	.43
MAIN	.57	1.48	1.73	519.75	287.49	737.40	5.00

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3891E+02 EXCESS= .3261E+00 OUTFLOW= .3920E+02 BASIN STORAGE= .2158E-02 PERCENT ERROR= .1

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.57	1.48	5.00	286.30	735.00	5.34
------	-----	------	------	--------	--------	------

HYDROGRAPH AT STATION CH4A

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW		
		6-HR	24-HR	72-HR
286.	12.25	66.	20.	14.
		4.424 (INCHES)	5.334	5.339
		32. (AC-FT)	39.	39.

CUMULATIVE AREA = .14 SQ MI

* *
194 KK * N13 *
* *

RUNOFF AREA N13

196 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

197 BA SUBBASIN CHARACTERISTICS
TAREA .03 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

.....	HYDRO-35	TP-40	TP-49		
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .03

198 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNBR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

199 US SNYDER UNITGRAPH
 TP .53 LAG
 CP .69 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS

CLARK TC= .64 HR, R= .39 HR
 SNYDER TP= .53 HR, CP= .69

UNIT HYDROGRAPH

30 END-OF-PERIOD ORDINATES

1.	5.	10.	16.	21.	24.	25.	23.	20.	16.
13.	10.	8.	7.	5.	4.	4.	3.	2.	2.
2.	1.	1.	1.	1.	1.	0.	0.	0.	0.

HYDROGRAPH AT STATION N13

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW		
		6-HR	24-HR	72-HR
+	(CFS)	(CFS)		
+	55.	14.	4.	3.
	12.58	4.490	5.535	5.535
		(INCHES)		
		(AC-FT)	7.	9.
			9.	9.

CUMULATIVE AREA = .03 SQ MI

 * *
 200 KK * W1 *
 * *

RUNOFF AREA W1 (POND 1)

202 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

203 BA SUBBASIN CHARACTERISTICS
 TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

.....	HYDRO-35	TP-40	TP-49		
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .01

204 LS SCS LOSS RATE
 STRTL .00 INITIAL ABSTRACTION
 CRVNBR 100.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

205 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG .00 LAG

UNIT HYDROGRAPH
5 END-OF-PERIOD ORDINATES

75. 21. 4. 1. 0.
 *** **

HYDROGRAPH AT STATION W1

TOTAL RAINFALL = 7.44, TOTAL LOSS = .00, TOTAL EXCESS = 7.44

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
67.	12.08	8.	3.	2.	2.
		(INCHES) 5.468	7.437	7.440	7.440
		(AC-FT) 4.	5.	5.	5.

CUMULATIVE AREA = .01 SQ MI

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 206 KK * PNDLIN *
 * *

COMBINE ALL FLOWS INTO POND 1

208 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

209 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION PNDLIN

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
352.	12.25	87.	27.	19.	19.
		(INCHES) 4.493	5.496	5.522	5.522
		(AC-FT) 43.	53.	53.	53.

CUMULATIVE AREA = .18 SQ MI

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 210 KK * PNDLOU * T
 * *

ROUTE THROUGH UPPER DET. POND (POND 1) 3-42" AT 451

212 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

HYDROGRAPH ROUTING DATA

213 RS STORAGE ROUTING

NSTPS	1	NUMBER OF SUBREACHES
ITYP	ELEV	TYPE OF INITIAL CONDITION
RSVRC	455.20	INITIAL CONDITION

X .00 WORKING R AND D COEFFICIENT

214 SA AREA .0 7.8 7.9 8.0 8.2

215 SE ELEVATION 455.20 455.50 456.00 456.50 457.00

217 SL LOW-LEVEL OUTLET
 ELEV 452.77 ELEVATION AT CENTER OF OUTLET
 CAREA 19.64 CROSS-SECTIONAL AREA
 COQL .80 COEFFICIENT
 EXPL .50 EXPONENT OF HEAD

216 SS SPILLWAY
 CREL 456.00 SPILLWAY CREST ELEVATION
 SPWID 25.00 SPILLWAY WIDTH
 COQW 2.60 WEIR COEFFICIENT
 EXPW 1.50 EXPONENT OF HEAD

COMPUTED STORAGE-ELEVATION DATA

STORAGE	.00	.78	4.70	8.69	12.74
ELEVATION	455.20	455.50	456.00	456.50	457.00

COMPUTED OUTFLOW-ELEVATION DATA

OUTFLOW	.00	199.32	202.35	205.47	208.68	212.00	215.43	218.97	222.63	226.41
ELEVATION	455.20	455.27	455.35	455.43	455.51	455.60	455.69	455.79	455.89	456.00
OUTFLOW	237.55	242.13	247.75	254.50	262.48	271.78	282.50	294.73	308.57	324.10
ELEVATION	456.18	456.24	456.30	456.38	456.46	456.55	456.65	456.76	456.88	457.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	.01	.10	.35	.78	.89	1.57	2.29	3.05	3.85
OUTFLOW	196.38	199.32	202.35	205.47	208.15	208.68	212.00	215.43	218.97	222.63
ELEVATION	455.20	455.27	455.35	455.43	455.50	455.51	455.60	455.69	455.79	455.89
STORAGE	4.70	6.12	6.59	7.12	7.72	8.38	8.69	9.12	9.92	10.79
OUTFLOW	226.41	237.55	242.13	247.75	254.50	262.48	266.29	271.78	282.50	294.73
ELEVATION	456.00	456.18	456.24	456.30	456.38	456.46	456.50	456.55	456.65	456.76
STORAGE	11.73	12.74								
OUTFLOW	308.57	324.10								
ELEVATION	456.88	457.00								

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HYDROGRAPH AT STATION PND10U

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	34.58-HR	
+	(CFS)	(HR)					
+	229.	12.75	(CFS)				
			202.	198.	197.	197.	
			(INCHES)	10.427	40.858	58.751	58.751
			(AC-FT)	100.	392.	564.	564.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE				
			6-HR	24-HR	72-HR	34.58-HR	
+	(AC-FT)	(HR)					
	5.	12.75	0.	0.	0.	-1.	
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE				
			6-HR	24-HR	72-HR	34.58-HR	
+	(FEET)	(HR)					
	456.04	12.75	455.34	455.24	455.23	455.23	

CUMULATIVE AREA = .18 SQ MI

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 218 KK N16 *
 * *

RUNOFF AREA N16

220 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED

TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

221 BA SUBBASIN CHARACTERISTICS
TAREA .00 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
..... HYDRO-35 TP-40 TP-49
5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
.74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .00

222 LS SCS LOSS RATE
STRTL .38 INITIAL ABSTRACTION
CRVNR 84.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

223 US SNYDER UNITGRAPH
TP .24 LAG
CP .71 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS
CLARK TC= .31 HR, R= .14 HR
SNYDER TP= .24 HR, CP= .70

UNIT HYDROGRAPH
11 END-OF-PERIOD ORDINATES
1. 5. 8. 8. 5. 3. 1. 1. 0. 0.
0.

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HYDROGRAPH AT STATION N16

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
+ (CFS) (HR) 6-HR 24-HR 72-HR 34.58-HR
+ 12. 12.25 (CFS) 2. 1. 0. 0.
(INCHES) 4.498 5.534 5.534 5.534
(AC-FT) 1. 1. 1. 1.

CUMULATIVE AREA = .00 SQ MI

*** **

224 KK

CHW1

RUNOFF AREA CHW1

226 KO

OUTPUT CONTROL VARIABLES

IPRNT 3 PRINT CONTROL
IFLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

227 BA SUBBASIN CHARACTERISTICS
TAREA .00 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
..... HYDRO-35 TP-40 TP-49
5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
.74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .00

228 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNBR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

229 UK KINEMATIC WAVE
 OVERLAND-FLOW ELEMENT NO. 1
 L 42. OVERLAND FLOW LENGTH
 S .3300 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

230 RD MUSKINGUM-CUNGE
 MAIN CHANNEL
 L 551. CHANNEL LENGTH
 S .0010 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 20.00 BOTTOM WIDTH OR DIAMETER
 Z 3.00 SIDE SLOPE
 RUPSTQ YES ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)	DX (FT)				
PLANE1	2.45	1.67	.39	8.37	7.02	724.78	.44	
MAIN	.30	1.48	5.00	275.57	13.02	740.00	1.25	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1240E+01 EXCESS= .4150E+00 OUTFLOW= .1639E+01 BASIN STORAGE= .1476E-02 PERCENT ERROR= .9

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.30	1.48	5.00	13.02	740.00	5.49
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HYDROGRAPH AT STATION CHW1

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
13.	12.33	3.	1.	1.	1.
		(INCHES) 4.490	5.487	5.487	5.487
		(AC-FT) 1.	2.	2.	2.

CUMULATIVE AREA = .01 SQ MI

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231 KK *****
 * *
 * MIDRD *
 * *

COMBINE ALL FLOWS U/S OF ENTRANCE ROAD

233 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

234 HC HYDROGRAPH COMBINATION
 ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

MAIN	.30	1.48	5.00	13.02	740.00	5.49
------	-----	------	------	-------	--------	------

HYDROGRAPH AT STATION MIDRD

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
		3.	1.	1.	1.
		(INCHES) 4.490	5.487	5.487	5.487
		(AC-FT) 1.	2.	2.	2.

```

+ (CFS) (HR)
+ 2673. 12.75
(CFS) 1070. 468. 385. 385.
(INCHES) 5.060 8.849 10.487 10.487
(AC-FT) 531. 928. 1100. 1100.
CUMULATIVE AREA = 1.97 SQ MI

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235 KK * S5 *
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RUNOFF AREA S5

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237 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

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SUBBASIN RUNOFF DATA

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238 BA SUBBASIN CHARACTERISTICS
TAREA .00 SUBBASIN AREA

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PRECIPITATION DATA

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11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
..... HYDRO-35 ..... TP-40 ..... TP-49 .....
5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
.74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
STORM AREA = .00

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239 LS SCS LOSS RATE
STRFL .38 INITIAL ABSTRACTION
CRVNR 84.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

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240 US SNYDER UNITGRAPH
TP .23 LAG
CP .75 PEAKING COEFFICIENT

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SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

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UNIT HYDROGRAPH PARAMETERS
CLARK TC= .30 HR, R= .12 HR
SNYDER TP= .23 HR, CP= .74

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UNIT HYDROGRAPH
10 END-OF-PERIOD ORDINATES

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0. 1. 2. 2. 1. 1. 0. 0. 0. 0.

```

*** **

HYDROGRAPH AT STATION S5

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

```

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
(CFS) (HR) (CFS)
+ 3. 12.25 0. 0. 0. 0.
(INCHES) 4.499 5.535 5.535 5.535
(AC-FT) 0. 0. 0. 0.
CUMULATIVE AREA = .00 SQ MI

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241 KK * CS5 *
*

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COMBINE ALL FLOWS U/S OF ENTRANCE ROAD WITH S5

243 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

244 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** *** *** *** ***

HYDROGRAPH AT STATION CS5

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	34.58-HR	
2674.	12.75	1070.	468.	385.	385.	
		(INCHES)	5.059	8.847	10.484	10.484
		(AC-FT)	531.	928.	1100.	1100.

CUMULATIVE AREA = 1.97 SQ MI

*** **

245 KK 04

OFFSITE AREA 04

247 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

248 BA SUBBASIN CHARACTERISTICS
 TAREA .13 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35					TP-40					TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY			
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00			

STORM AREA = .13

249 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

250 US SNYDER UNITGRAPH
 TP .43 LAG
 CP .64 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS
 CLARK TC= .51 HR, R= .36 HR
 SNYDER TP= .43 HR, CP= .64

UNIT HYDROGRAPH
 27 END-OF-PERIOD ORDINATES

10.	36.	71.	105.	126.	131.	115.	92.	73.	58.
46.	37.	29.	23.	18.	15.	12.	9.	7.	6.
5.	4.	3.	2.	2.	1.	1.			

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***          ***          ***          ***          ***
          HYDROGRAPH AT STATION      O4
TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56
PEAK FLOW      TIME          MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)          6-HR      24-HR      72-HR      34.58-HR
+ 269.         12.50         (CFS)
          (INCHES) 4.491      20.        14.        14.
          (AC-FT) 32.        5.534      5.534      5.534
          CUMULATIVE AREA = .13 SQ MI

```

```

*****
*
251 KK * C4MWY *
*
*****

```

COMBINE ALL FLOWS UPSTREAM OF N10

```

253 KO OUTPUT CONTROL VARIABLES
      IPRNT 3 PRINT CONTROL
      IPLOT 0 PLOT CONTROL
      QSCAL 0. HYDROGRAPH PLOT SCALE
      IPNCH 7 PUNCH COMPUTED HYDROGRAPH
      IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
      ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
      ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
      TIMINT .083 TIME INTERVAL IN HOURS

```

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254 HC HYDROGRAPH COMBINATION
      ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

```

```

***          ***          ***          ***          ***
          HYDROGRAPH AT STATION      C4MWY
PEAK FLOW      TIME          MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)          6-HR      24-HR      72-HR      34.58-HR
+ 2887.         12.75         (CFS)
          (INCHES) 5.022      488.       399.       399.
          (AC-FT) 563.       8.635     10.168     10.168
          CUMULATIVE AREA = 2.10 SQ MI

```

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*****
*
255 KK * N10T *
*
*****

```

RUNOFF AREA N10T

```

257 KO OUTPUT CONTROL VARIABLES
      IPRNT 3 PRINT CONTROL
      IPLOT 0 PLOT CONTROL
      QSCAL 0. HYDROGRAPH PLOT SCALE
      IPNCH 7 PUNCH COMPUTED HYDROGRAPH
      IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
      ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
      ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
      TIMINT .083 TIME INTERVAL IN HOURS

```

SUBBASIN RUNOFF DATA

```

258 BA SUBBASIN CHARACTERISTICS
      TAREA .02 SUBBASIN AREA

```

PRECIPITATION DATA

```

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
      ..... HYDRO-35 ..... TP-40 ..... TP-49 .....

```

5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .02

259 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

260 UK KINEMATIC WAVE
 OVERLAND-FLOW ELEMENT NO. 1
 L 733. OVERLAND FLOW LENGTH
 S .0200 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

261 RK KINEMATIC WAVE
 MAIN CHANNEL
 L 619. CHANNEL LENGTH
 S .0020 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .02 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER
 Z 4.00 SIDE SLOPE
 NDXMIN 2 MINIMUM NUMBER OF DX INTERVALS
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

 COMPUTED KINEMATIC PARAMETERS
 VARIABLE TIME STEP
 (DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	.60	1.67	4.49	104.72	37.16	741.60	5.54	.39
MAIN	.87	1.33	1.23	206.29	36.95	741.58	5.53	3.19

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .5514E+01 OUTFLOW= .5490E+01 BASIN STORAGE= .1379E-01 PERCENT ERROR= .2

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN .87 1.33 5.00 36.82 745.00 5.55

*** **

HYDROGRAPH AT STATION N10T

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	34.58-HR	
37.	12.42	9.	3.	2.	2.	
		(INCHES)	4.484	5.535	5.546	5.546
		(AC-FT)	4.	5.	6.	6.

CUMULATIVE AREA = .02 SQ MI

*** **

 * *
 262 KK * N10S *
 * *

RUNOFF AREA N10S

264 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

265 BA SUBBASIN CHARACTERISTICS
TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
 STORM AREA = .01

266 LS SCS LOSS RATE
 STRTL .33 INITIAL ABSTRACTION
 CRVNR 86.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

267 UK KINEMATIC WAVE
 OVERLAND-FLOW ELEMENT NO. 1
 L 100. OVERLAND FLOW LENGTH
 S .2000 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

268 RK KINEMATIC WAVE
 MAIN CHANNEL
 L 717. CHANNEL LENGTH
 S .0130 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .01 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER
 Z 4.00 SIDE SLOPE
 NDXMIN 2 MINIMUM NUMBER OF DX INTERVALS
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

 COMPUTED KINEMATIC PARAMETERS
 VARIABLE TIME STEP
 (DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANEL	1.90	1.67	.79	19.95	57.51	724.48	5.79	.53
MAIN	2.21	1.33	.62	239.07	55.67	725.10	5.79	7.10

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .3551E+01 OUTFLOW= .3550E+01 BASIN STORAGE= .1045E-03 PERCENT ERROR= .0

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 2.21 1.33 5.00 55.40 725.00 5.79

*** **

HYDROGRAPH AT STATION N10S

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
55.	12.08	6.	2.	1.	1.
		(INCHES) 4.686	5.794	5.795	5.795
		(AC-FT) 3.	4.	4.	4.

CUMULATIVE AREA = .01 SQ MI

269 KK *****
 * *
 * CN10 *
 * *

COMBINE N10 AREAS

271 KO OUTPUT CONTROL VARIABLES
 IPRNF 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 ICUT 21 SAVE HYDROGRAPH ON THIS UNIT

ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

272 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

 HYDROGRAPH AT STATION CN10
 PEAK FLOW TIME MAXIMUM AVERAGE FLOW
 + (CFS) (HR) 6-HR 24-HR 72-HR 34.58-HR
 + 78. 12.08 (CFS) 15. 5. 3. 3.
 (INCHES) 4.539 5.629 5.641 5.641
 (AC-FT) 7. 9. 9. 9.
 CUMULATIVE AREA = .03 SQ MI
 *** **

 * *
 273 KK CH10 *
 * *

 RUNOFF AREA CH10

275 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

276 BA SUBBASIN CHARACTERISTICS
 TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
 STORM AREA = .01

277 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

278 UK OVERLAND-FLOW ELEMENT NO. 1
 L 88. OVERLAND FLOW LENGTH
 S .0150 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

MUSKINGUM-CUNGE

279 RD MAIN CHANNEL
 L 1454. CHANNEL LENGTH
 S .0110 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .01 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 10.00 BOTTOM WIDTH OR DIAMETER
 Z 3.00 SIDE SLOPE
 RUPSTQ YES ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	M	DT	DX	PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELERITY
			(MIN)	(FT)	(CFS)	(MIN)	(IN)	(FPS)
PLANE1	.52	1.67	1.45	17.68	51.95	725.99	5.56	.21

MAIN 1.45 1.42 3.89 726.90 120.07 728.17 5.59 6.22

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9055E+01 EXCESS= .3884E+01 OUTFLOW= .1288E+02 BASIN STORAGE= .2546E-02 PERCENT ERROR= .4

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

```

***          ***          ***          ***          ***
          MAIN          1.45          1.42          5.00          114.78          730.00          5.59
          ***          ***          ***          ***          ***
          HYDROGRAPH AT STATION          CH10
TOTAL RAINFALL =          7.44, TOTAL LOSS =          1.86, TOTAL EXCESS =          5.56
PEAK FLOW          TIME          MAXIMUM AVERAGE FLOW
+ (CFS)          (HR)          6-HR          24-HR          72-HR          34.58-HR
+ 115.          12.17          (CFS)
          (INCHES)          4.522          5.577          5.586          5.586
          (AC-FT)          10.          13.          13.          13.
          CUMULATIVE AREA =          .04 SQ MI
  
```

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*****
*          *
280 KK          *          CABELM          *
*          *
*****
  
```

COMBINE AREAS UPSTREAM OF ELM FORK

```

282 KO          OUTPUT CONTROL VARIABLES
          IPRNT          3          PRINT CONTROL
          IPLOT          0          PLOT CONTROL
          QSCAL          0.          HYDROGRAPH PLOT SCALE
          IPNCH          7          PUNCH COMPUTED HYDROGRAPH
          IOUT          21          SAVE HYDROGRAPH ON THIS UNIT
          ISAV1          1          FIRST ORDINATE PUNCHED OR SAVED
          ISAV2          416          LAST ORDINATE PUNCHED OR SAVED
          TIMINT          .083          TIME INTERVAL IN HOURS
  
```

```

283 HC          HYDROGRAPH COMBINATION
          ICOMP          2          NUMBER OF HYDROGRAPHS TO COMBINE
  
```

```

***          ***          ***          ***          ***
          HYDROGRAPH AT STATION          CABELM
PEAK FLOW          TIME          MAXIMUM AVERAGE FLOW
+ (CFS)          (HR)          6-HR          24-HR          72-HR          34.58-HR
+ 2933.          12.75          (CFS)
          (INCHES)          5.012          8.574          10.075          10.075
          (AC-FT)          573.          981.          1152.          1152.
          CUMULATIVE AREA =          2.14 SQ MI
  
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*****
*          *
284 KK          *          N9T          *
*          *
*****
  
```

RUNOFF AREA N9T

```

286 KO          OUTPUT CONTROL VARIABLES
          IPRNT          3          PRINT CONTROL
          IPLOT          0          PLOT CONTROL
          QSCAL          0.          HYDROGRAPH PLOT SCALE
          IPNCH          7          PUNCH COMPUTED HYDROGRAPH
          IOUT          21          SAVE HYDROGRAPH ON THIS UNIT
          ISAV1          1          FIRST ORDINATE PUNCHED OR SAVED
          ISAV2          416          LAST ORDINATE PUNCHED OR SAVED
          TIMINT          .083          TIME INTERVAL IN HOURS
  
```

SUBBASIN RUNOFF DATA

287 BA SUBBASIN CHARACTERISTICS
TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
..... HYDRO-35 TP-40 TP-49
5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
.74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .02

288 LS SCS LOSS RATE
STRTL .38 INITIAL ABSTRACTION
CRVNR 84.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

289 UK OVERLAND-FLOW ELEMENT NO. 1
L 566. OVERLAND FLOW LENGTH
S .0200 SLOPE
N .350 ROUGHNESS COEFFICIENT
PA 100.0 PERCENT OF SUBBASIN
DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

KINEMATIC WAVE

290 RK MAIN CHANNEL
L 696. CHANNEL LENGTH
S .0030 SLOPE
N .030 CHANNEL ROUGHNESS COEFFICIENT
CA .02 CONTRIBUTING AREA
SHAPE TRAP CHANNEL SHAPE
WD .00 BOTTOM WIDTH OR DIAMETER
Z 4.00 SIDE SLOPE
NDXMIN 2 MINIMUM NUMBER OF DX INTERVALS
RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

COMPUTED KINEMATIC PARAMETERS
VARIABLE TIME STEP
(DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	.60	1.67	4.26	94.36	40.09	734.99	5.54	.37
MAIN	1.06	1.33	1.05	232.03	39.81	739.00	5.54	3.75

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .5247E+01 OUTFLOW= .5229E+01 BASIN STORAGE= .8873E-02 PERCENT ERROR= .2

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1.06 1.33 5.00 39.58 740.00 5.54

*** **

HYDROGRAPH AT STATION N9T

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
40.	12.33	9.	3.	2.	2.
		(INCHES) 4.481	5.528	5.537	5.537
		(AC-FT) 4.	5.	5.	5.

CUMULATIVE AREA = .02 SQ MI

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* *
291 KK * N9S *
* *

RUNOFF AREA N9S

293 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL

QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

294 BA SUBBASIN CHARACTERISTICS
 TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .01

295 LS SCS LOSS RATE
 STRTL .33 INITIAL ABSTRACTION
 CRVNER 86.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

296 UK OVERLAND-FLOW ELEMENT NO. 1
 L 84. OVERLAND FLOW LENGTH
 S .2000 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

KINEMATIC WAVE

297 RK MAIN CHANNEL
 L 792. CHANNEL LENGTH
 S .0140 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .01 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER
 Z 4.00 SIDE SLOPE
 NDXMIN 2 MINIMUM NUMBER OF DX INTERVALS
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

 COMPUTED KINEMATIC PARAMETERS
 VARIABLE TIME STEP
 (DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANEL	1.90	1.67	.71	16.71	74.98	724.42	5.79	.50
MAIN	2.29	1.33	.57	263.88	73.17	725.45	5.79	7.77

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .4570E+01 OUTFLOW= .4568E+01 BASIN STORAGE= .1143E-03 PERCENT ERROR= .0

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 2.29 1.33 5.00 72.83 725.00 5.80

*** **

HYDROGRAPH AT STATION N9S

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (INCHES)	72-HR (AC-FT)	34.58-HR (CFS)
73.	12.08	7.	4.693	4.	2.
			5.801	5.	5.801

CUMULATIVE AREA = .01 SQ MI

 * *
 298 KK * CN9 *

*

COMBINE N9 AREAS

300 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

301 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION CN9

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
99.	12.08	16.	5.	3.	3.
		(INCHES) 4.559	5.649	5.657	5.657
		(AC-FT) 8.	10.	10.	10.

CUMULATIVE AREA = .03 SQ MI

*** **

 *
 *
 * CH9 *
 *
 *

RUNOFF AREA CH9

304 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

305 BA SUBBASIN CHARACTERISTICS
 TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .01

306 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNR 84.00 CURVE NUMBER
 RTIME .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

307 UK OVERLAND-FLOW ELEMENT NO. 1
 L 85. OVERLAND FLOW LENGTH
 S .1570 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

MUSKINGUM-CUNGE

308 RD MAIN CHANNEL
 L 1689. CHANNEL LENGTH
 S .0010 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .01 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 10.00 BOTTOM WIDTH OR DIAMETER
 Z 3.00 SIDE SLOPE

RUPSTQ YES ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS
COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANEL	1.69	1.67	.64	16.97	26.58	724.79	5.56	.45
MAIN	.44	1.42	5.00	844.65	83.50	735.00	5.58	2.65

CONTINUITY SUMMARY (AC-FT) - INFLOW= .9806E+01 EXCESS= .1601E+01 OUTFLOW= .1129E+02 BASIN STORAGE= .4162E-02 PERCENT ERROR= 1.0

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.44	1.42	5.00	83.50	735.00	5.58
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*** **

HYDROGRAPH AT STATION CH9

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	34.58-HR	
84.	12.25	18.	6.	4.	4.	
		(INCHES)	4.525	5.576	5.584	5.584
		(AC-FT)	9.	11.	11.	11.

CUMULATIVE AREA = .04 SQ MI

*** **

* *
309 KK * N5T *
* *

RUNOFF AREA N5T

311 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

312 BA SUBBASIN CHARACTERISTICS

TAREA	.03	SUBBASIN AREA
-------	-----	---------------

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .03

313 LS SCS LOSS RATE

STRTL	.38	INITIAL ABSTRACTION
CRVNBR	84.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

314 UK KINEMATIC WAVE
OVERLAND-FLOW ELEMENT NO. 1

L	1134.	OVERLAND FLOW LENGTH
S	.0200	SLOPE
N	.350	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

315 RK KINEMATIC WAVE
MAIN CHANNEL

L	154.	CHANNEL LENGTH
S	.0020	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT

CA .03 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER
 Z 4.00 SIDE SLOPE
 NDXMIN 2 MINIMUM NUMBER OF DX INTERVALS
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

 COMPUTED KINEMATIC PARAMETERS
 VARIABLE TIME STEP
 (DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	.60	1.67	5.00	125.96	50.66	750.75	5.52	.42
MAIN	.87	1.33	.30	51.38	50.41	754.37	5.52	3.46

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .9338E+01 OUTFLOW= .9275E+01 BASIN STORAGE= .4378E-01 PERCENT ERROR= .2

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN .87 1.33 5.00 50.41 755.00 5.51

*** **

HYDROGRAPH AT STATION N5T

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
50.	12.58	15.	5.	3.	3.
		(INCHES) 4.428	5.498	5.513	5.513
		(AC-FT) 7.	9.	9.	9.

CUMULATIVE AREA = .03 SQ MI

*** **

 * *
 316 KK * N5S *
 * *

RUNOFF AREA N5S

318 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

319 BA SUBBASIN CHARACTERISTICS
 TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
 STORM AREA = .01

320 LS SCS LOSS RATE
 STRTL .33 INITIAL ABSTRACTION
 CRVNR 86.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

321 UK KINEMATIC WAVE
 OVERLAND-FLOW ELEMENT NO. 1
 L 126. OVERLAND FLOW LENGTH
 S .1400 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN

DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

322 RK KINEMATIC WAVE
 MAIN CHANNEL
 L 629. CHANNEL LENGTH
 S .0100 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .01 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER
 Z 4.00 SIDE SLOPE
 NDxmin 2 MINIMUM NUMBER OF DX INTERVALS
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

 COMPUTED KINEMATIC PARAMETERS
 VARIABLE TIME STEP
 (DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	1.59	1.67	.94	25.22	33.64	725.19	5.79	.51
MAIN	1.93	1.33	.73	209.60	32.50	726.07	5.79	5.64

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2161E+01 OUTFLOW= .2161E+01 BASIN STORAGE= .1163E-03 PERCENT ERROR= .0

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1.93 1.33 5.00 31.52 725.00 5.79

*** **

HYDROGRAPH AT STATION N55

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
32.	12.08	4.	1.	1.	1.
		(INCHES) 4.683	5.791	5.792	5.792
		(AC-FT) 2.	2.	2.	2.

CUMULATIVE AREA = .01 SQ MI

323 KK *****
 * CN5 *

COMBINE N5 AREAS

325 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

326 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION CNS

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
63.	12.08	18.	6.	4.	4.
		(INCHES) 4.458	5.545	5.564	5.564
		(AC-FT) 9.	11.	11.	11.

CUMULATIVE AREA = .04 SQ MI

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 * *
 327 KK * CH5 *
 * *

RUNOFF AREA CH5

329 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

330 BA SUBBASIN CHARACTERISTICS
 TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
 STORM AREA = .01

331 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNER 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

332 UK OVERLAND-FLOW ELEMENT NO. 1
 L 101. OVERLAND FLOW LENGTH
 S .1980 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

MUSKINGUM-CUNGE

333 RD MAIN CHANNEL
 L 1359. CHANNEL LENGTH
 S .0010 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .01 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 10.00 BOTTOM WIDTH OR DIAMETER
 Z 3.00 SIDE SLOPE
 RUPSTQ YES ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)	DX (FT)				
PLANE1	1.89	1.67	.69	20.16	24.88	724.60	5.56	
MAIN	.44	1.42	5.00	679.30	66.15	740.00	5.54	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1142E+02 EXCESS= .1512E+01 OUTFLOW= .1288E+02 BASIN STORAGE= .8477E-02 PERCENT ERROR= .4

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.44	1.42	5.00	66.15	740.00	5.54
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 HYDROGRAPH AT STATION CH5

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	34.58-HR	
+ 66.	12.33	21.	6.	5.	5.	
		(INCHES)	4.444	5.521	5.538	5.538

(AC-FT) 10. 13. 13. 13.
 CUMULATIVE AREA = .04 SQ MI

*** **

334 KK * N6T *

RUNOFF AREA N6T

336 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

337 BA SUBBASIN CHARACTERISTICS
 TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
 STORM AREA = .01

338 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNER 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

339 UK KINEMATIC WAVE
 OVERLAND-FLOW ELEMENT NO. 1
 L 476. OVERLAND FLOW LENGTH
 S .0200 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

340 RK KINEMATIC WAVE
 MAIN CHANNEL
 L 653. CHANNEL LENGTH
 S .0050 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .01 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER
 Z 4.00 SIDE SLOPE
 NDXMIN 2 MINIMUM NUMBER OF DX INTERVALS
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

 COMPUTED KINEMATIC PARAMETERS
 VARIABLE TIME STEP
 (DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	.60	1.67	4.47	95.22	20.75	732.88	5.54	.36
MAIN	1.37	1.33	1.02	217.64	20.70	737.48	5.54	3.88

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2550E+01 OUTFLOW= .2541E+01 BASIN STORAGE= .3798E-02 PERCENT ERROR= .2

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	1.37	1.33	5.00	20.47	735.00	5.53
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HYDROGRAPH AT STATION N6T

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
+ (CFS)	(HR)	(CFS)			
+ 20.	12.25	4.	1.	1.	1.
		(INCHES)	4.475	5.520	5.528
		(AC-FT)	2.	3.	3.

CUMULATIVE AREA = .01 SQ MI

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 * *
 341 KK * N6S *
 * *

RUNOFF AREA N6S

343 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLST	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

344 BA SUBBASIN CHARACTERISTICS

TAREA	.01	SUBBASIN AREA
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PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .01

345 LS SCS LOSS RATE

STRFL	.33	INITIAL ABSTRACTION
CRVNBR	86.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

346 UK KINEMATIC WAVE

OVERLAND-FLOW ELEMENT NO. 1		
L	86.	OVERLAND FLOW LENGTH
S	.2000	SLOPE
N	.350	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

347 RK KINEMATIC WAVE

MAIN CHANNEL		
L	641.	CHANNEL LENGTH
S	.0050	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.01	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	.00	BOTTOM WIDTH OR DIAMETER
Z	4.00	SIDE SLOPE
NDXMIN	2	MINIMUM NUMBER OF DX INTERVALS
RUPSTQ	NO	ROUTE UPSTREAM HYDROGRAPH

 COMPUTED KINEMATIC PARAMETERS
 VARIABLE TIME STEP
 (DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	1.90	1.67	.59	17.15	32.70	724.84	5.79	.50
MAIN	1.37	1.33	.91	213.76	30.94	725.80	5.79	4.27

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .1976E+01 OUTFLOW= .1976E+01 BASIN STORAGE= .4982E-04 PERCENT ERROR= .0

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1.37 1.33 5.00 30.36 725.00 5.80

*** **

HYDROGRAPH AT STATION N65

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
30.	12.08	3.	1.	1.	1.
		(INCHES) 4.692	5.800	5.801	5.801
		(AC-FT) 2.	2.	2.	2.

CUMULATIVE AREA = .01 SQ MI

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*      *
348 KK *   CN6 *
*      *
*****

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COMBINE N6 AREAS

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350 KO  OUTPUT CONTROL VARIABLES
        IPRNT      3  PRINT CONTROL
        IPLOT      0  PLOT CONTROL
        QSCAL      0. HYDROGRAPH PLOT SCALE
        IPNCH      7  PUNCH COMPUTED HYDROGRAPH
        IOUT       21 SAVE HYDROGRAPH ON THIS UNIT
        ISAV1      1  FIRST ORDINATE PUNCHED OR SAVED
        ISAV2     416 LAST ORDINATE PUNCHED OR SAVED
        TIMINT     .083 TIME INTERVAL IN HOURS

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351 HC  HYDROGRAPH COMBINATION
        ICOMP      2  NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION CN6

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
44.	12.08	7.	2.	2.	2.
		(INCHES) 4.554	5.637	5.644	5.644
		(AC-FT) 4.	5.	5.	5.

CUMULATIVE AREA = .02 SQ MI

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*      *
352 KK *   CCH6 *
*      *
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COMBINE AREAS N5 AND N6 AT CH6

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354 KO  OUTPUT CONTROL VARIABLES
        IPRNT      3  PRINT CONTROL
        IPLOT      0  PLOT CONTROL
        QSCAL      0. HYDROGRAPH PLOT SCALE
        IPNCH      7  PUNCH COMPUTED HYDROGRAPH
        IOUT       21 SAVE HYDROGRAPH ON THIS UNIT
        ISAV1      1  FIRST ORDINATE PUNCHED OR SAVED
        ISAV2     416 LAST ORDINATE PUNCHED OR SAVED
        TIMINT     .083 TIME INTERVAL IN HOURS

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355 HC  HYDROGRAPH COMBINATION
        ICOMP      2  NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION CCH6

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
100.	12.17	28. (INCHES) (AC-FT)	9. 4.464 14.	6. 5.549 17.	6. 5.565 17.

CUMULATIVE AREA = .06 SQ MI

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* *
356 KK * CH6 *
* *

RUNOFF AREA CH6

358 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLST	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

359 BA SUBBASIN CHARACTERISTICS

TAREA	.00	SUBBASIN AREA
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PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .00

360 LS SCS LOSS RATE

STRTL	.38	INITIAL ABSTRACTION
CRVNR	84.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

361 UK KINEMATIC WAVE

OVERLAND-FLOW ELEMENT NO. 1		
L	101.	OVERLAND FLOW LENGTH
S	.1700	SLOPE
N	.350	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

362 RD MUSKINGUM-CUNGE

MAIN CHANNEL		
L	1371.	CHANNEL LENGTH
S	.0010	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.00	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	20.00	BOTTOM WIDTH OR DIAMETER
Z	3.00	SIDE SLOPE
RUPSTQ	YES	ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)	DX (FT)				
PLANEL	1.76	1.67	.74	20.24	22.15	725.13	5.56	
MAIN	.30	1.48	5.00	685.60	101.78	740.00	5.54	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1739E+02 EXCESS= .1364E+01 OUTFLOW= .1868E+02 BASIN STORAGE= .1235E-01 PERCENT ERROR= .4

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	.30	1.48	5.00	101.78	740.00	5.54
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HYDROGRAPH AT STATION CH6

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.08, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	34.58-HR	
102.	12.33	30.	9.	7.	7.	
		(INCHES)	4.449	5.527	5.541	5.541
		(AC-FT)	15.	19.	19.	19.

CUMULATIVE AREA = .06 SQ MI

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* *
363 KK * N7AT *
* *

RUNOFF AREA N7AT

365 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLST	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

366 BA SUBBASIN CHARACTERISTICS

TAREA	.02	SUBBASIN AREA
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PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .02

367 LS SCS LOSS RATE

STRTL	.38	INITIAL ABSTRACTION
CRVNR	84.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

368 UK OVERLAND-FLOW ELEMENT NO. 1

L	583.	OVERLAND FLOW LENGTH
S	.0200	SLOPE
N	.350	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

KINEMATIC WAVE

369 RK MAIN CHANNEL

L	408.	CHANNEL LENGTH
S	.0030	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.02	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	.00	BOTTOM WIDTH OR DIAMETER
Z	4.00	SIDE SLOPE
NDXMIN	2	MINIMUM NUMBER OF DX INTERVALS
RUPSTQ	NO	ROUTE UPSTREAM HYDROGRAPH

COMPUTED KINEMATIC PARAMETERS
VARIABLE TIME STEP
(DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	.60	1.67	4.35	97.14	42.01	738.86	5.54	.37
MAIN	1.06	1.33	.75	136.06	41.97	738.16	5.54	3.86

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .5603E+01 OUTFLOW= .5580E+01 BASIN STORAGE= .9999E-02 PERCENT ERROR= .2

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

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MAIN          1.06    1.33    5.00          41.55   740.00   5.48
***          ***          ***          ***          ***
HYDROGRAPH AT STATION  N7AT
TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56
PEAK FLOW      TIME          MAXIMUM AVERAGE FLOW
+ (CFS)        (HR)          6-HR    24-HR    72-HR    34.58-HR
+ 42.         12.33          (CFS)
                (INCHES)  4.422   5.469   5.478   5.478
                (AC-FT)   4.       6.       6.       6.
CUMULATIVE AREA = .02 SQ MI
    
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*****
*      *
370 KK *      N7AS *
*      *
*****
    
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RUNOFF AREA N7AS

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372 KO  OUTPUT CONTROL VARIABLES
        IPRNT      3  PRINT CONTROL
        IPLOT      0  PLOT CONTROL
        QSCAL      0. HYDROGRAPH PLOT SCALE
        IPNCH      7  PUNCH COMPUTED HYDROGRAPH
        IOUT       21 SAVE HYDROGRAPH ON THIS UNIT
        ISAV1      1  FIRST ORDINATE PUNCHED OR SAVED
        ISAV2     416 LAST ORDINATE PUNCHED OR SAVED
        TIMINT     .083 TIME INTERVAL IN HOURS
    
```

SUBBASIN RUNOFF DATA

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373 BA  SUBBASIN CHARACTERISTICS
        TAREA      .01 SUBBASIN AREA
    
```

PRECIPITATION DATA

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11 PH  DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
        ..... HYDRO-35 ..... TP-40 ..... TP-49 .....
        5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
        .74  1.57  3.19  4.18  4.52  5.47  6.43  7.44  .00  .00  .00  .00
    
```

STORM AREA = .01

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374 LS  SCS LOSS RATE
        STRFL      .33 INITIAL ABSTRACTION
        CRVNR      86.00 CURVE NUMBER
        RTIMP      .00 PERCENT IMPERVIOUS AREA
    
```

KINEMATIC WAVE

```

375 UK  OVERLAND-FLOW ELEMENT NO. 1
        L          92. OVERLAND FLOW LENGTH
        S          .2000 SLOPE
        N          .350 ROUGHNESS COEFFICIENT
        PA        100.0 PERCENT OF SUBBASIN
        DXMIN      5  MINIMUM NUMBER OF DX INTERVALS
    
```

KINEMATIC WAVE

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376 RK  MAIN CHANNEL
        L          467. CHANNEL LENGTH
        S          .0110 SLOPE
        N          .030 CHANNEL ROUGHNESS COEFFICIENT
        CA         .01 CONTRIBUTING AREA
        SHAPE      TRAP CHANNEL SHAPE
        WD         .00 BOTTOM WIDTH OR DIAMETER
        Z          4.00 SIDE SLOPE
        NDXMIN     2  MINIMUM NUMBER OF DX INTERVALS
        RUPSTQ     NO  ROUTE UPSTREAM HYDROGRAPH
    
```

 COMPUTED KINEMATIC PARAMETERS
 VARIABLE TIME STEP
 (DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
---------	-------	---	-------------	------------	---------------	--------------------------	----------------	------------------------------

PLANE1 1.90 1.67 .76 18.35 34.43 724.63 5.79 .52
 MAIN 2.03 1.33 .46 155.79 33.53 725.11 5.79 5.85

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2100E+01 OUTFLOW= .2098E+01 BASIN STORAGE= .5111E-04 PERCENT ERROR= .0

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

*** ***(MAIN) 2.03 1.33 5.00 33.45 725.00 5.80***

HYDROGRAPH AT STATION N7AS

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
33.	12.08	3.	1.	1.	1.
		(INCHES) 4.694	5.802	5.802	5.802
		(AC-FT) 2.	2.	2.	2.

CUMULATIVE AREA = .01 SQ MI

 * *
 377 KK * CN7A *
 * *

COMBINE N7A AREAS

379 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLST	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

380 HC HYDROGRAPH COMBINATION

ICOMP	2	NUMBER OF HYDROGRAPHS TO COMBINE
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*** ***(MAIN) 2.03 1.33 5.00 33.45 725.00 5.80***

HYDROGRAPH AT STATION CN7A

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
61.	12.08	12.	4.	3.	3.
		(INCHES) 4.480	5.553	5.564	5.564
		(AC-FT) 6.	8.	8.	8.

CUMULATIVE AREA = .03 SQ MI

 * *
 381 KK * CCH7A *
 * *

COMBINE AREAS N5, N6, N7A AT CH7A

383 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLST	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

384 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** *** *** *** ***

HYDROGRAPH AT STATION CCH7A

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
153.	12.33	43.	13.	9.	9.
		4.453	5.534	5.548	5.548
		21.	26.	26.	26.

CUMULATIVE AREA = .09 SQ MI

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 385 KK CH7A *
 * *

RUNOFF AREA CH7A

387 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

388 BA SUBBASIN CHARACTERISTICS
 TAREA .00 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .00

389 LS SCS LOSS RATE

STRTL	.38	INITIAL ABSTRACTION
CRVNR	84.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

390 UK OVERLAND-FLOW ELEMENT NO. 1

L	78.	OVERLAND FLOW LENGTH
S	.2030	SLOPE
N	.350	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

MUSKINGUM-CUNGE

391 RD MAIN CHANNEL

L	885.	CHANNEL LENGTH
S	.0010	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.00	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	40.00	BOTTOM WIDTH OR DIAMETER
Z	3.00	SIDE SLOPE
RUPSTQ	YES	ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DX (FT)				
PLANE1	1.92	1.67	.70	15.66	17.79	724.44	5.56
MAIN	.19	1.54	5.00	885.29	153.03	745.00	5.53

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2630E+02 EXCESS= .1067E+01 OUTFLOW= .2726E+02 BASIN STORAGE= .1321E-01 PERCENT ERROR= .4

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

	MAIN	.19	1.54	5.00	153.03	745.00	5.53
***	***	***	***	***	***		

HYDROGRAPH AT STATION CH7A

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	34.58-HR
+ 153.	12.42	(CFS)	44.	14.	10.	10.
		(INCHES)	4.441	5.512	5.525	5.525
		(AC-FT)	22.	27.	27.	27.

CUMULATIVE AREA = .09 SQ MI

392 KK * N7BT *

RUNOFF AREA N7BT

394 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

395 BA SUBBASIN CHARACTERISTICS

TAREA	.01	SUBBASIN AREA
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PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

.....	HYDRO-35	TP-40	TP-49	
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .01

396 LS SCS LOSS RATE

STRTL	.38	INITIAL ABSTRACTION
CRVNB	84.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

397 UK OVERLAND-FLOW ELEMENT NO. 1

L	563.	OVERLAND FLOW LENGTH
S	.0200	SLOPE
N	.350	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

KINEMATIC WAVE

398 RK MAIN CHANNEL

L	410.	CHANNEL LENGTH
S	.0030	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.01	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	.00	BOTTOM WIDTH OR DIAMETER
Z	4.00	SIDE SLOPE
NDXMIN	2	MINIMUM NUMBER OF DX INTERVALS
RUPSTQ	NO	ROUTE UPSTREAM HYDROGRAPH

COMPUTED KINEMATIC PARAMETERS
VARIABLE TIME STEP
(DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT	DX	PEAK	TIME TO	VOLUME	MAXIMUM
---------	-------	---	----	----	------	---------	--------	---------

	(MIN)	(FT)	(CFS)	PEAK (MIN)	(IN)	CELERITY (FPS)
PLANE1	.60	1.67	4.26	93.81	19.21	734.56
MAIN	1.06	1.33	.87	136.73	19.17	738.52
						5.54
						3.16

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2520E+01 OUTFLOW= .2511E+01 BASIN STORAGE= .4450E-02 PERCENT ERROR= .2

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1.06 1.33 5.00 18.96 740.00 5.51

*** **

HYDROGRAPH AT STATION N7BT

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (CFS)	72-HR (CFS)	34.58-HR (CFS)
19.	12.33	4.	1.	1.	1.
		4.458 (INCHES)	5.504	5.513	5.513
		2.	2.	2.	2.

CUMULATIVE AREA = .01 SQ MI

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*
* N7BS *
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RUNOFF AREA N7BS

401 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

402 BA SUBBASIN CHARACTERISTICS

TAREA	.01	SUBBASIN AREA
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PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .01

403 LS SCS LOSS RATE

STRPL	.33	INITIAL ABSTRACTION
CRVNBR	86.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

404 UK OVERLAND-FLOW ELEMENT NO. 1

L	86.	OVERLAND FLOW LENGTH
S	.2000	SLOPE
N	.350	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

KINEMATIC WAVE

405 RK MAIN CHANNEL

L	405.	CHANNEL LENGTH
S	.0140	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.01	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	.00	BOTTOM WIDTH OR DIAMETER
Z	4.00	SIDE SLOPE
NDXMIN	2	MINIMUM NUMBER OF DX INTERVALS
RUPSTQ	NO	ROUTE UPSTREAM HYDROGRAPH

 COMPUTED KINEMATIC PARAMETERS
 VARIABLE TIME STEP
 (DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	1.90	1.67	.73	17.29	26.43	725.04	5.79	.51
MAIN	2.29	1.33	.46	135.11	26.06	725.03	5.79	6.08

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .1606E+01 OUTFLOW= .1605E+01 BASIN STORAGE= .3639E-04 PERCENT ERROR= .0

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 2.29 1.33 5.00 26.03 725.00 5.80

*** *** *** *** ***

HYDROGRAPH AT STATION N7B

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79

PEAK FLOW {CFS}	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
+ 26.	12.08	3.	1.	1.	1.
		(INCHES) 4.696	5.804	5.804	5.804
		(AC-FT) 1.	2.	2.	2.

CUMULATIVE AREA = .01 SQ MI

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406 KK *   CN7B *
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*****
  
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COMBINE N7B AREAS

408 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLST	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

409 HC HYDROGRAPH COMBINATION

ICOMP	2	NUMBER OF HYDROGRAPHS TO COMBINE
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HYDROGRAPH AT STATION CN7B

PEAK FLOW {CFS}	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
+ 39.	12.08	7.	2.	1.	1.
		(INCHES) 4.530	5.614	5.624	5.624
		(AC-FT) 3.	4.	4.	4.

CUMULATIVE AREA = .01 SQ MI

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410 KK *   CCH7B *
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COMBINE AREAS N5, N6, N7A, N7B AT CH7B

412 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

413 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** *** *** *** ***

HYDROGRAPH AT STATION CCH7B

PEAK FLOW (CFS)	TIME (HR)	(CFS)	MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	34.58-HR
+ 178.	12.33		51.	16.	11.	11.
		(INCHES)	4.449	5.525	5.538	5.538
		(AC-FT)	25.	31.	31.	31.

CUMULATIVE AREA = .11 SQ MI

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 414 KK * CH7B *
 * *

 RUNOFF AREA CH7A

416 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

417 BA SUBBASIN CHARACTERISTICS
 TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40					TP-49			
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .01

418 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNBR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE

419 UK OVERLAND-FLOW ELEMENT NO. 1
 L 109. OVERLAND FLOW LENGTH
 S .1770 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

MUSKINGUM-CUNGE

420 RD MAIN CHANNEL
 L 1127. CHANNEL LENGTH
 S .0010 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .01 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 40.00 BOTTOM WIDTH OR DIAMETER
 Z 3.00 SIDE SLOPE
 RUPSTQ YES ROUTE UPSTREAM HYDROGRAPH

COMPUTED MUSKINGUM-CUNGE PARAMETERS
COMPUTATION TIME STEP

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	1.79	1.67	.76	21.81	27.68	724.82	5.56	.52
MAIN	.19	1.54	5.00	1127.00	178.99	745.00	5.50	2.53

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3137E+02 EXCESS= .1690E+01 OUTFLOW= .3283E+02 BASIN STORAGE= .1812E-01 PERCENT ERROR= .6

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN .19 1.54 5.00 178.99 745.00 5.50

*** **

HYDROGRAPH AT STATION CH7B

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (INCHES)	72-HR (AC-FT)	34.58-HR (CFS)
179.	12.42	53.	4.431	26.	11.
			5.489	33.	11.
			5.501	33.	11.

CUMULATIVE AREA = .11 SQ MI

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421 KK * N8T *
* *

RUNOFF AREA N8T

423 KO OUTPUT CONTROL VARIABLES

IFRNT	3	PRINT CONTROL
IPLST	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

424 BA SUBBASIN CHARACTERISTICS
TAREA .03 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .03

425 LS SCS LOSS RATE

STRTL	.38	INITIAL ABSTRACTION
CRVNBR	84.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

426 UK KINEMATIC WAVE
OVERLAND-FLOW ELEMENT NO. 1

L	552.	OVERLAND FLOW LENGTH
S	.0200	SLOPE
N	.350	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

427 RK KINEMATIC WAVE
MAIN CHANNEL

L	668.	CHANNEL LENGTH
S	.0030	SLOPE
N	.030	CHANNEL ROUGHNESS COEFFICIENT
CA	.03	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	.00	BOTTOM WIDTH OR DIAMETER

Z 4.00 SIDE SLOPE
 NDXMIN 2 MINIMUM NUMBER OF DX INTERVALS
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

 COMPUTED KINEMATIC PARAMETERS
 VARIABLE TIME STEP
 (DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANE1	.60	1.67	4.22	91.99	58.94	737.44	5.54	.37
MAIN	1.06	1.33	1.03	222.57	58.33	737.03	5.54	4.16

CONTINUITY SUMMARY (AC-FT) -- INFLOW= .0000E+00 EXCESS= .7648E+01 OUTFLOW= .7622E+01 BASIN STORAGE= .1297E-01 PERCENT ERROR= .2

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 1.06 1.33 5.00 58.04 740.00 5.53

*** *** *** *** ***

HYDROGRAPH AT STATION N8T

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR (CFS)	24-HR	72-HR	34.58-HR
+ 58.	12.33	12.	4.	3.	3.
		(INCHES) 4.479	5.525	5.534	5.534
		(AC-FT) 6.	8.	8.	8.

CUMULATIVE AREA = .03 SQ MI

 * *
 428 KK * N8S *
 * *

RUNOFF AREA N8S

430 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

431 BA SUBBASIN CHARACTERISTICS
 TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
 STORM AREA = .02

432 LS SCS LOSS RATE
 STRTL .33 INITIAL ABSTRACTION
 CRVNR 86.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE
 433 UK OVERLAND-FLOW ELEMENT NO. 1
 L 92. OVERLAND FLOW LENGTH
 S .2000 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

KINEMATIC WAVE

434 RK MAIN CHANNEL
 L 925. CHANNEL LENGTH
 S .0180 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .02 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD .00 BOTTOM WIDTH OR DIAMETER
 Z 4.00 SIDE SLOPE
 NDXMIN 2 MINIMUM NUMBER OF DX INTERVALS
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

 COMPUTED KINEMATIC PARAMETERS
 VARIABLE TIME STEP
 (DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANEL	1.90	1.67	.76	18.34	81.00	724.62	5.79	.52
MAIN	2.60	1.33	.67	308.17	78.07	725.64	5.79	8.74

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .4940E+01 OUTFLOW= .4939E+01 BASIN STORAGE= .1245E-03 PERCENT ERROR= .0

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 2.60 1.33 5.00 77.49 725.00 5.80

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HYDROGRAPH AT STATION N8S

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.65, TOTAL EXCESS = 5.79

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
77.	12.08	8.	2.	2.	2.
		(INCHES) 4.689	5.797	5.797	5.797
		(AC-FT) 4.	5.	5.	5.

CUMULATIVE AREA = .02 SQ MI

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 * *
 435 KK * CN8 *
 * *

COMBINE N8 AREAS

437 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

438 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION CN8

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
116.	12.08	20.	6.	4.	4.
		(INCHES) 4.543	5.626	5.635	5.635
		(AC-FT) 10.	13.	13.	13.

CUMULATIVE AREA = .04 SQ MI

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* *
439 KK C2W2 *
* *

COMBINE AREAS N5-N9 INTO POND 2

441 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

442 HC HYDROGRAPH COMBINATION
ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION C2W2

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	34.58-HR	
+	334.	12.33				
		(CFS)	92.	29.	20.	20.
		(INCHES)	4.469	5.536	5.547	5.547
		(AC-FT)	46.	57.	57.	57.
CUMULATIVE AREA =			.19 SQ MI			

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443 KK W2 *
* *

RUNOFF WITHIN POND 2

445 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

446 BA SUBBASIN CHARACTERISTICS
TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

11 PH	DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM											
	HYDRO-35			TP-40				TP-49				
	5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
	.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00
STORM AREA =		.02										

447 LS SCS LOSS RATE
STRTL .00 INITIAL ABSTRACTION
CRVNR 100.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

448 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .00 LAG

UNIT HYDROGRAPH
5 END-OF-PERIOD ORDINATES

89. 25. 5. 1. 0.

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***          ***          ***          ***          ***
          HYDROGRAPH AT STATION      W2
TOTAL RAINFALL = 7.44, TOTAL LOSS = .00, TOTAL EXCESS = 7.44
PEAK FLOW      TIME
+ (CFS)        (HR)
+ 79.          12.08
          (CFS)
          (INCHES) 5.468
          (AC-FT)  4.
          CUMULATIVE AREA = .02 SQ MI
          MAXIMUM AVERAGE FLOW
          6-HR      24-HR      72-HR      34.58-HR
          9.        3.         2.         2.
          5.468    7.437    7.440    7.440
          4.        6.         6.         6.

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449 KK      * PND2IN *
*          *
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COMBINE AREAS INTO POND 2

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451 KO      OUTPUT CONTROL VARIABLES
          IPRNT      3 PRINT CONTROL
          IPLOT      0 PLOT CONTROL
          QSCAL      0. HYDROGRAPH PLOT SCALE
          IPNCH      7 PUNCH COMPUTED HYDROGRAPH
          IOUT       21 SAVE HYDROGRAPH ON THIS UNIT
          ISAV1      1 FIRST ORDINATE PUNCHED OR SAVED
          ISAV2     416 LAST ORDINATE PUNCHED OR SAVED
          TIMINT     .083 TIME INTERVAL IN HOURS

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452 HC      HYDROGRAPH COMBINATION
          ICOMP      2 NUMBER OF HYDROGRAPHS TO COMBINE

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***          ***          ***          ***          ***
          HYDROGRAPH AT STATION      PND2IN
PEAK FLOW      TIME
+ (CFS)        (HR)
+ 366.         12.25
          (CFS)
          (INCHES) 4.523
          (AC-FT)  50.
          CUMULATIVE AREA = .21 SQ MI
          MAXIMUM AVERAGE FLOW
          6-HR      24-HR      72-HR      34.58-HR
          101.     31.        22.        22.
          4.523   5.645    5.688    5.688
          50.     62.        63.        63.

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*          *
453 KK      * PD2OUT *
*          *
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ROUTE THROUGH POND W2

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455 KO      OUTPUT CONTROL VARIABLES
          IPRNT      3 PRINT CONTROL
          IPLOT      0 PLOT CONTROL
          QSCAL      0. HYDROGRAPH PLOT SCALE
          IPNCH      7 PUNCH COMPUTED HYDROGRAPH
          IOUT       21 SAVE HYDROGRAPH ON THIS UNIT
          ISAV1      1 FIRST ORDINATE PUNCHED OR SAVED
          ISAV2     416 LAST ORDINATE PUNCHED OR SAVED
          TIMINT     .083 TIME INTERVAL IN HOURS

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HYDROGRAPH ROUTING DATA

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456 RS      STORAGE ROUTING
          NSTPS      1 NUMBER OF SUBREACHES
          ITYP       ELEV TYPE OF INITIAL CONDITION
          RSVRIC     454.00 INITIAL CONDITION
          X          .00 WORKING R AND D COEFFICIENT

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457 SA      AREA          .0      4.4      6.8      8.3      8.4      8.5      8.6      8.9      9.1

```

458 SE ELEVATION 454.00 454.50 455.00 455.50 456.00 456.50 457.00 458.00 459.00

460 SL LOW-LEVEL OUTLET
 ELEV 456.00 ELEVATION AT CENTER OF OUTLET
 CAREA 28.27 CROSS-SECTIONAL AREA
 COQL .80 COEFFICIENT
 EXPL .50 EXPONENT OF HEAD

459 SS SPILLWAY
 CREL 458.00 SPILLWAY CREST ELEVATION
 SPWID 25.00 SPILLWAY WIDTH
 COQW 2.60 WEIR COEFFICIENT
 EXPW 1.50 EXPONENT OF HEAD

COMPUTED STORAGE-ELEVATION DATA

STORAGE	.00	.74	3.53	7.28	11.44	15.66	19.94	28.69	37.69
ELEVATION	454.00	454.50	455.00	455.50	456.00	456.50	457.00	458.00	459.00

COMPUTED OUTFLOW-ELEVATION DATA

OUTFLOW	.00	.00	284.43	280.08	275.86	271.77	267.80	263.94	260.19	256.55
ELEVATION	454.00	456.00	458.46	458.38	458.31	458.24	458.18	458.12	458.06	458.00
OUTFLOW	307.16	313.30	319.87	326.90	334.39	342.35	350.80	359.75	369.22	379.21
ELEVATION	458.48	458.53	458.58	458.63	458.69	458.74	458.81	458.87	458.93	459.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	.74	3.53	7.28	11.44	15.66	19.94	28.69	32.78	32.97
OUTFLOW	.00	.00	.00	.00	.00	128.27	181.41	256.55	304.59	307.16
ELEVATION	454.00	454.50	455.00	455.50	456.00	456.50	457.00	458.00	458.46	458.48
STORAGE	33.40	33.86	34.34	34.85	35.37	35.92	36.48	37.07	37.69	
OUTFLOW	313.30	319.87	326.90	334.39	342.35	350.80	359.75	369.22	379.21	
ELEVATION	458.53	458.58	458.63	458.69	458.74	458.81	458.87	458.93	459.00	

*** *** *** *** ***

HYDROGRAPH AT STATION PD2OUT

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
+ (CFS)	(HR)	(CFS)			
+ 201.	13.00	88.	26.	18.	18.
		(INCHES)	3.933	4.651	4.651
		(AC-FT)	43.	51.	51.
PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	34.58-HR
+ (AC-FT)	(HR)				
+ 22.	13.00	15.	12.	9.	9.
PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	34.58-HR
+ (FEET)	(HR)				
+ 457.26	13.00	456.44	456.08	455.54	455.54

CUMULATIVE AREA = .21 SQ MI

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 * *
 461 KK * N14 *
 * *

RUNOFF AREA N14

463 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

464 BA SUBBASIN CHARACTERISTICS
 TAREA .04 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
 STORM AREA = .04

465 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

466 US SNYDER UNITGRAPH
 TP .38 LAG
 CP .67 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS
 CLARK TC= .45 HR, R= .31 HR
 SNYDER TP= .38 HR, CP= .67

UNIT HYDROGRAPH
 23 END-OF-PERIOD ORDINATES
 4. 15. 29. 41. 46. 42. 33. 25. 19. 14.
 11. 8. 6. 5. 4. 3. 2. 2. 1. 1.
 1. 1. 0.

*** **

HYDROGRAPH AT STATION N14

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56
 PEAK FLOW TIME MAXIMUM AVERAGE FLOW
 + (CFS) (HR) 6-HR 24-HR 72-HR 34.56-HR
 + 88. 12.42 (CFS) 20. 6. 4. 4.
 (INCHES) 4.495 5.536 5.536 5.536
 (AC-FT) 10. 12. 12. 12.
 CUMULATIVE AREA = .04 SQ MI

*** **

 * *
 467 KK * N15 *
 * *

RUNOFF AREA N15

469 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

470 BA SUBBASIN CHARACTERISTICS
 TAREA .03 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
 STORM AREA = .03

471 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

472 US SNYDER UNITGRAPH
 TP .47 LAG

CP .68 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS
CLARK TC= .56 HR, R= .36 HR
SNYDER TP= .47 HR, CP= .69

UNIT HYDROGRAPH
27 END-OF-PERIOD ORDINATES

2. 7. 14. 21. 27. 29. 28. 23. 18. 15.
12. 9. 7. 6. 5. 4. 3. 2. 2. 1.
1. 1. 1. 1. 0. 0. 0.

*** **

HYDROGRAPH AT STATION N15

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
(CFS) (HR) 6-HR 24-HR 72-HR 34.58-HR
+ 61. 12.50
(INCHES) 4.491 5.534 5.534 5.534
(AC-FT) 7. 9. 9. 9.
CUMULATIVE AREA = .03 SQ MI

*** **

* *
473 KK * C1N14 *
* *

COMBINE AREAS N14, N15 & POND 2

475 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

476 HC HYDROGRAPH COMBINATION
ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION C1N14

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
(CFS) (HR) 6-HR 24-HR 72-HR 34.58-HR
+ 325. 12.58
(INCHES) 3.995 4.870 4.878 4.878
(AC-FT) 59. 72. 73. 73.
CUMULATIVE AREA = .28 SQ MI

*** **

* *
477 KK * S2 *
* *

RUNOFF AREA S2

479 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH

IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

480 BA SUBBASIN CHARACTERISTICS
 TAREA .05 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .05

481 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

482 US SNYDER UNITGRAPH
 TP .73 LAG
 CP .67 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS

CLARK TC= .84 HR, R= .59 HR
 SNYDER TP= .74 HR, CP= .68

UNIT HYDROGRAPH
 43 END-OF-PERIOD ORDINATES

1.	4.	8.	13.	18.	23.	26.	29.	30.	29.
26.	23.	20.	17.	15.	13.	11.	10.	9.	7.
6.	6.	5.	4.	4.	3.	3.	2.	2.	2.
2.	1.	1.	1.	1.	1.	1.	1.	1.	0.
0.	0.	0.							

*** *** *** ***

HYDROGRAPH AT STATION S2

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	34.58-HR
75.	12.75	24.	7.	5.	5.
		(INCHES)	4.475	5.531	5.531
		(AC-FT)	12.	15.	15.

CUMULATIVE AREA = .05 SQ MI

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 483 KK * N19 *
 * *

RUNOFF AREA N19

485 KO OUTPUT CONTROL VARIABLES
 IPRWT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

486 BA SUBBASIN CHARACTERISTICS
 TAREA .00 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

..... HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .00

487 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

488 UK KINEMATIC WAVE
 OVERLAND-FLOW ELEMENT NO. 1
 L 44. OVERLAND FLOW LENGTH
 S .3300 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

489 RD MUSKINGUM-CUNGE
 MAIN CHANNEL
 L 1305. CHANNEL LENGTH
 S .0016 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .00 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 10.00 BOTTOM WIDTH OR DIAMETER
 Z 3.00 SIDE SLOPE
 RUPSTQ YES ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP		PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)				
PLANE1	2.45	1.67	.46	8.73	14.05	724.63	5.56
MAIN	.55	1.42	5.00	652.50	75.13	775.00	5.53

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1454E+02 EXCESS= .8301E+00 OUTFLOW= .1535E+02 BASIN STORAGE= .2158E-02 PERCENT ERROR= .1

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN .55 1.42 5.00 75.13 775.00 5.53

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HYDROGRAPH AT STATION N19

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
75.	12.92	25.	8.	5.	5.
		(INCHES) 4.473	5.526	5.526	5.526
		(AC-FT) 12.	15.	15.	15.

CUMULATIVE AREA = .05 SQ MI

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 * *
 490 KK * N18 *
 * *

RUNOFF AREA N18

492 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

493 BA SUBBASIN CHARACTERISTICS
 TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
 HYDRO-35 TP-40 TP-49
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
 .74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00
 STORM AREA = .01

494 LS SCS LOSS RATE
 STRTL .38 INITIAL ABSTRACTION
 CRVNBR 84.00 CURVE NUMBER
 RTIMP .00 PERCENT IMPERVIOUS AREA

495 UK KINEMATIC WAVE
 OVERLAND-FLOW ELEMENT NO. 1
 L 41. OVERLAND FLOW LENGTH
 S .3300 SLOPE
 N .350 ROUGHNESS COEFFICIENT
 PA 100.0 PERCENT OF SUBBASIN
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

496 RD MUSKINGUM-CUNGE
 MAIN CHANNEL
 L 1123. CHANNEL LENGTH
 S .0016 SLOPE
 N .030 CHANNEL ROUGHNESS COEFFICIENT
 CA .01 CONTRIBUTING AREA
 SHAPE TRAP CHANNEL SHAPE
 WD 15.00 BOTTOM WIDTH OR DIAMETER
 Z 3.00 SIDE SLOPE
 RUPSTQ YES ROUTE UPSTREAM HYDROGRAPH

 COMPUTED MUSKINGUM-CUNGE PARAMETERS

ELEMENT	ALPHA	COMPUTATION TIME STEP			PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
		M	DT (MIN)	DX (FT)				
PLANE1	2.45	1.67	.35	8.24	32.11	724.67	.43	
MAIN	.45	1.45	5.00	561.70	77.82	780.00	2.63	

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1535E+02 EXCESS= .1897E+01 OUTFLOW= .1723E+02 BASIN STORAGE= .2334E-02 PERCENT ERROR= .1

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN .45 1.45 5.00 77.82 780.00 5.52

*** **

HYDROGRAPH AT STATION N18

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	34.58-HR	
78.	13.00	28.	9.	6.	6.	
		(INCHES)	4.470	5.523	5.523	5.523
		(AC-FT)	14.	17.	17.	17.

CUMULATIVE AREA = .06 SQ MI

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 * *
 497 KK * 05 *
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OFFSITE AREA 05

499 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE
 IPNCH 7 PUNCH COMPUTED HYDROGRAPH
 IOUPT 21 SAVE HYDROGRAPH ON THIS UNIT
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
 ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
 TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

500 BA SUBBASIN CHARACTERISTICS
TAREA .18 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
..... HYDRO-35 TP-40 TP-49
5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
.74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .18

501 LS SCS LOSS RATE
STRTL .38 INITIAL ABSTRACTION
CRVNBR 84.00 CURVE NUMBER
RTIMP .00 PERCENT IMPERVIOUS AREA

502 US SNYDER UNITGRAPH
TP .59 LAG
CP .64 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS

CLARK TC= .67 HR, R= .52 HR
SNYDER TP= .59 HR, CP= .64

UNIT HYDROGRAPH

38 END-OF-PERIOD ORDINATES

7.	24.	48.	74.	100.	119.	129.	116.	99.
84.	72.	61.	52.	44.	38.	32.	27.	20.
17.	14.	12.	10.	9.	7.	6.	5.	4.
3.	3.	2.	2.	2.	1.	1.		

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HYDROGRAPH AT STATION O5

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	34.58-HR
302.	12.67	88.	27.	19.	19.
		(INCHES) 4.481	5.533	5.533	5.533
		(AC-FT) 43.	54.	54.	54.

CUMULATIVE AREA = .18 SQ MI

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503 KK * S1 *
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RUNOFF AREA S1

505 KO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLST 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE
IPNCH 7 PUNCH COMPUTED HYDROGRAPH
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED
ISAV2 416 LAST ORDINATE PUNCHED OR SAVED
TIMINT .083 TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

506 BA SUBBASIN CHARACTERISTICS
TAREA .02 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM
..... HYDRO-35 TP-40 TP-49
5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY
.74 1.57 3.19 4.18 4.52 5.47 6.43 7.44 .00 .00 .00 .00

STORM AREA = .02

507 LS SCS LOSS RATE
STRTL .38 INITIAL ABSTRACTION
CRVNBR 84.00 CURVE NUMBER

RTIMP .00 PERCENT IMPERVIOUS AREA
 508 US SNYDER UNITGRAPH
 TP .75 LAG
 CP .70 PEAKING COEFFICIENT
 SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS
 CLARK TC= .86 HR, R= .56 HR
 SNYDER TP= .75 HR, CP= .69

UNIT HYDROGRAPH
 42 END-OF-PERIOD ORDINATES

0.	1.	3.	4.	6.	8.	9.	10.	10.	10.
9.	8.	7.	6.	5.	4.	4.	3.	3.	2.
2.	2.	2.	1.	1.	1.	1.	1.	1.	1.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.								

HYDROGRAPH AT STATION S1

TOTAL RAINFALL = 7.44, TOTAL LOSS = 1.88, TOTAL EXCESS = 5.56

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	(CFS)	6-HR	24-HR	72-HR	34.58-HR
25.	12.75	8.	8.	2.	2.	2.
		{INCHES}	4.479	5.534	5.534	5.534
		{AC-FT}	4.	5.	5.	5.

CUMULATIVE AREA = .02 SQ MI

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 509 KK * N17 *
 * *

RUNOFF AREA N17

511 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

SUBBASIN RUNOFF DATA

512 BA SUBBASIN CHARACTERISTICS
 TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

11 PH DEPTHS FOR 4-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40				TP-49				
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.74	1.57	3.19	4.18	4.52	5.47	6.43	7.44	.00	.00	.00	.00

STORM AREA = .01

513 LS SCS LOSS RATE

STRTL	.38	INITIAL ABSTRACTION
CRVNR	84.00	CURVE NUMBER
RTIMP	.00	PERCENT IMPERVIOUS AREA

514 US SNYDER UNITGRAPH
 TP .12 LAG
 CP .64 PEAKING COEFFICIENT

SYNTHETIC ACCUMULATED-AREA VS. TIME CURVE WILL BE USED

UNIT HYDROGRAPH PARAMETERS
 CLARK TC= .14 HR, R= .09 HR
 SNYDER TP= .12 HR, CP= .64

UNIT HYDROGRAPH
7 END-OF-PERIOD ORDINATES

	11.	21.	13.	5.	2.	1.	0.
***	***	***	***	***	***	***	***
HYDROGRAPH AT STATION N17							
TOTAL RAINFALL =	7.44,	TOTAL LOSS =	1.88,	TOTAL EXCESS =	5.56		
PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW					
(CFS)	(HR)	6-HR	24-HR	72-HR	34.58-HR		
+	24.	12.17					
		(CFS)	3.	1.	1.	1.	
		(INCHES)	4.508	5.545	5.545	5.545	
		(AC-FT)	2.	2.	2.	2.	
CUMULATIVE AREA = .01 SQ MI							

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515 KK * C107 *
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COMBINE AREAS S1, O6, AND N17-19

517 KO OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNGH	7	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	416	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

518 HC HYDROGRAPH COMBINATION
ICOMP 4 NUMBER OF HYDROGRAPHS TO COMBINE

	***	***	***	***	***		
HYDROGRAPH AT STATION C107							
PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW					
(CFS)	(HR)	6-HR	24-HR	72-HR	34.58-HR		
+	395.	12.67					
		(CFS)	127.	39.	27.	27.	
		(INCHES)	4.476	5.531	5.531	5.531	
		(AC-FT)	63.	78.	78.	78.	
CUMULATIVE AREA = .26 SQ MI							

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RUNOFF SUMMARY
FLOW IN CUBIC FEET PER SECOND
TIME IN HOURS, AREA IN SQUARE MILES

	OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
					6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT	O1	298.	12.42	70.	22.	15.	.14		
+	HYDROGRAPH AT	O1A	70.	12.58	18.	6.	4.	.04		
+	HYDROGRAPH AT	O2	2171.	12.75	767.	239.	166.	1.58		
+	HYDROGRAPH AT	S4	113.	13.00	43.	13.	9.	.09		
+	3 COMBINED AT	CS4	2337.	12.75	828.	258.	179.	1.70		
+	HYDROGRAPH AT	N1	39.	12.42	9.	3.	2.	.02		
+	HYDROGRAPH AT	O3	62.	12.33	12.	4.	3.	.03		

+	3 COMBINED AT	C1MWY	2396.	12.75	848.	264.	183.	1.74		
+	HYDROGRAPH AT	S3	45.	12.83	15.	5.	3.	.03		
+	HYDROGRAPH AT	N20	47.	13.00	17.	5.	4.	.04		
+	2 COMBINED AT	C2MWY	2437.	12.75	865.	269.	187.	1.78		
+	HYDROGRAPH AT	N11T	12.	12.25	2.	1.	0.	.00		
+	HYDROGRAPH AT	N11S	32.	12.08	3.	1.	1.	.01		
+	2 COMBINED AT	CN11	41.	12.08	6.	2.	1.	.01		
+	HYDROGRAPH AT	CH11	40.	12.25	8.	2.	2.	.02		
+	HYDROGRAPH AT	N2T	31.	12.25	7.	2.	1.	.01		
+	HYDROGRAPH AT	N2S	24.	12.08	2.	1.	1.	.00		
+	2 COMBINED AT	CN2	47.	12.08	9.	3.	2.	.02		
+	2 COMBINED AT	CCH2	82.	12.17	17.	5.	4.	.04		
+	HYDROGRAPH AT	CH2	84.	12.25	18.	6.	4.	.04		
+	HYDROGRAPH AT	N12	28.	12.42	6.	2.	1.	.01		
+	HYDROGRAPH AT	N3T	122.	12.25	25.	7.	5.	.05		
+	HYDROGRAPH AT	N3S	26.	12.08	3.	1.	1.	.01		
+	3 COMBINED AT	CN3	156.	12.25	33.	10.	7.	.07		
+	2 COMBINED AT	CCH3	240.	12.25	51.	15.	11.	.11		
+	HYDROGRAPH AT	CH3	237.	12.33	53.	16.	11.	.11		
+	HYDROGRAPH AT	N4T	23.	12.33	6.	2.	1.	.01		
+	HYDROGRAPH AT	N4S	34.	12.08	4.	1.	1.	.01		
+	2 COMBINED AT	CN4	50.	12.08	9.	3.	2.	.02		
+	HYDROGRAPH AT	CH4	62.	12.17	12.	4.	3.	.02		
+	2 COMBINED AT	C1CH4A	288.	12.25	65.	20.	14.	.14		
+	HYDROGRAPH AT	CH4A	286.	12.25	66.	20.	14.	.14		
+	HYDROGRAPH AT	N13	55.	12.58	14.	4.	3.	.03		
+	HYDROGRAPH AT	W1	67.	12.08	8.	3.	2.	.01		
+	3 COMBINED AT	PND1IN	352.	12.25	87.	27.	19.	.18		
+	ROUTED TO	PND1OU	229.	12.75	202.	198.	197.	.18	456.04	12.75
+	HYDROGRAPH AT	N16	12.	12.25	2.	1.	0.	.00		
+	HYDROGRAPH AT	CHW1	13.	12.33	3.	1.	1.	.01		

+	3 COMBINED AT	MIDRD	2673.	12.75	1070.	468.	385.	1.97
	HYDROGRAPH AT							
+		S5	3.	12.25	0.	0.	0.	.00
+	2 COMBINED AT	CS5	2674.	12.75	1070.	468.	385.	1.97
	HYDROGRAPH AT							
+		O4	269.	12.50	65.	20.	14.	.13
+	2 COMBINED AT	C4MWY	2887.	12.75	1135.	488.	399.	2.10
	HYDROGRAPH AT							
+		N10T	37.	12.42	9.	3.	2.	.02
	HYDROGRAPH AT							
+		N10S	55.	12.08	6.	2.	1.	.01
+	2 COMBINED AT	CN10	78.	12.08	15.	5.	3.	.03
	HYDROGRAPH AT							
+		CH10	115.	12.17	21.	6.	5.	.04
+	2 COMBINED AT	CABELM	2933.	12.75	1156.	494.	403.	2.14
	HYDROGRAPH AT							
+		N9T	40.	12.33	9.	3.	2.	.02
	HYDROGRAPH AT							
+		N9S	73.	12.08	7.	2.	2.	.01
+	2 COMBINED AT	CN9	99.	12.08	16.	5.	3.	.03
	HYDROGRAPH AT							
+		CH9	84.	12.25	18.	6.	4.	.04
	HYDROGRAPH AT							
+		N5T	50.	12.58	15.	5.	3.	.03
	HYDROGRAPH AT							
+		N5S	32.	12.08	4.	1.	1.	.01
+	2 COMBINED AT	CN5	63.	12.08	18.	6.	4.	.04
	HYDROGRAPH AT							
+		CH5	66.	12.33	21.	6.	5.	.04
	HYDROGRAPH AT							
+		N6T	20.	12.25	4.	1.	1.	.01
	HYDROGRAPH AT							
+		N6S	30.	12.08	3.	1.	1.	.01
+	2 COMBINED AT	CN6	44.	12.08	7.	2.	2.	.02
+	2 COMBINED AT	CCH6	100.	12.17	28.	9.	6.	.06
	HYDROGRAPH AT							
+		CH6	102.	12.33	30.	9.	7.	.06
	HYDROGRAPH AT							
+		N7AT	42.	12.33	9.	3.	2.	.02
	HYDROGRAPH AT							
+		N7AS	33.	12.08	3.	1.	1.	.01
+	2 COMBINED AT	CN7A	61.	12.08	12.	4.	3.	.03
+	2 COMBINED AT	CCH7A	153.	12.33	43.	13.	9.	.09
	HYDROGRAPH AT							
+		CH7A	153.	12.42	44.	14.	10.	.09
	HYDROGRAPH AT							
+		N7BT	19.	12.33	4.	1.	1.	.01
	HYDROGRAPH AT							
+		N7BS	26.	12.08	3.	1.	1.	.01
+	2 COMBINED AT	CN7B	39.	12.08	7.	2.	1.	.01

+	2 COMBINED AT	CCH7B	178.	12.33	51.	16.	11.	.11		
	HYDROGRAPH AT									
+	HYDROGRAPH AT	CH7B	179.	12.42	53.	17.	11.	.11		
	HYDROGRAPH AT									
+	HYDROGRAPH AT	N8T	58.	12.33	12.	4.	3.	.03		
	HYDROGRAPH AT									
+	HYDROGRAPH AT	N8S	77.	12.08	8.	2.	2.	.02		
	2 COMBINED AT									
+	2 COMBINED AT	CN8	116.	12.08	20.	6.	4.	.04		
	3 COMBINED AT									
+	3 COMBINED AT	C2W2	334.	12.33	92.	29.	20.	.19		
	HYDROGRAPH AT									
+	HYDROGRAPH AT	W2	79.	12.08	9.	3.	2.	.02		
	2 COMBINED AT									
+	2 COMBINED AT	PND2IN	366.	12.25	101.	31.	22.	.21		
	ROUTED TO									
+	ROUTED TO	PD2OUT	201.	13.00	88.	26.	18.	.21	457.26	13.00
	HYDROGRAPH AT									
+	HYDROGRAPH AT	N14	88.	12.42	20.	6.	4.	.04		
	HYDROGRAPH AT									
+	HYDROGRAPH AT	N15	61.	12.50	15.	5.	3.	.03		
	3 COMBINED AT									
+	3 COMBINED AT	C1N14	325.	12.58	120.	37.	25.	.28		
	HYDROGRAPH AT									
+	HYDROGRAPH AT	S2	75.	12.75	24.	7.	5.	.05		
	HYDROGRAPH AT									
+	HYDROGRAPH AT	N19	75.	12.92	25.	8.	5.	.05		
	HYDROGRAPH AT									
+	HYDROGRAPH AT	N18	78.	13.00	28.	9.	6.	.06		
	HYDROGRAPH AT									
+	HYDROGRAPH AT	O5	302.	12.67	88.	27.	19.	.18		
	HYDROGRAPH AT									
+	HYDROGRAPH AT	S1	25.	12.75	8.	2.	2.	.02		
	HYDROGRAPH AT									
+	HYDROGRAPH AT	N17	24.	12.17	3.	1.	1.	.01		
	4 COMBINED AT									
+	4 COMBINED AT	C107	395.	12.67	127.	39.	27.	.26		
1										

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	INTERPOLATED TO COMPUTATION INTERVAL			
						DT	PEAK	TIME TO PEAK	VOLUME
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
N20	MANE	5.00	46.52	780.00	5.53	5.00	46.52	780.00	5.53
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9325E+01 EXCESS= .1215E+01 OUTFLOW= .1052E+02 BASIN STORAGE= .2178E-02 PERCENT ERROR= .1									
N11T	MANE	3.26	11.91	733.23	5.53	5.00	11.86	735.00	5.53
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .1393E+01 OUTFLOW= .1385E+01 BASIN STORAGE= .1876E-02 PERCENT ERROR= .4									
N11S	MANE	3.12	34.59	724.20	5.65	5.00	32.23	725.00	5.64
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2130E+01 OUTFLOW= .2077E+01 BASIN STORAGE= .4285E-03 PERCENT ERROR= 2.5									
CH11	MANE	5.00	40.46	735.00	5.42	5.00	40.46	735.00	5.42
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3461E+01 EXCESS= .1364E+01 OUTFLOW= .4683E+01 BASIN STORAGE= .2406E-02 PERCENT ERROR= 2.9									
N2T	MANE	3.86	31.70	737.41	5.49	5.00	31.34	735.00	5.49

CONTINUITY SUMMARY (AC-FT) - INFLOW=	.0000E+00	EXCESS=	.4180E+01	OUTFLOW=	.4128E+01	BASIN STORAGE=	.7392E-02	PERCENT ERROR=	1.1
N2S MANE	1.54	24.45	723.94	5.68	5.00	23.72	725.00	5.69	
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.0000E+00	EXCESS=	.1513E+01	OUTFLOW=	.1483E+01	BASIN STORAGE=	.2001E-03	PERCENT ERROR=	2.0
CH2 MANE	3.94	84.60	733.28	5.48	5.00	84.05	735.00	5.48	
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.1030E+02	EXCESS=	.7115E+00	OUTFLOW=	.1099E+02	BASIN STORAGE=	.1160E-02	PERCENT ERROR=	.2
N3T MANE	2.95	122.61	737.11	5.07	5.00	122.18	735.00	5.07	
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.0000E+00	EXCESS=	.1574E+02	OUTFLOW=	.1436E+02	BASIN STORAGE=	.2430E-01	PERCENT ERROR=	8.6
N3S MANE	3.63	25.94	725.04	5.73	5.00	25.88	725.00	5.78	
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.0000E+00	EXCESS=	.1667E+01	OUTFLOW=	.1650E+01	BASIN STORAGE=	.4547E-03	PERCENT ERROR=	1.0
CH3 MANE	3.74	238.09	737.52	5.30	5.00	237.19	740.00	5.30	
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.3069E+02	EXCESS=	.1097E+01	OUTFLOW=	.3170E+02	BASIN STORAGE=	.3574E-02	PERCENT ERROR=	.2
N4T MANE	2.52	22.88	740.50	5.47	5.00	22.84	740.00	5.47	
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.0000E+00	EXCESS=	.3439E+01	OUTFLOW=	.3387E+01	BASIN STORAGE=	.8891E-02	PERCENT ERROR=	1.3
N4S MANE	3.62	35.90	723.22	5.68	5.00	33.64	725.00	5.65	
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.0000E+00	EXCESS=	.2439E+01	OUTFLOW=	.2392E+01	BASIN STORAGE=	.5147E-03	PERCENT ERROR=	1.9
CH4 MANE	5.00	62.27	730.00	5.53	5.00	62.27	730.00	5.53	
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.5767E+01	EXCESS=	.1453E+01	OUTFLOW=	.7200E+01	BASIN STORAGE=	.1358E-02	PERCENT ERROR=	.3
CH4A MANE	1.73	287.49	737.40	5.34	5.00	286.30	735.00	5.34	
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.3891E+02	EXCESS=	.3261E+00	OUTFLOW=	.3920E+02	BASIN STORAGE=	.2158E-02	PERCENT ERROR=	.1
CHW1 MANE	5.00	13.02	740.00	5.49	5.00	13.02	740.00	5.49	
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.1240E+01	EXCESS=	.4150E+00	OUTFLOW=	.1639E+01	BASIN STORAGE=	.1476E-02	PERCENT ERROR=	.9
N10T MANE	1.23	36.95	741.58	5.53	5.00	36.82	745.00	5.55	
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.0000E+00	EXCESS=	.5514E+01	OUTFLOW=	.5490E+01	BASIN STORAGE=	.1379E-01	PERCENT ERROR=	.2
N10S MANE	.62	55.67	725.10	5.79	5.00	55.40	725.00	5.79	
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.0000E+00	EXCESS=	.3551E+01	OUTFLOW=	.3550E+01	BASIN STORAGE=	.1045E-03	PERCENT ERROR=	.0
CH10 MANE	3.89	120.07	728.17	5.59	5.00	114.78	730.00	5.59	
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.9055E+01	EXCESS=	.3884E+01	OUTFLOW=	.1288E+02	BASIN STORAGE=	.2546E-02	PERCENT ERROR=	.4
N9T MANE	1.05	39.81	739.00	5.54	5.00	39.58	740.00	5.54	
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.0000E+00	EXCESS=	.5247E+01	OUTFLOW=	.5229E+01	BASIN STORAGE=	.8873E-02	PERCENT ERROR=	.2
N9S MANE	.57	73.17	725.45	5.79	5.00	72.83	725.00	5.80	
CONTINUITY SUMMARY (AC-FT) - INFLOW=	.0000E+00	EXCESS=	.4570E+01	OUTFLOW=	.4568E+01	BASIN STORAGE=	.1143E-03	PERCENT ERROR=	.0

CH9	MANE	5.00	83.50	735.00	5.58	5.00	83.50	735.00	5.58
CONTINUITY SUMMARY (AC-FT) - INFLOW= .9806E+01 EXCESS= .1601E+01 OUTFLOW= .1129E+02 BASIN STORAGE= .4162E-02 PERCENT ERROR= 1.0									
N5T	MANE	.30	50.41	754.37	5.52	5.00	50.41	755.00	5.51
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .9338E+01 OUTFLOW= .9275E+01 BASIN STORAGE= .4378E-01 PERCENT ERROR= .2									
N5S	MANE	.73	32.50	726.07	5.79	5.00	31.52	725.00	5.79
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2161E+01 OUTFLOW= .2161E+01 BASIN STORAGE= .1163E-03 PERCENT ERROR= .0									
CH5	MANE	5.00	66.15	740.00	5.54	5.00	66.15	740.00	5.54
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1142E+02 EXCESS= .1512E+01 OUTFLOW= .1288E+02 BASIN STORAGE= .8477E-02 PERCENT ERROR= .4									
N6T	MANE	1.02	20.70	737.48	5.54	5.00	20.47	735.00	5.53
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2550E+01 OUTFLOW= .2541E+01 BASIN STORAGE= .3798E-02 PERCENT ERROR= .2									
N6S	MANE	.91	30.94	725.80	5.79	5.00	30.36	725.00	5.80
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .1976E+01 OUTFLOW= .1976E+01 BASIN STORAGE= .4982E-04 PERCENT ERROR= .0									
CH6	MANE	5.00	101.78	740.00	5.54	5.00	101.78	740.00	5.54
CONTINUITY SUMMARY (AC-FT) - INFLOW= .1739E+02 EXCESS= .1364E+01 OUTFLOW= .1868E+02 BASIN STORAGE= .1235E-01 PERCENT ERROR= .4									
N7AT	MANE	.75	41.97	738.16	5.54	5.00	41.55	740.00	5.48
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .5603E+01 OUTFLOW= .5580E+01 BASIN STORAGE= .9999E-02 PERCENT ERROR= .2									
N7AS	MANE	.46	33.53	725.11	5.79	5.00	33.45	725.00	5.80
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2100E+01 OUTFLOW= .2098E+01 BASIN STORAGE= .5111E-04 PERCENT ERROR= .0									
CH7A	MANE	5.00	153.03	745.00	5.53	5.00	153.03	745.00	5.53
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2630E+02 EXCESS= .1067E+01 OUTFLOW= .2726E+02 BASIN STORAGE= .1321E-01 PERCENT ERROR= .4									
N7BT	MANE	.87	19.17	738.52	5.54	5.00	18.96	740.00	5.51
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2520E+01 OUTFLOW= .2511E+01 BASIN STORAGE= .4450E-02 PERCENT ERROR= .2									
N7BS	MANE	.46	26.06	725.03	5.79	5.00	26.03	725.00	5.80
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .1606E+01 OUTFLOW= .1605E+01 BASIN STORAGE= .3639E-04 PERCENT ERROR= .0									
CH7B	MANE	5.00	178.99	745.00	5.50	5.00	178.99	745.00	5.50
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3137E+02 EXCESS= .1690E+01 OUTFLOW= .3283E+02 BASIN STORAGE= .1812E-01 PERCENT ERROR= .6									
N8T	MANE	1.03	58.33	737.03	5.54	5.00	58.04	740.00	5.53
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .7648E+01 OUTFLOW= .7622E+01 BASIN STORAGE= .1297E-01 PERCENT ERROR= .2									
N8S	MANE	.67	78.07	725.64	5.79	5.00	77.49	725.00	5.80
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .4940E+01 OUTFLOW= .4939E+01 BASIN STORAGE= .1245E-03 PERCENT ERROR= .0									
N19	MANE	5.00	75.13	775.00	5.53	5.00	75.13	775.00	5.53

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1454E+02 EXCESS= .8301E+00 OUTFLOW= .1535E+02 BASIN STORAGE= .2158E-02 PERCENT ERROR= .1

N18	MANE	5.00	77.82	780.00	5.52	5.00	77.82	780.00	5.52
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CONTINUITY SUMMARY (AC-FT) - INFLOW= .1535E+02 EXCESS= .1897E+01 OUTFLOW= .1723E+02 BASIN STORAGE= .2334E-02 PERCENT ERROR= .1

*** NORMAL END OF HEC-1 ***

VOLUME CALCULATIONS

EXCESS RAINFALL VOLUME CALCULATION

The volume generated by the site and the surrounding properties is calculated for the 25-year storm event. A summary of the design information that is included in this Appendix and related appendices are listed below.

- Excess rainfall and drainage areas used in the volume calculations were taken from the HEC-1 analysis located on pages IIIF-E-20 through IIIF-E-109.
- Updated permitted condition volume information is summarized on pages IIIF-E-112 through IIIF-E-114.

CAMELOT LANDFILL
1339-351-11-02-01
25-YEAR EXCESS RAINFALL
VOLUME CALCULATIONS

Required: Determine the 25-year 24-hour storm volume generated by the site and offsite areas using the excess rainfall calculated in the HEC-1 analysis of the permitted site conditions.

Method: 1. Use the excessive rainfall data generated by the HEC-1 analysis (pages IIF-E-20 through IIF-E-108) to determine the volume produced by the site for the permitted conditions.

Updated Permitted Conditions

1. Volume Discharging Southeast Downstream of Entrance Road

1a. Volume Upstream of Entrance Road

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
O1	0.1367	5.90	87.47	43
O1A	0.0366	5.67	23.42	11
O2	1.5754	5.66	1,008.23	476
S4	0.0897	5.56	57.41	27
Total Volume Upstream of Entrance Road				556

1b. Non-Landfill Areas Downstream of Entrance Road

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
N1	0.0176	5.56	11.26	5
O3	0.0253	5.56	16.18	7
S3	0.0316	5.56	20.21	9
N20	0.0041	5.56	2.62	1
Total Volume of Non-Landfill Areas D.S. of Entrance Road				23

1c. Landfill Areas Discharging into Pond W1 and Flowing under Entrance Road

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
N11T	0.0047	5.56	3.03	1
N11S	0.0069	5.79	4.40	2
CH11	0.0046	5.56	2.97	1
N2T	0.0141	5.56	9.05	4
N2S	0.0049	5.79	3.16	2
CH2	0.0024	5.56	1.56	1
N12	0.0124	5.56	7.96	4
N3T	0.0531	5.56	34.01	16
N3S	0.0054	5.79	3.47	2
CH3	0.0037	5.56	2.39	1
N4T	0.0116	5.56	7.45	3
N4S	0.0079	5.79	5.05	2
CH4	0.0049	5.56	3.11	1
CH4A	0.0011	5.56	0.68	0
N13	0.0293	5.56	18.73	9
W1	0.0130	7.44	8.30	5
N16	0.0043	5.56	2.72	1
CHW1	0.0014	5.56	0.89	0
S5	0.0010	5.56	0.67	0
Total Volume Flowing under Entrance Road				57

Total Volume Discharging Southeast Downstream
of Entrance Road = **637** ac-ft

CAMELOT LANDFILL
1339-351-11-02-01
25-YEAR EXCESS RAINFALL
VOLUME CALCULATIONS

2. Volume in Midway Branch Exiting Permit Boundary

2a. Volume in Midway Branch Entering Permit Boundary

Offsite Area Entering Midway Branch	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
O4	0.1344	5.56	86.04	40
Total Volume in Midway Branch Entering Permit Boundary				40

2b. Landfill Areas Flowing East into Midway Branch

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
N10T	0.0186	5.56	11.93	6
N10S	0.0115	5.79	7.39	4
CH10	0.0131	5.56	8.41	4
Total Volume Flowing East into Midway Branch				13

Total Volume in Midway Branch Excluding Section
1 Discharge Volume = **53** ac-ft

Total Volume in Midway Branch Exiting Permit
Boundary = **689** ac-ft

3. Volume Discharging South into Elm Fork

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
N9T	0.0177	5.56	11.35	5
N9S	0.0148	5.79	9.50	5
CH9	0.0054	5.56	3.48	2
N5T	0.0315	5.56	20.18	9
N5S	0.0070	5.79	4.50	2
CH5	0.0051	5.56	3.26	2
N6T	0.0086	5.56	5.48	3
N6S	0.0064	5.79	4.10	2
CH6	0.0046	5.56	2.95	1
N7AT	0.0189	5.56	12.08	6
N7AS	0.0068	5.79	4.36	2
CH7A	0.0036	5.56	2.30	1
N7BT	0.0085	5.56	5.45	3
N7BS	0.0052	5.79	3.34	2
CH7B	0.0057	5.56	3.66	2
N8T	0.0258	5.56	16.52	8
N8S	0.0160	5.79	10.27	5
W2	0.0154	7.44	9.83	6
Total Volume Discharging South into Elm Fork				64

4. Volume Discharging Southeast into Elm Fork

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
N15	0.0311	5.56	19.93	9
Total Volume Discharging Southeast into Elm Fork				9

5. Volume Discharging Southwest into Elm Fork

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
N14	0.0407	5.56	26.06	12
Total Volume Discharging Southwest into Elm Fork				12

6. Southern Volume Discharging Southwest Towards Elm Fork

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
N17	0.0068	5.56	4.32	2
Total Southern Volume Discharging Southwest Towards Elm Fork				2

7. Northern Volume Discharging West Towards Elm Fork

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
S2	0.0493	5.56	31.53	15
N19	0.0028	5.56	1.82	1
N18	0.0064	5.56	4.12	2
Total Northern Volume Discharging West Towards Elm Fork				17

8. Volume Discharging from Northwest Corner Towards Elm Fork

Area No.	Area (sq mi)	Total Excess Rainfall (in)	Area (ac)	Volume (ac-ft)
S1	0.0163	5.56	10.40	5
Total Volume Discharging from NW Corner Towards Elm Fork				5

Total Volume Exiting Permit Boundary = 799 ac-ft

VELOCITY CALCULATIONS

Required: Determine the flow velocities entering and exiting the permit boundary using HYDROCALC HYDRAULICS (Version 1.2a, 1996) for the flows calculated for the 25-year storm event in the HEC-1 analysis. HEC-RAS is used to determine the velocity in Elm Fork.

Method:

1. Use the flow data generated by the HEC-1 analysis to determine velocity of runoff entering the landfill permit boundary.
2. Use the flow data generated by the HEC-1 analysis to determine velocity of runoff exiting the landfill permit boundary.

I. Flow Velocity entering the landfill permit boundary

DPI

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$$Q_{25} = 2171 \text{ cfs}$$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	2171	0.010	0.03	4.00	20.00	60.00	2.85	8.08

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

DP2

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$$Q_{25} = 62 \text{ cfs}$$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	62	0.090	0.03	4.00	6.00	87.00	0.16	4.38

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

DP4

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$$Q_{25} = 2887 \text{ cfs}$$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	2887	0.005	0.03	10.00	2.00	22.00	6.00	8.29

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

DPI2

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$$Q_{25} = 298 \text{ cfs}$$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	298	0.001	0.03	77.00	83.00	0.00	1.65	1.38

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

DP13

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$$Q_{25} = 70 \text{ cfs}$$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	70	0.019	0.03	50.00	48.00	0.00	0.66	3.27

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

2. Flow Velocity exiting the landfill permit boundary

DP3

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$$Q_{25} = 2674 \text{ cfs}$$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	2674	0.008	0.03	16.00	17.00	27.00	3.86	7.64

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

DP5

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$$Q_{25} = 2933 \text{ cfs}$$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	2933	0.008	0.03	2.00	2.00	9.00	8.75	12.64

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

DP6

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$$Q_{25} = 201 \text{ cfs}$$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	201	0.030	0.03	1.00	2.00	1.00	3.17	11.00

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

DP7

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$$Q_{25} = 61 \text{ cfs}$$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	61	0.010	0.03	24.00	29.00	0.00	0.89	2.89

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

DP8

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$$Q_{25} = 88 \text{ cfs}$$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	88	0.083	0.03	4.50	5.00	0.00	1.32	10.64

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

DP9

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$$Q_{25} = 24 \text{ cfs}$$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	24	0.089	0.03	99.00	100.00	0.00	0.25	3.76

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

DP10

- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$$Q_{25} = 78 \text{ cfs}$$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	78	0.001	0.03	3.00	3.00	20.00	1.64	1.91

Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

DP11

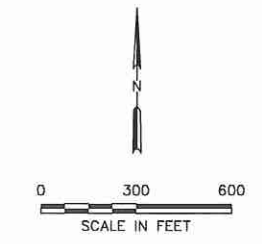
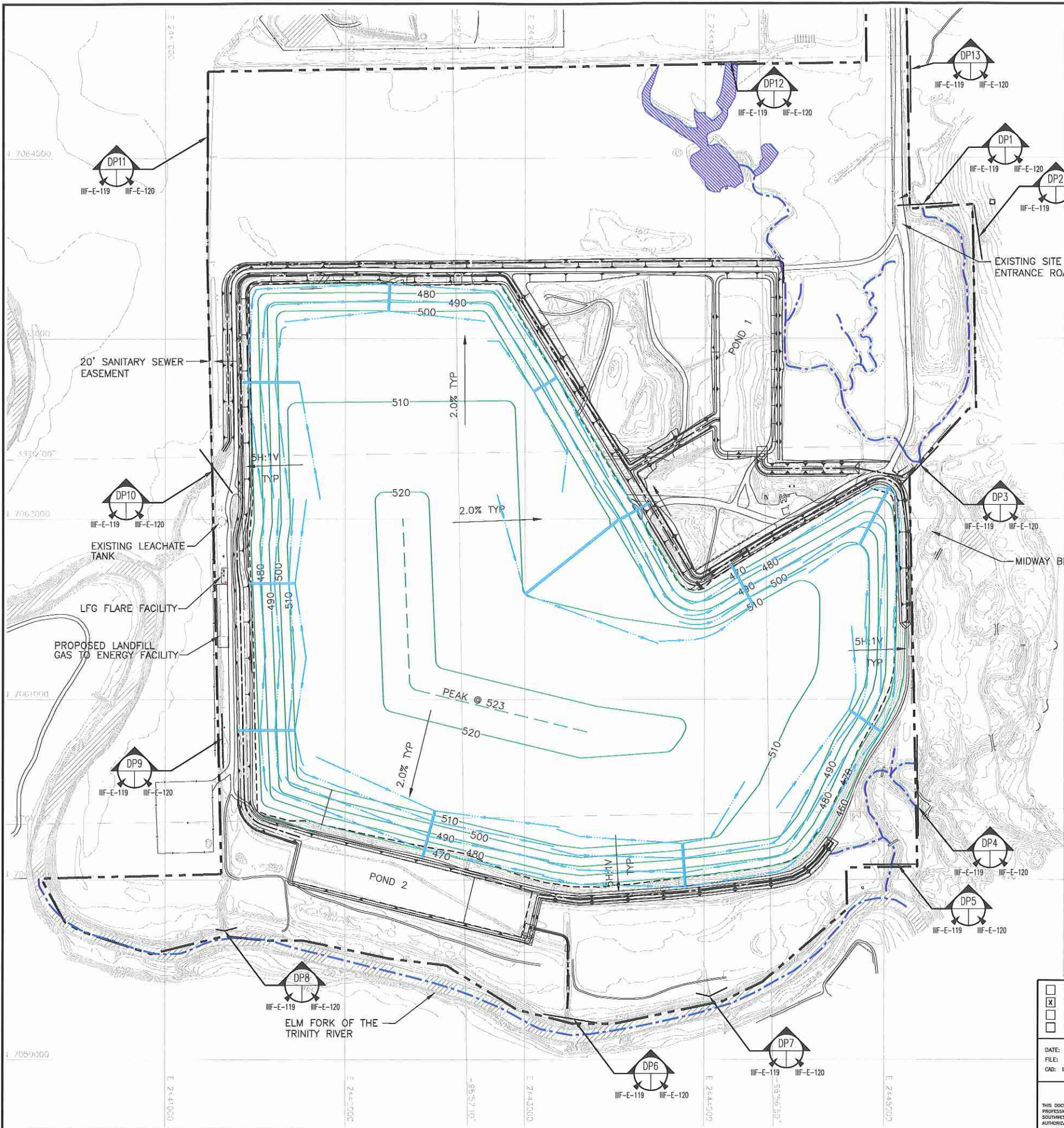
- Flow for the 25-year storm event was obtained from the HEC-1 files included in this Appendix and are summarized below.

$$Q_{25} = 25 \text{ cfs}$$

Storm Year	Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)
25	25	0.001	0.03	100.00	100.00	0.00	0.60	0.70

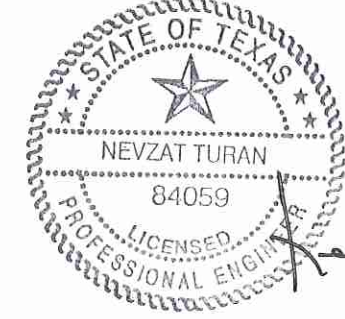
Note: Calculations were performed using the HYDROCALC HYDRAULICS for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

O:\1339\351\EXPANSION 2009\PART III-SDP\III-E\III-B-119 DISCHARGE PT VEL CALC.dwg, Jwilson, 1:2



- LEGEND**
- PERMIT BOUNDARY
 - AUTHORIZED LIMIT OF WASTE
 - STATE PLANE COORDINATE SYSTEM
 - GEODETIC COORDINATE SYSTEM
 - 600 PERMITTED FINAL COVER CONTOUR
 - 500 EXISTING CONTOUR (SEE NOTE 1)
 - PERMITTED DRAINAGE SWALE
 - PERMITTED LETDOWN STRUCTURE
 - USACE SECTION 404 JURISDICTIONAL WATERS OF THE U.S. (SEE NOTE 2)
 - USACE JURISDICTIONAL WETLANDS

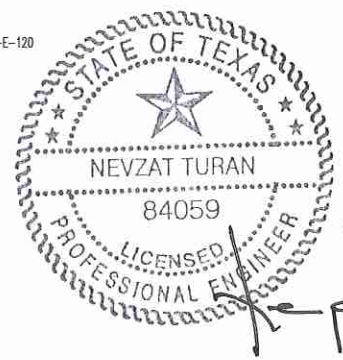
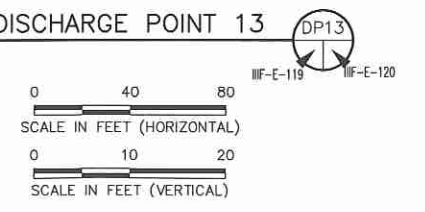
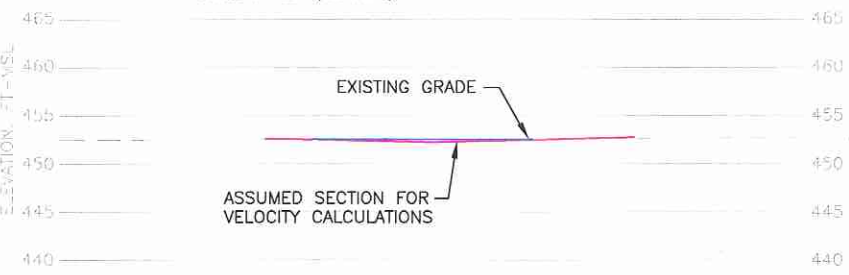
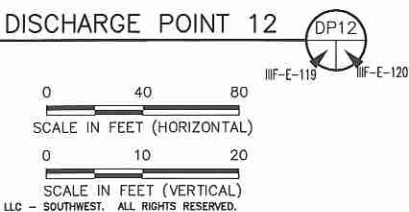
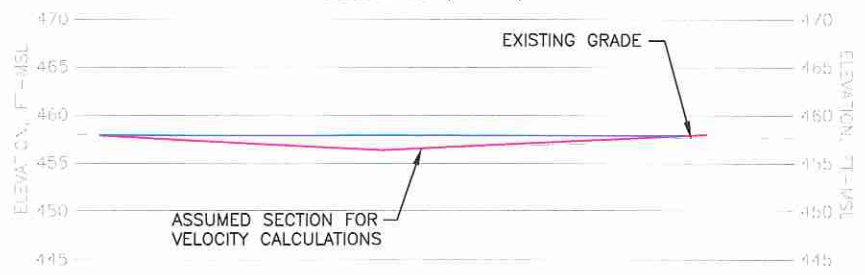
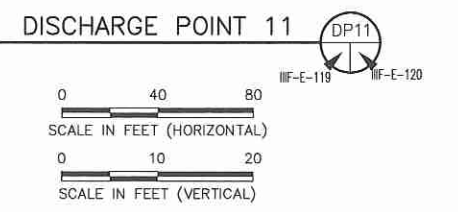
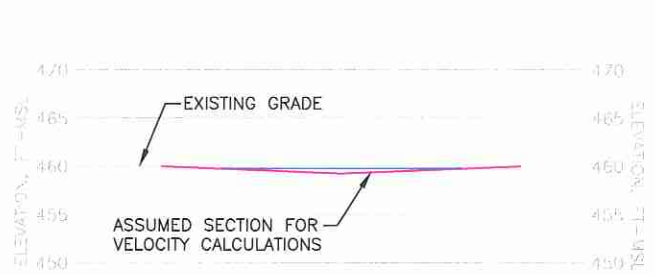
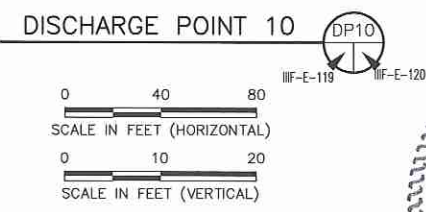
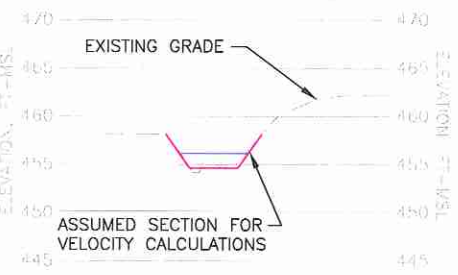
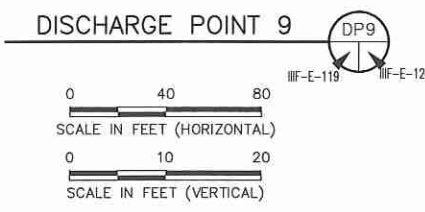
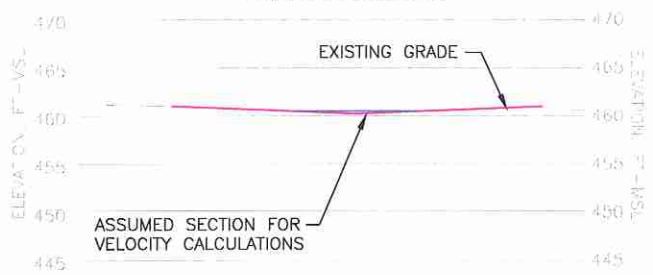
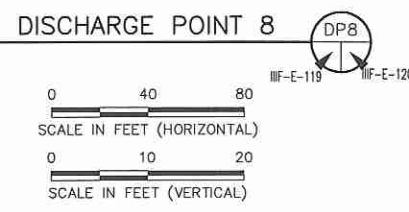
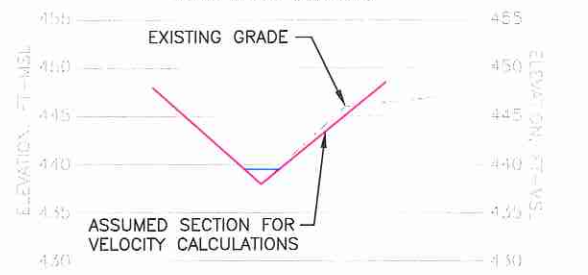
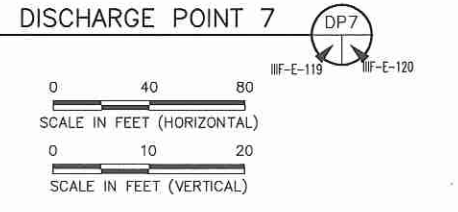
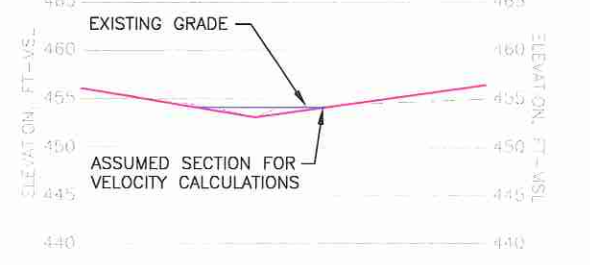
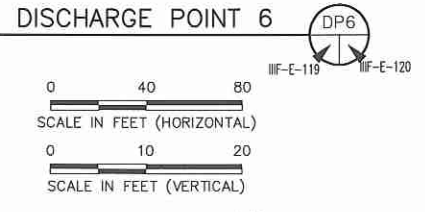
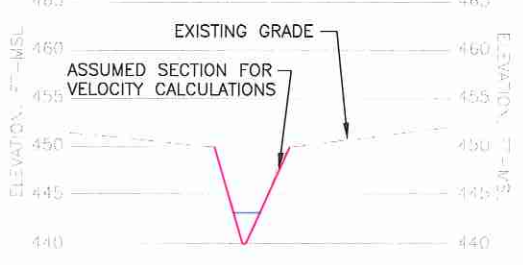
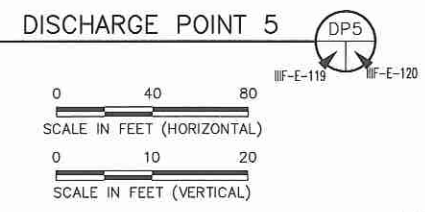
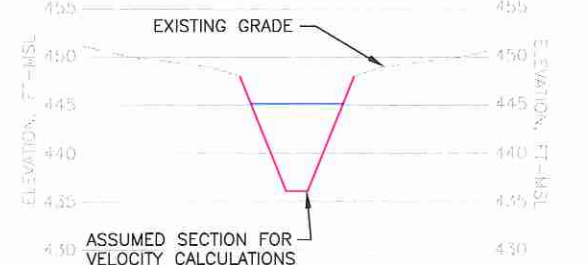
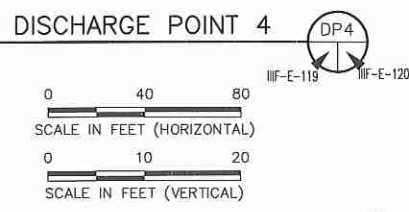
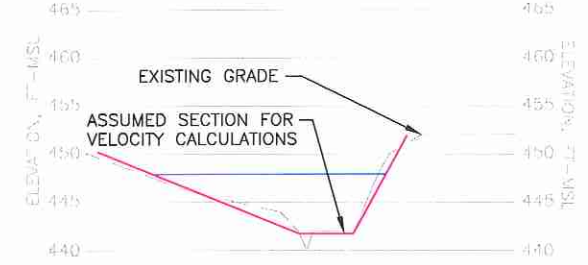
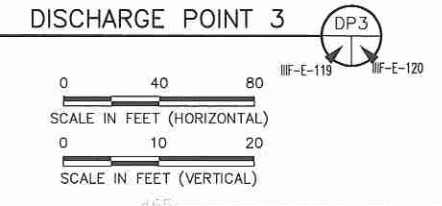
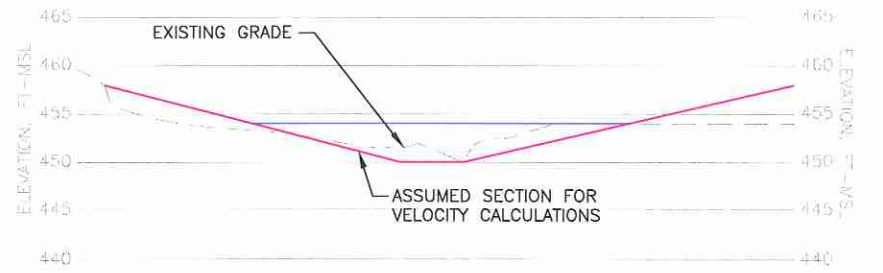
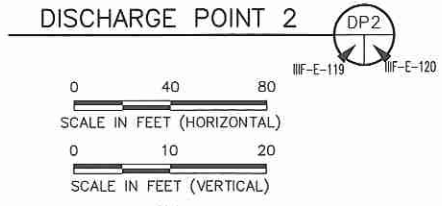
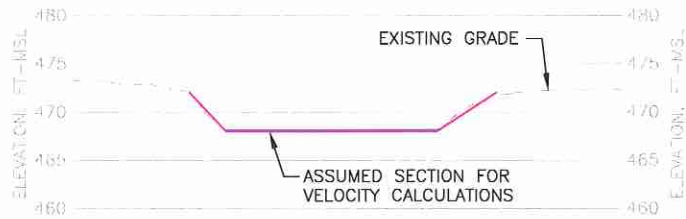
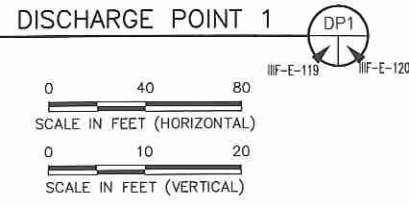
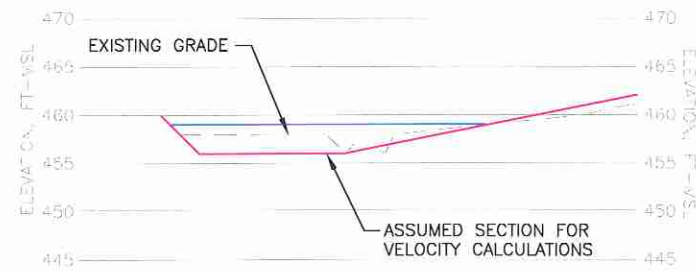
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 3. PERMIT BOUNDARY WAS PREPARED BY PEISER SUREYING CO. IN NOVEMBER 2010.



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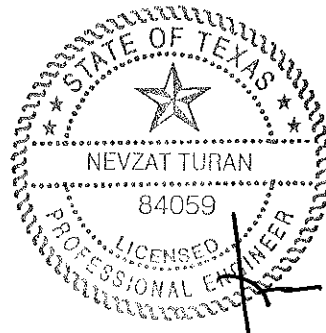


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APPENDIX III-F

**EROSION CONTROL PLAN FOR ALL PHASES
OF LANDFILL OPERATION**



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Includes pages III-F-1 through III-F-14

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APPENDIX III-F-1

Temporary Add-on Swale Design

APPENDIX III-F-2

Temporary Letdown Design

APPENDIX III-F-3

Sediment Control Pond Design



EROSION CONTROL PLAN FOR ALL PHASES OF LANDFILL OPERATION

1.0 Introduction

The purpose of this appendix is to provide an Erosion Control Plan (ECP) to meet the requirements of Title 30 Texas Administrative Code (TAC) Chapter §330.305(d), which are listed below.

“The landfill design must provide effective erosional stability to top dome surfaces and external embankment side slopes during all phases of landfill operation, closure, and post-closure care in accordance with the following.

(1) Estimated peak velocities for top surfaces and external embankment slopes should be less than the permissible non-erodible velocities under similar conditions.

(2) The top surfaces and external embankment slopes of municipal solid waste landfill units must be designed to minimize erosion and soil loss through the use of appropriate side slopes, vegetation, and other structural and nonstructural controls, as necessary. Soil erosion loss (tons/acre) for the top surfaces and external embankment slopes may be calculated using the Soil Conservation Service of the United States Department of Agriculture’s Universal Soil Loss Equation, in which case the potential soil loss should not exceed the permissible soil loss for comparable soil-slope lengths and soil-cover conditions.”

This ECP has also been developed to meet the requirements of the Texas Commission on Environmental Quality (TCEQ) guidance document titled, “Guidance for Addressing Erosional Stability During All Phases of Landfill Operation.” As noted in the above guidance document, landfill cover phases are defined as daily cover, intermediate cover, and final cover. Top dome surfaces and external embankment side slopes are:

- Those above grade slopes that directly drain to the site perimeter stormwater management system (i.e., areas where the stormwater directly flows to a perimeter channel or detention pond designed in accordance with Title 30 TAC §330.63(c), §330.303, and §330.305);
- Above grade slopes that have received intermediate or final cover; and
- Above grade slopes that have either reached their permitted elevation, or will subsequently remain inactive for longer than 180 days. For example, after an above grade slope has reached the permitted elevation and intermediate cover has been placed, the structural erosion control features (e.g., drainage swales, letdown

structures, and/or sedimentation ponds) will be in-place 180 days after intermediate cover has been placed.

Slopes which drain to ongoing waste placement areas, pre-excavated areas, areas that have received only daily cover, and areas under construction which have not received waste are not considered external side slopes.

The ECP for daily cover areas and top dome surfaces and external side slopes that drain directly to the site perimeter stormwater management system, have received intermediate cover, and either reached their permitted configuration or will remain inactive for longer than 180 days are addressed in the following sections. Erosion control measures for final cover areas are addressed in the currently TCEQ-approved Site Development Plan (SDP).

Inspection, maintenance, and recordkeeping requirements are included in the Site Operating Plan (SOP) and discussed in Section 2.4. The word “temporary” is used throughout the ECP to describe any erosion control feature that is not a permanent erosion control feature that is included in the approved Site Development Plan. Additionally, “temporary” is defined as the time between construction of intermediate cover and the construction of final cover. Temporary erosion controls are those controls which are installed or constructed within 180 days from when the intermediate cover is constructed and in place until permanent controls are constructed for the final cover.

2.0 Erosion Control Plan for Top Dome Surfaces and External Side Slopes with Intermediate Cover

Erosion control for above grade top dome surfaces and external embankment side slopes that drain directly to the site perimeter stormwater management system, have received intermediate cover, and either reached their permitted configuration or will remain inactive for longer than 180 days will be managed using a system of nonstructural and structural erosion and sediment controls to meet rule requirements for the intermediate cover phase of landfill construction.

The structural controls will consist of a combination of vegetation, temporary add-on swales, and letdown structures. These structural controls will be configured in a manner that will result in a net soil loss of 50 tons/acre/year or less from the external slope area. As shown on Sheet III-F-9, stormwater runoff will be collected in swales and conveyed to drainage letdown structures down the 25 percent slopes to the perimeter drainage system. The primary goal will be to establish the vegetative cover percentage and swale spacing distance indicated in the swale design summary table on Sheet III-F-10 on all external top dome surfaces and external embankment slopes. These criteria will result in a net soil loss of 50 tons/acres/year or less for each drainage swale and letdown combination specified on Sheets III-F-9 and III-F-10 (refer to Section 2.1 for additional information).

Mulch, woodchips, compost or straw/hay will be used as a layer placed over the intermediate cover to protect the exposed soil surface from erosive forces and conserve

soil moisture until vegetation can be established. The mulch, woodchips, compost or straw/hay will be used to stabilize recently graded or seeded areas. If needed, the mulch, woodchips, compost or straw/hay will be spread evenly over a recently seeded area and tracked into the surface to protect the soil from erosion and moisture loss, and provide additional erosional stability to the intermediate cover surface during the establishment of vegetation. These materials are not required for the establishment of vegetation on the intermediate cover unless they are needed to provide additional erosional stability to the intermediate cover surface. These materials will vary in thickness but the mulch, woodchips, compost or straw/hay will be placed so as not to inhibit the growth of vegetation. In the event that the indicated vegetative ground cover required for a specific swale spacing distance is not obtained within 180 days after intermediate cover is placed on a top dome or external side slope, mulch, woodchips, compost or straw/hay will be used as a secondary measure to limit soil loss to 50 tons/acre/year or less until vegetation is established. In the above referenced cases, other erosion protection measures will only be used upon prior written authorization by TCEQ (e.g., permit modification). Stormwater discharge from the site must comply with the current TPDES for the site. The discharge locations for the site are identified in Appendix IIIF as a part of the final drainage design and cannot be revised based on this ECP. Design and use of temporary erosion control measures can not result in offsite discharge exceeding the peak flow rates, volumes, or velocities listed in Table 4-1 of Appendix IIIF.

As an alternative to mulch, wood chips, compost, or straw/hay, a detention/sedimentation pond may be used as a secondary measure to limit the discharge of eroded soil loss to 50 tons/acre/year or less (refer to Section 2.2 for additional information) if the required percent vegetation goal is not obtained within 180 days after intermediate cover is placed on the top dome or external side slopes. In this case, the detention/sedimentation pond will remain in place until the specified percent vegetation goal is met (e.g., 60 percent vegetation on the external embankment slopes and top dome surfaces).

2.1 Drainage Swale and Letdown Structure Requirements

Sheet IIIF-F-9 shows a typical layout for erosion control structures, including temporary add-on swales and drainage letdowns. Sheet IIIF-F-10 provides a swale design summary, which includes spacing and vegetative cover requirements for the swales. Supporting calculations for the specifications listed on Sheet IIIF-F-10 are provided in Appendix IIIF-F-1 – Temporary Add-on Swale Design. Appendix IIIF-F-1 also includes a demonstration to show that sheet flow velocities for the grass established surfaces for all swale spacings are less than 5 ft/sec and sheet flow velocity for “nearly bare ground” is less than 3.5 ft/sec (consistent with Title 30 TAC §330.305(d)(1)).

Letdown structures will be located and constructed in a manner that minimizes erosion loss. The letdowns are designed to convey runoff from the 25-year frequency storm event (refer to Appendix IIIF-F-2 – Temporary Letdown Design for more information). Sheet IIIF-F-11 shows letdown details and the letdown design summary. As shown on Sheet IIIF-F-11, the letdowns will consist of either a lined open channel structure or a pipe letdown. The type, size, and number of letdowns will be determined based on the size of

the drainage area using the design information specified on Sheet III-F-11. As noted on Sheet III-F-11, the use of pipe letdowns will be limited to 1 inlet per letdown.

As noted on Sheet III-F-9, the acceptable soil loss is determined for each acre on the top dome surfaces and external embankment side slopes. The soil loss for top dome surfaces and external embankment side slopes will vary depending on swale spacing and percent vegetative cover (refer to Sheet III-F-10 for soil loss estimates). If certain percent vegetative cover is not achieved, a sediment control pond will be temporarily used for sediment capture to reduce the discharge of eroded soil from the external slopes to a rate that is equal to or less than 50 tons/acre/year. The swale spacing as shown on Sheet III-F-10 for top dome and side slope surfaces is based on the limiting soil loss of 50 tons/acres/year. If a vegetative coverage and swale spacing configuration results in a soil loss greater than 50 tons/acre/year, the following procedure will be used to verify that an acceptable intermediate cover thickness is maintained.

- Intermediate cover areas will be inspected to detect erosion gullies and vegetation loss.
- After identifying the areas requiring additional soil, these areas will be replenished with additional soil and graded to provide uniform surfaces prior to reseeding.
- Any damaged concentrated flow drainage structures such as swales will be repaired to eliminate uncontrolled concentrated flow.

Temporary open channel letdowns will be inspected for erosion/hollowing through and under the lining materials (e.g., gabions, grouted riprap, and turf reinforcement) and repaired as necessary to ensure the letdown is functioning as designed. As of October 2009, numerous erosion control structures have been installed at the site that conform to the requirements of this ECP, and these structures will remain in place and continue to serve as erosion control measures until they are decommissioned.

As stated previously, the primary goal is to obtain the required vegetation coverage percentage for each condition (e.g., swale spacing).

2.2 Sedimentation Pond Design

As noted on Sheets III-F-9 and III-F-10, if vegetative cover for any surface is maintained at or above the percentages given for swale spacing distances, the estimated soil loss is less than 50 tons/acre/year. In the event that certain percent ground cover that limits the soil loss to 50 tons/acre/year is not achieved and soil loss is temporarily greater than 50 tons/acre/year, a sedimentation pond will be used along with other structural and non-structural BMPs approved as part of this plan to limit the discharge of eroded soil. Sheet III-F-12 provides a procedure for determining the required pond size. Supporting calculations for the procedure listed on Sheet III-F-12 are included in Appendix III-F-3 – Sediment Control Pond Design. If a sediment control pond is used to limit the off-site discharge of eroded soil to 50 tons/acre/year or less from the external slope area, a demonstration noting how the pond was sized will be documented and maintained in the

Site Operating Record. This document will also include a statement that notes how the temporary sedimentation pond, the pond outlet, and any related perimeter channels were constructed consistent with the requirements of the Site Development Plan. Sheet III-F-13 shows the different options for typical pond outlet structures.

The sedimentation pond option is a secondary erosion control option, similar to mulch, wood chips, compost, or straw/hay, and will only be used if the required percent vegetation specification is not met. If the sedimentation pond option is implemented, the swales and letdowns specified will remain in-place. The sedimentation pond option simply allows for the control of sediment while vegetation is being established.

For example, if intermediate cover is placed over a 20-acre external side slope area that is at the permitted elevation on December 31, then the operator will install swales and letdowns on the 20-acre slope consistent with the design and specifications listed in Section 2.1. The operator then has 180 days (which for this example would be June 29) to obtain the required vegetation coverage on the 20-acre area. If in early June it becomes apparent that the percent vegetation will be less than the required coverage on June 29, then the operator may install a sedimentation pond downstream of the 20-acre area, consistent with the requirements shown on Sheet III-F-12. Consistent with Section II.D of the TCEQ guidance document titled, "Guidance for Addressing Erosional Stability During All Phases of Landfill Operation," the sedimentation pond will remain in-place so that the net annual soil loss from the 20-acre area that could leave the facility boundary is less than 50 tons/acre/year until the required percent vegetation specification is met.

If a sedimentation pond is used as a source to maintain a soil loss equal to or less than 50 tons/acre/year, the following procedure will be used to verify that an acceptable intermediate cover thickness is maintained.

- Intermediate cover areas will be inspected to detect erosion gullies and vegetation loss.
- After identifying the areas requiring additional soil, these areas will be replenished with additional soil and graded to provide uniform surfaces prior to reseeded.
- Any damaged concentrated flow drainage structures such as swales will be repaired to eliminate uncontrolled concentrated flow.

As stated previously, the primary goal is to obtain the specified vegetation coverage percentage on top dome surfaces and external embankments. The sedimentation pond will only be used until the specified vegetation coverage percentage is obtained. The sedimentation pond may only be used for a period of 12 months after the 180-day period has expired (e.g., 12 months after the June 29th date used in the above example). Once the required vegetation percentage is achieved, then the sedimentation pond will no longer be needed (but may remain in-place as an additional BMP until the site reaches the permitted final configuration). If the percent vegetation does not meet the required specification within the 12-month period, then additional erosion control measures will be implemented. These measures will include: (1) adjusting the swale spacing, (2)

applying mulch, wood chips, compost, or straw/hay, or similar TCEQ approved materials, or (3) the submittal of a permit modification to revise this erosion control plan to provide additional erosion protection measures that will allow the site to meet the goals of this plan.

2.3 Other Erosion Control BMPs

Other best management practices (BMPs) used in conjunction with the above erosion control measures are listed below.

- Check Dams – These structures will be used in channels to slow down flow velocities and improve sediment capture.
- Silt Fences – These structures will be used in capturing sediment transported by sheet flow and for diversion of flow for controlling sediment discharge.
- Compost Filter Berms – These structures may be used in capturing sediment transported by sheet flow and for diversion of flow for controlling sediment discharge.
- Erosion Booms – These structures may be used in capturing sediment and for diversion of flow for controlling sediment discharge.

These erosion control measures will be used on slopes to help control erosion loss. Rock check dams will be used in the detention/sedimentation pond. Refer to Sheet III-F-14 for details of typical BMPs.

Nonstructural controls that will be used at the site to minimize erosion loss include: plans and designs to minimize disruption of the natural features, drainage, topography, and vegetative cover features; phased development to minimize the area of bare soil exposed at any given time; plans to disturb only the smallest area necessary to perform current activities; scheduling of construction activities during the time of year with the least erosion potential; and specific plans for the stabilization of exposed surfaces in a timely manner. Other BMPs will only be utilized upon prior written authorization (e.g., permit modification) by TCEQ.

2.4 Schedule and Recordkeeping Requirements

After an external side slope or top dome surface reaches the final permitted grade or will remain inactive for longer than 180 days, the structural erosion control features and letdown structures will be in place within 180 days from when intermediate cover is placed. During this 180 day period, the structural erosion control structures will be constructed and vegetation established. Structural erosion control measures consist of drainage swales, letdown structures, and detention ponds.

At the end of this 180-day period, the cover log will be updated to document the external side slope and top dome surface area, the structural controls that were installed, and a

demonstration showing how the structural controls meet the 50 tons/acre/year or less soil loss requirement (e.g., percent vegetation coverage, swale spacing, and letdowns installed). Inspection requirements and schedules are listed in the SOP for all drainage features, including intermediate cover areas. If the required percent vegetation coverage is not achieved within the 180-day period, secondary erosion control measures such as mulch, wood chips or compost will be used to limit the soil loss to the 50 tons/acre/year or less. Other erosion protection measures will only be utilized upon prior written authorization (e.g., permit modification) by TCEQ. In addition, a detention/sedimentation pond may also be used until the required vegetation coverage is achieved. Any secondary measure used will be documented in the Site Operating Record at the end of the 180-day period to document compliance with this plan. In addition, the date the required vegetation cover is achieved and the date that the secondary measure is no longer needed will also be documented in the Site Operating Record. The dates and locations of installation of erosion and sediment control will also be documented in the Site Operating Record. Inspection requirements and schedules are listed in the SOP for all drainage features, including intermediate cover areas. Inspection and maintenance of the erosion and sediment control structures of the top dome surfaces and external embankment side slopes will follow the same schedule and methods as described in Section 4.24 of the facility's SOP.

For example, as stated in Section 4.18.3 of the current Site Operating Plan (SOP), intermediate cover areas are inspected weekly and within 72 hours of a rainfall event of 0.5 inches or more, or as soon as the areas are accessible, for proper placement, thickness, erosion, and compaction. Additionally, Section 4.23 of the SOP also requires inspections of perimeter channels and ponds to ensure they are functioning as designed (e.g., excess sediment removed, outlet structures intact, and erosion control measures intact, etc.) on a weekly basis and after a rainfall event of 0.5 inches or more, or as soon as the areas are accessible.

During the inspection of structural controls (e.g., vegetation over intermediate cover areas), if significant soil loss is identified in a given intermediate cover area, impacted areas will be replenished with additional soil. Prior to application of temporary erosion controls and seeding, the area will be graded to eliminate preferential path ways or any other uneven surface due to settlement to prevent concentrated flow over the intermediate cover areas. Soil for replenishment of cover areas will be borrowed from sedimentation ponds or any other soil source. If sediment collected from wet retention pond(s) (e.g., Pond P5 or temporary sedimentation ponds) is used for erosion layer replenishment, it will be stockpiled outside the ponds to dry out prior to being used for intermediate cover layer replenishment. Soil borrowed from other soil sources may be used as intermediate cover layer and erosion layer replenishment soil.

2.5 Construction Activities on Top Dome Surfaces and External Side Slopes with Intermediate Cover

Occasionally, top dome surfaces and external side slopes that have been stabilized through the use of swales, letdown structures, and compliance with the minimum required

vegetation cover specification will be disturbed due to various construction activities such as the installation or repair of a landfill gas system, regrading of an area due to ponded water caused by uneven waste settlement, the repair of erosion rills, or damage due to an extreme storm event or natural disaster. Each of these events will be documented in the Site Operating Record. Recorded information will include the date of construction, approximate area disturbed, and the date re-seeding of the disturbed area occurred. In accordance with Title 30 TAC §330.165(g), previously stabilized surfaces will be repaired within 5 days of detection of the disturbance of these surfaces.

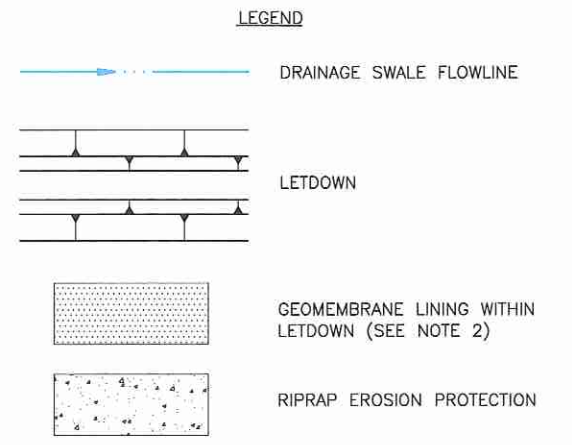
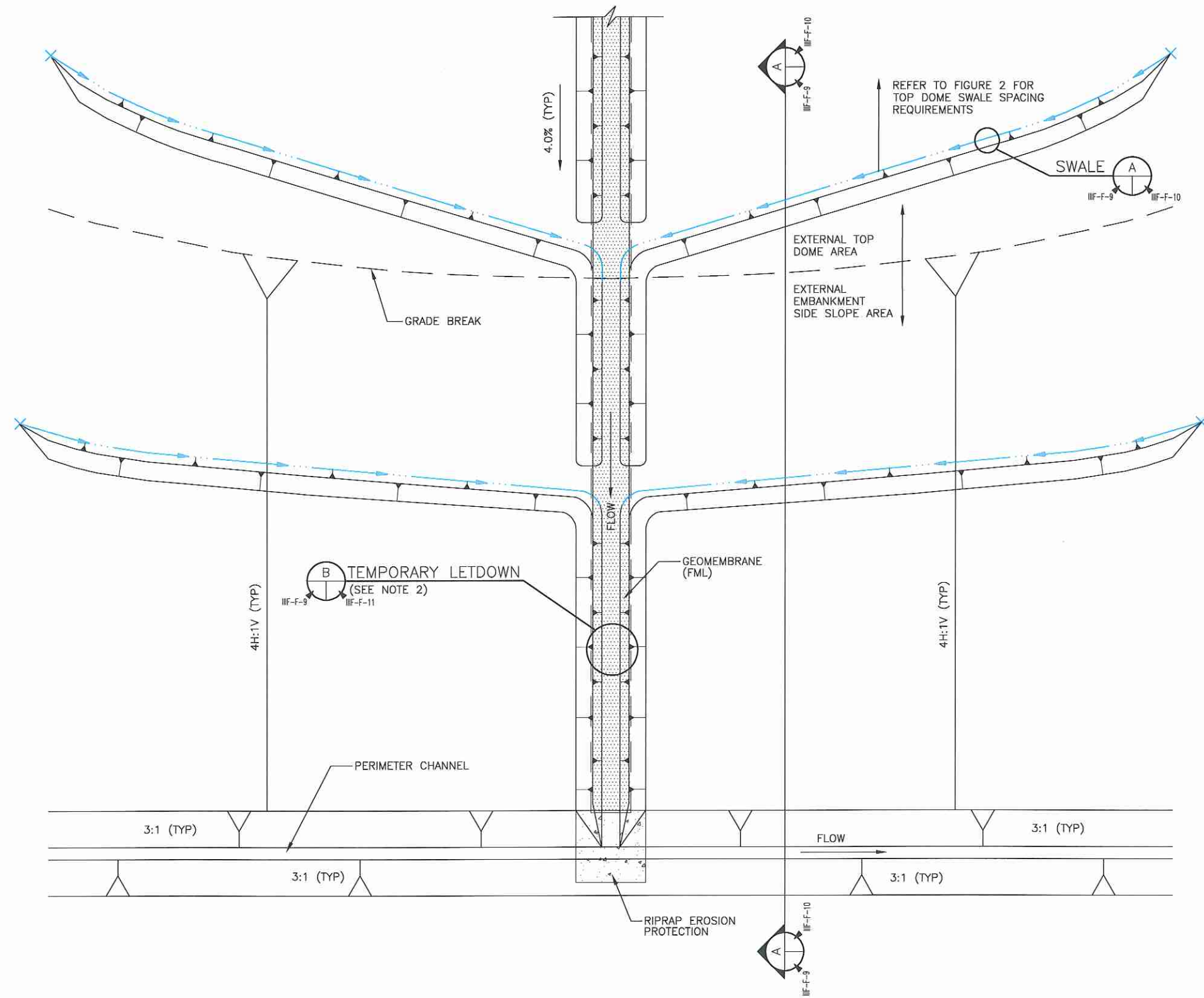
3.0 Erosion Control Plan for Daily Cover Areas and Intermediate Cover Areas for Non-External Side Slopes

BMPs will be employed to control erosion. BMPs will include the use of temporary rock riprap, silt fences, straw bales, check dams, interceptor swales and berms, temporary and permanent seeding and sodding, surface roughening, matting and mulching, sediment traps, and surface wetting for dust control.

Examples of erosion and sedimentation control features that will be used during the phased development of the site are shown in Appendix IIIA-A of the Site Development Plan. The following provides general guidelines of how the erosion control features will minimize sediment discharge from the site.

- As noted in the SOP, vegetation will be established on above-grade intermediate cover areas that remain inactive. The temporary vegetative cover will minimize erosion potential.
- Typically, uncontaminated stormwater runoff from the site will be channeled through the perimeter channel system to detention ponds before being discharged from the site. Sediment that collects in the channels and detention ponds will be removed consistent with the stormwater system maintenance plan presented in Section 2.3 of Appendix IIIF.
- Erosion will be controlled by vegetation in drainage structures with flow velocities less than or equal to 5 ft/sec. For drainage structures with flow velocities greater than 5 ft/sec, rock riprap or gabions will be used for surface reinforcement. Other erosion protection measures will only be utilized upon prior written authorization (e.g., permit modification) by TCEQ.

Typical erosion control features are shown on Sheet IIIF-F-14. Inspection items and schedules are listed in the SOP for all drainage features, daily cover, and intermediate cover areas.

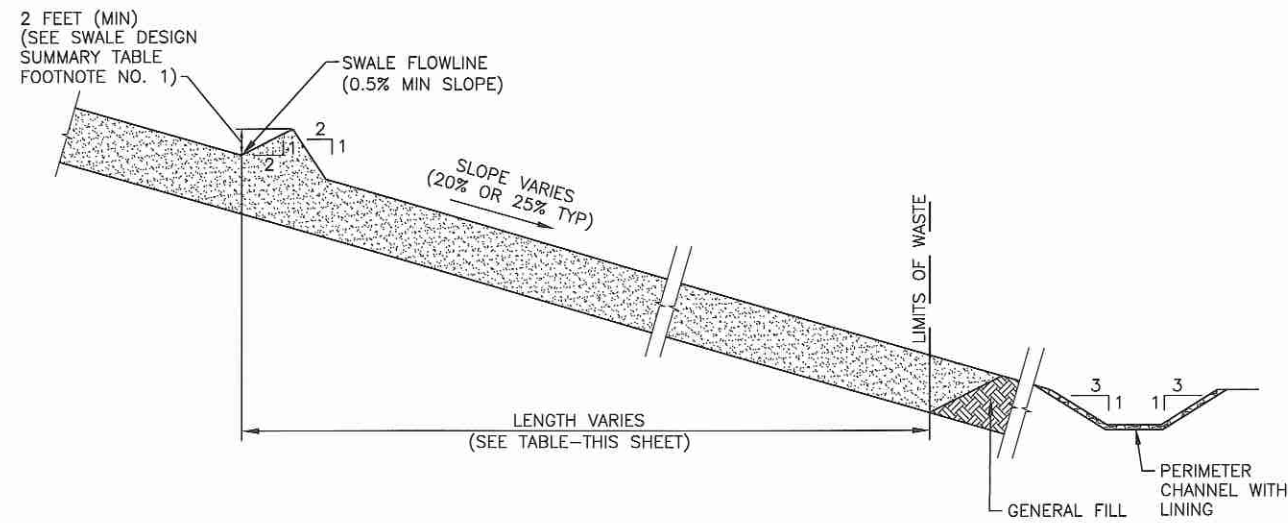


- NOTES:**
1. THE ACCEPTABLE SOIL LOSS IS LESS THAN OR EQUAL TO 50 TONS/ACRE/YEAR. THE SOIL LOSS FOR TOP DOME SURFACES AND EXISTING EXTERNAL EMBANKMENT SIDE SLOPES WILL VARY DEPENDING ON SWALE SPACING AND PERCENT VEGETATIVE COVER (REFER TO SHEET III-F-10 FOR SOIL LOSS ESTIMATES).
 2. TEMPORARY LETDOWN IS SHOWN AS AN OPEN CHANNEL WITH A GEOMEMBRANE LINER. AS NOTED ON SHEET III-F-11, OTHER CHANNEL LININGS MAY BE USED (e.g., GABIONS, GROUT, GROUTED CONCRETE RIPRAP, AND TURF REINFORCEMENT MAT). IN ADDITION, PIPE LETDOWNS MAY ALSO BE USED. HOWEVER, IF PIPE LETDOWNS ARE USED THEY WILL BE LIMITED TO 1-INLET AS SHOWN ON SHEET III-F-11.

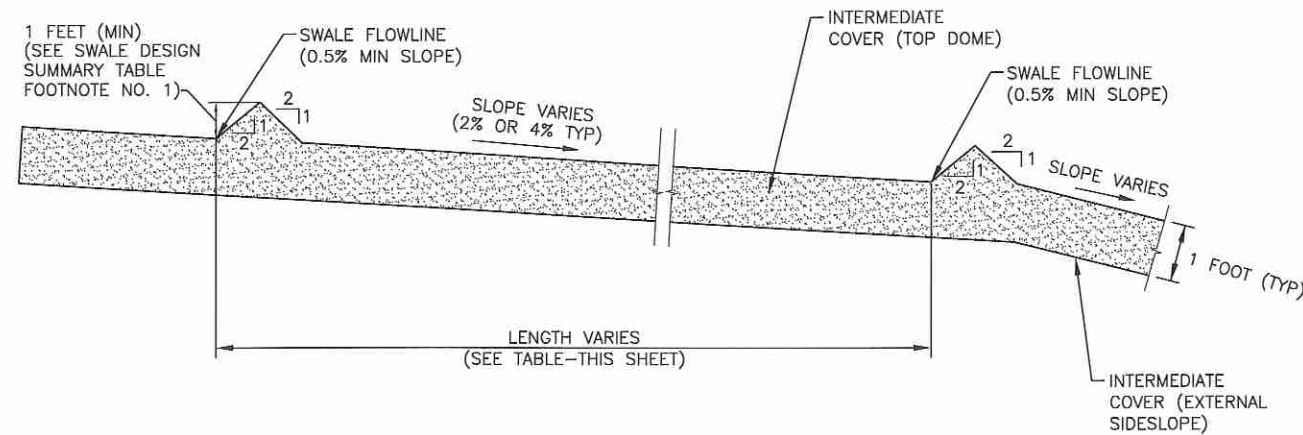


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		SHEET III-F-9

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SIDE SLOPE DRAINAGE SWALE
 III-F-9 III-F-10



TOP DOME SURFACE DRAINAGE SWALE
 III-F-9 III-F-10

SWALE DESIGN SUMMARY¹

SIDE SLOPE (25%)				TOP SLOPE (4%)			
VEGETATIVE COVER PERCENTAGE	DISTANCE BETWEEN SWALES (FT)	ESTIMATED SOIL LOSS (TONS/ACRE/YEAR)	ADDITIONAL SEDIMENT CAPTURE REQUIRED ²	VEGETATIVE COVER PERCENTAGE	DISTANCE BETWEEN SWALES ³ (FT)	ESTIMATED SOIL LOSS (TONS/ACRE/YEAR)	ADDITIONAL SEDIMENT CAPTURE REQUIRED ²
60	300	17.8	NO	60	500	1.3	NO
70	300	7.2	NO	70	500	0.5	NO
80	300	5.5	NO	80	500	0.4	NO
90	300	2.7	NO	90	500	0.2	NO
SIDE SLOPE (20%)				TOP SLOPE (2%)			
60	300	13.3	NO	60	600	1.4	NO
70	300	5.4	NO	70	600	0.6	NO
80	300	4.1	NO	80	600	0.4	NO
90	300	2.0	NO	90	600	0.2	NO
				60	700	1.5	NO
				70	700	0.6	NO
				80	700	0.5	NO
				90	700	0.2	NO
				60	700	0.7	NO
				70	700	0.3	NO
				80	700	0.2	NO
				90	700	0.1	NO

¹ REFER TO APPENDIX III-F-1 FOR SUPPORTING CALCULATIONS.
² IF SITE SPECIFIC CONDITIONS YIELD A MAXIMUM HORIZONTAL DISTANCE BETWEEN THE TOE OF THE SLOPE AND GRADE BREAK OF LESS THAN 300 FEET FOR SIDE SLOPES AND A DISTANCE OF 500 FEET FROM THE GRADE BREAK TO THE PEAK OF THE TOP SLOPES, ESTABLISHMENT OF 60% VEGETATION WILL BE SUFFICIENT MEANS OF EROSION CONTROL WITHOUT THE ADDITION OF TEMPORARY SWALES AND LETDOWNS GIVEN THAT THE TOTAL SOIL LOSS FOR THE SIDE SLOPE IS LESS THAN 50 TONS/ACRE/YEAR AND THE TOP SLOPE IS LESS THAN 50 TONS/ACRE/YEAR.
³ NUMBERS INDICATE THE MAXIMUM SWALE SPACING FOR A GIVEN VEGETATIVE COVER PERCENTAGE.

SWALE DRAINAGE AREA SUMMARY

CONDITION (SWALE HEIGHT)	MAXIMUM DRAINAGE AREA (ACRES)	MINIMUM SWALE SPACING ¹ (FEET)	MAXIMUM SWALE LENGTH ² (FEET)
TOP SLOPE (2 FT SWALE, 2%)	48.4	500	4,216
TOP SLOPE (1.5 FT SWALE, 2%)	22.3	500	1,942
TOP SLOPE (1 FT SWALE, 2%)	7.4	500	644
TOP SLOPE (2 FT SWALE, 4%)	25.3	500	2,204
TOP SLOPE (1.5 FT SWALE, 4%)	11.7	500	1,019
TOP SLOPE (1 FT SWALE, 4%)	3.9	500	340
SIDE SLOPE (2 FT SWALE, 25%)	5.4	300	784
SIDE SLOPE (2 FT SWALE, 20%)	6.3	300	915

¹ THE MINIMUM SWALE SPACING IS USED TO DETAIN THE MAXIMUM SWALE LENGTH GIVEN THAT THE AREA IS FIXED. MINIMUM SWALE SPACING IS OBTAINED FROM THE CALCULATIONS PROVIDED ON PAGE III-F-1-2.
² MAXIMUM SWALE LENGTH CALCULATED USING THE FOLLOWING EQUATION:
 MAXIMUM DRAINAGE AREA x (43,560 SF/ACRE)/MINIMUM SWALE SPACING



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OPEN CHANNEL GEOMEMBRANE LETDOWN DESIGN SUMMARY

DESIGN IS APPLICABLE FOR A DRAINAGE AREA UP TO 35 ACRES (TOP DECK AND SIDE SLOPE).

25% SLOPE
MAXIMUM FLOW DEPTH = 0.59 FT.
BOTTOM WIDTH = 8 FT.

20% SLOPE
MAXIMUM FLOW DEPTH = 0.63 FT.
BOTTOM WIDTH = 8 FT.

4% SLOPE
MAXIMUM FLOW DEPTH = 1.00 FT.
BOTTOM WIDTH = 8 FT.

2% SLOPE
MAXIMUM FLOW DEPTH = 1.22 FT.
BOTTOM WIDTH = 8 FT.

OPEN CHANNEL GABION LETDOWN DESIGN SUMMARY

DESIGN IS APPLICABLE FOR A DRAINAGE AREA UP TO 20 ACRES (2% TOP DECK), 30 ACRES (4% TOP DECK), AND 35 ACRES (SIDE SLOPE).

25% SLOPE
MAXIMUM FLOW DEPTH = 1.31 FT.
BOTTOM WIDTH = 8 FT.

20% SLOPE
MAXIMUM FLOW DEPTH = 1.39 FT.
BOTTOM WIDTH = 8 FT.

4% SLOPE
MAXIMUM FLOW DEPTH = 1.98 FT.
BOTTOM WIDTH = 8 FT.

2% SLOPE
MAXIMUM FLOW DEPTH = 1.92 FT.
BOTTOM WIDTH = 8 FT.

OPEN CHANNEL ROCK RIPRAP LETDOWN DESIGN SUMMARY

DESIGN IS APPLICABLE FOR TOP DECK DRAINAGE AREAS ONLY - UP TO 20 ACRES (2% TOP DECK), AND 25 ACRES (4% TOP DECK).

2% SLOPE
MAXIMUM FLOW DEPTH = 1.92 FT.
BOTTOM WIDTH = 8 FT.

4% SLOPE
MAXIMUM FLOW DEPTH = 1.80 FT.
BOTTOM WIDTH = 8 FT.

OPEN CHANNEL GROUDED RIPRAP LETDOWN DESIGN SUMMARY

DESIGN IS APPLICABLE FOR A DRAINAGE AREA UP TO 25 ACRES (2% TOP DECK), 35 ACRES (4% TOP DECK), AND 35 ACRES (SIDE SLOPE).

25% SLOPE
MAXIMUM FLOW DEPTH = 1.11 FT.
BOTTOM WIDTH = 8 FT.

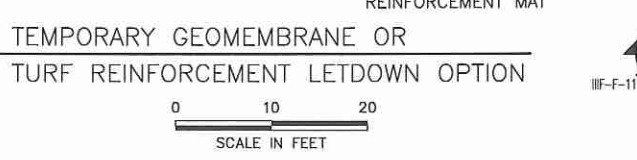
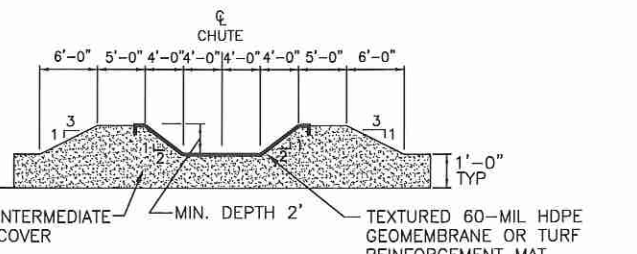
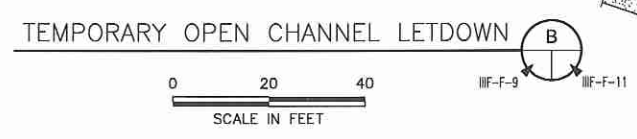
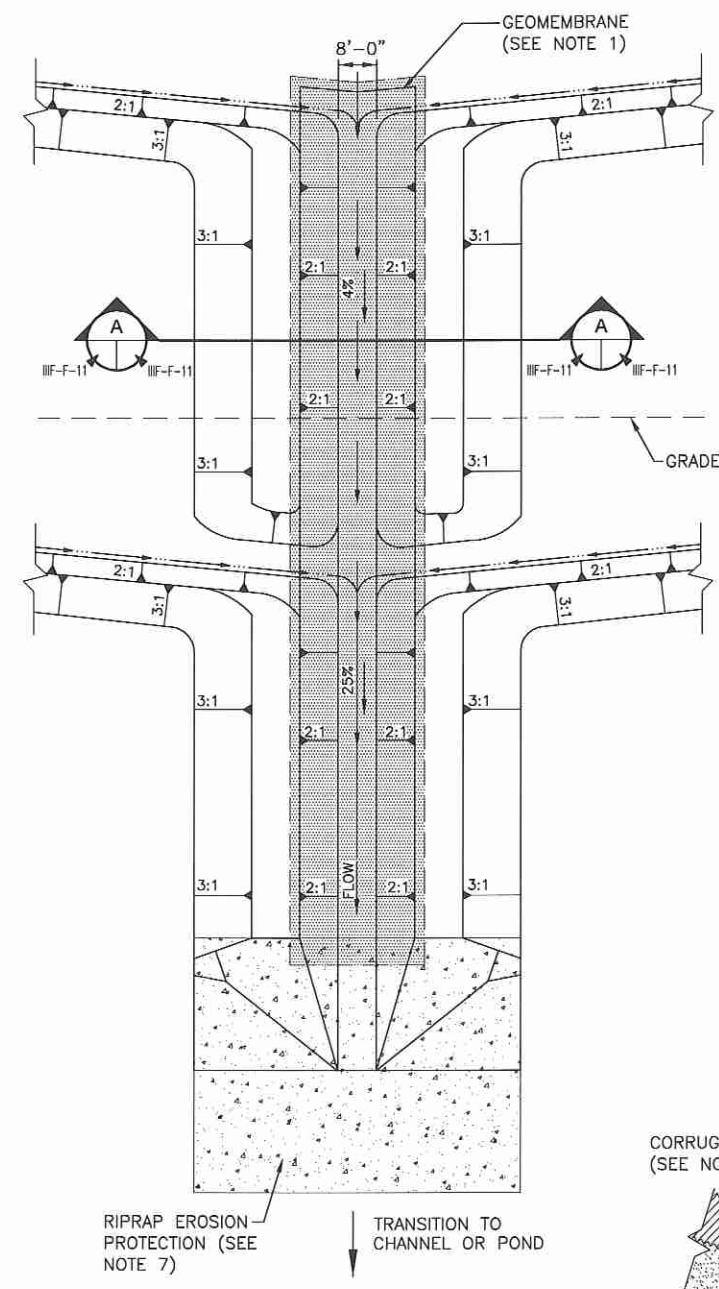
20% SLOPE
MAXIMUM FLOW DEPTH = 1.19 FT.
BOTTOM WIDTH = 8 FT.

4% SLOPE
MAXIMUM FLOW DEPTH = 1.85 FT.
BOTTOM WIDTH = 8 FT.

2% SLOPE
MAXIMUM FLOW DEPTH = 1.86 FT.
BOTTOM WIDTH = 8 FT.

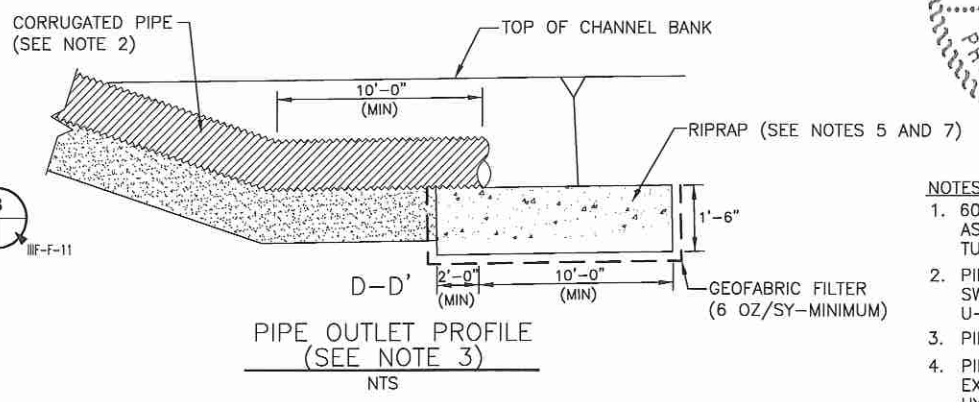
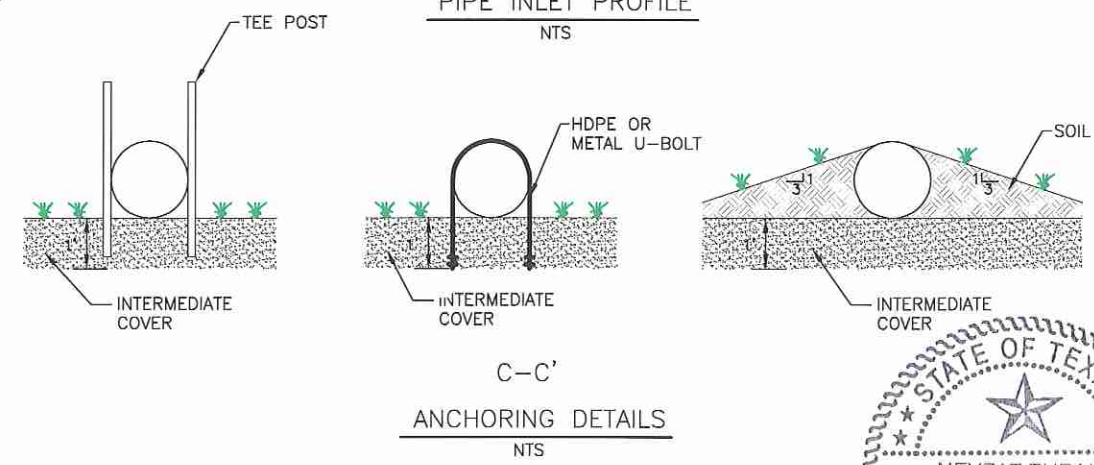
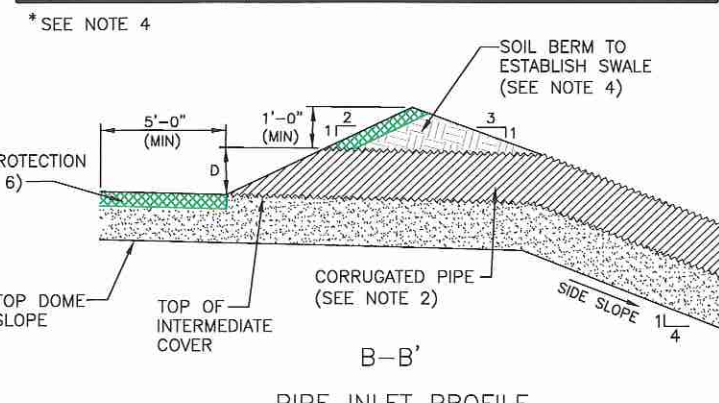
OPEN CHANNEL TURF REINFORCEMENT LETDOWN DESIGN SUMMARY

SEE GROUDED RIPRAP LETDOWN DESIGN.



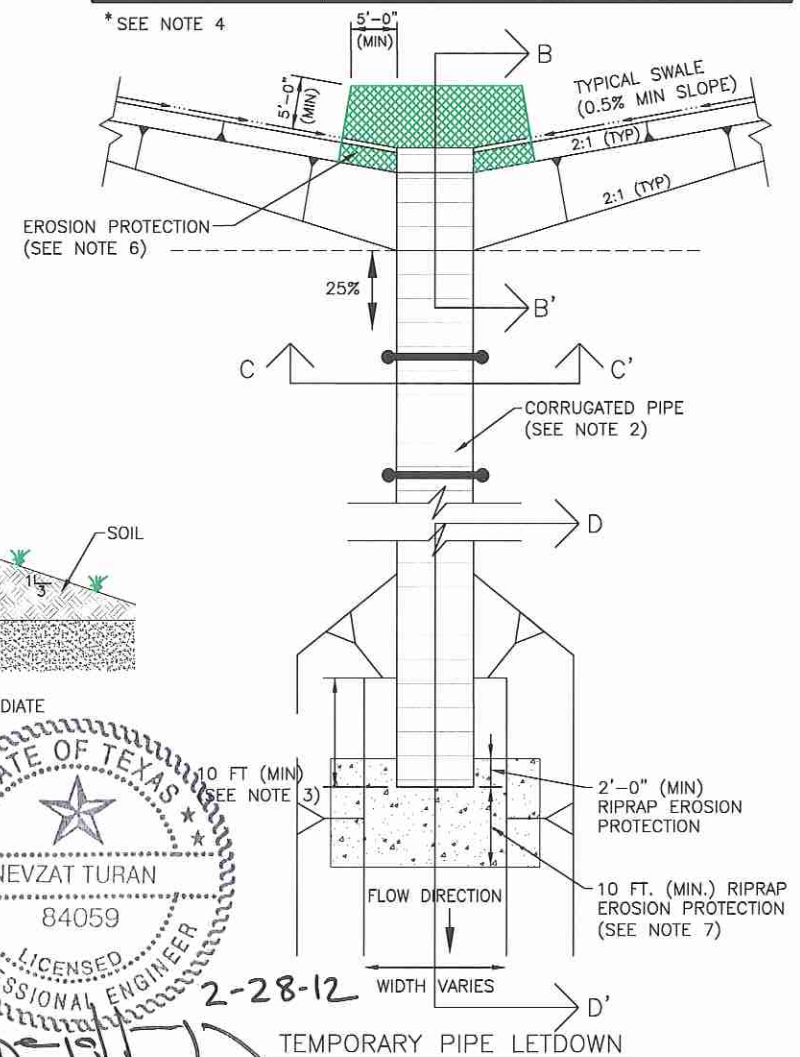
20% PIPE LETDOWN DESIGN SUMMARY*
(USE OF PIPE LETDOWN IS LIMITED TO 1-INLET)

DRAINAGE AREA (ACRE)	DESIGN FLOW RATE (CFS)	REQUIRED PIPE DIAMETER (FT)
3.1	23.0	2
3.5	26.0	3



25% PIPE LETDOWN DESIGN SUMMARY*
(USE OF PIPE LETDOWN IS LIMITED TO 1-INLET)

DRAINAGE AREA (ACRE)	DESIGN FLOW RATE (CFS)	REQUIRED PIPE DIAMETER (FT)
2.2	16.0	2
2.8	21.0	3



- NOTES:**
- 60 MIL HDPE GEOMEMBRANE TEXTURED BOTH SIDES WILL BE USED FOR GEOMEMBRANE LETDOWN LINING. AS AN ALTERNATIVE, TEMPORARY LETDOWN CAN BE LINED WITH GABIONS, GROUDED CONCRETE RIPRAP, TURF REINFORCEMENT MAT, OR ROCK RIPRAP.
 - PIPE DRAINAGE LETDOWN WILL BE ANCHORED BY USING SOIL BERM AT THE INLET LOCATED WITHIN THE SWALE. ADDITIONAL ANCHORING ON THE SIDE SLOPE MAY BE PROVIDED USING SOIL, HDPE OR METAL U-BOLTS, T-POSTS OR EQUIVALENT MATERIALS.
 - PIPE WILL BE EXTENDED INTO THE CHANNEL TO MINIMIZE EROSION.
 - PIPE LETDOWNS WILL BE LIMITED TO 1 INLET PER LETDOWN. SOIL BERMS AROUND THE PIPE INLET WILL BE EXTENDED A MINIMUM 1-FOOT ABOVE THE LETDOWN PIPE INLET. REFER TO PAGE III-F-2-25 FOR HYDRAULIC ANALYSIS.
 - RIPRAP APRON DESIGN IS PROVIDED ON PAGES III-F-2-37 AND 38 AND III-F-2-51 AND 52. D₅₀ FOR RIPRAP 5-INCHES IS MINIMUM.
 - RIPRAP, GROUDED RIPRAP, GABIONS, GEOMEMBRANE, EXISTING VEGETATION OR TURF REINFORCEMENT MAY BE USED FOR EROSION PROTECTION.
 - OTHER EROSION PROTECTION (e.g., RIPRAP, GROUDED RIPRAP, GABIONS OR TURF REINFORCEMENT) MAY BE USED AT TEMPORARY LETDOWN OUTFALLS.
 - REFER TO PAGE III-F-2-9 FOR EROSION PROTECTION DESIGN. IF LETDOWN DISCHARGES TO A POND, 10 FEET OF RIPRAP WILL BE SUFFICIENT.

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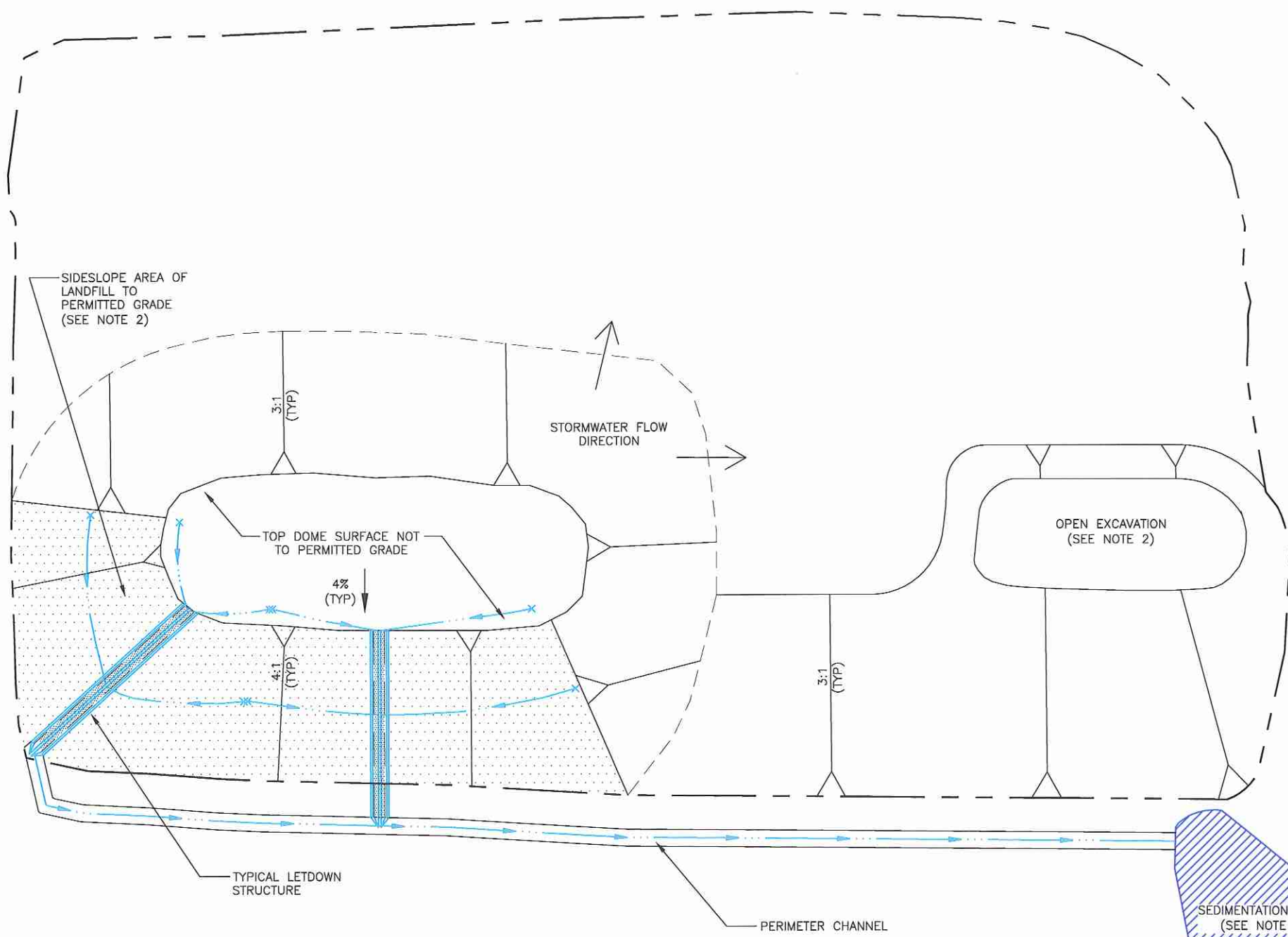
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EXAMPLE CALCULATION

REQUIRED POND SIZE = EXTERNAL EMBANKMENT AREA (ACRES) X POND AREA REQUIRED/UNIT DRAINAGE AREA FACTOR

EXTERNAL EMBANKMENT AREA DRAINING TO POND = 50 ACRES

ADDITIONAL UPLAND AREA DRAINING TO POND = 0 ACRES (SEE NOTE 1)

REQUIRED SEDIMENT REMOVAL FROM EXTERNAL SIDE SLOPE AREA = 80 TONS/ACRE/YEAR TO 50 TONS/ACRE/YEAR

POND AREA REQUIRED/UNIT DRAINAGE AREA FACTOR = 0.060 (FROM TABLE BELOW)

REQUIRED POND SIZE = 50 ACRES X 0.060 = 3.00 ACRES

SIZE OF POND REQUIRED ¹		
REQUIRED SEDIMENT REMOVAL (TONS/ACRE/YEAR)	POND AREA REQUIRED/UNIT DRAINAGE AREA FACTOR	EFFICIENCY OF POND (DYNAMIC AND QUIESCENT)
60 TO 50	0.025	16.6%
70 TO 50	0.040	28.9%
80 TO 50	0.060	37.6%
90 TO 50	0.075	45.0%
100 TO 50	0.110	50.3%
200 TO 50	0.300	75.0%

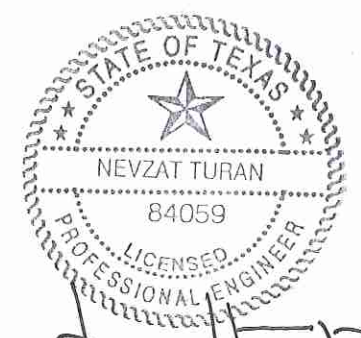
¹ REFER TO APPENDIX IIIF-F-3 FOR MORE INFORMATION. THE POND DESIGN AND DEMONSTRATION ARE PROVIDED TO ENSURE THAT SEDIMENT DISCHARGE FROM THE SITE WILL BE PREVENTED DURING INITIAL ESTABLISHMENT OF VEGETATION OVER THE SIDE SLOPES AND TOP DOME SURFACES.

NOTES:

- EXAMPLE POND CONFIGURATION IS SHOWN. A DEMONSTRATION WILL BE INCLUDED IN THE SITE OPERATING RECORD TO SHOW THAT THE POND HAS THE CAPABILITY TO CAPTURE SEDIMENT SUCH THAT DISCHARGE IS LESS THAN OR EQUAL TO 50 TONS/ACRE/YEAR FROM THE EXTERNAL SIDE SLOPE AND TOP DOME AREA. THE DEMONSTRATION WILL ACCOUNT FOR THE ADDITIONAL SEDIMENT CREATED BY THE UPLAND AREA THAT FLOWS TO THE POND. FOR DEMONSTRATION PURPOSES, THE POND DEPTH WILL BE AN AVERAGE OF 4 FEET. OVERALL SEDIMENT DISCHARGE FROM THE SITE MUST COMPLY WITH THE CURRENT TPDES PERMIT FOR THE SITE.
- EXCAVATED FUTURE CELL AREAS OR SOIL BORROW AREAS CAN ALSO BE USED AS SEDIMENTATION PONDS. IF THESE AREAS ARE USED FOR PONDS, A DEMONSTRATION NOTING THAT THE EXCAVATED FUTURE CELL AREA OR SOIL BORROW AREA HAS MORE CAPACITY THAN THE VOLUME PRODUCED BY THE 25-YEAR, 24-HOUR STORM WILL BE DOCUMENTED AND MAINTAINED IN THE SITE OPERATING RECORD.
- AS STATED IN SECTION 2.2, A STATEMENT WILL BE ADDED TO THE SITE OPERATING RECORD EACH TIME A SEDIMENTATION POND IS INSTALLED TO NOTE HOW THE TEMPORARY SEDIMENTATION POND AND THE POND OUTLET WERE CONSTRUCTED CONSISTENT WITH THE REQUIREMENTS OF THE SITE DEVELOPMENT PLAN.

LEGEND

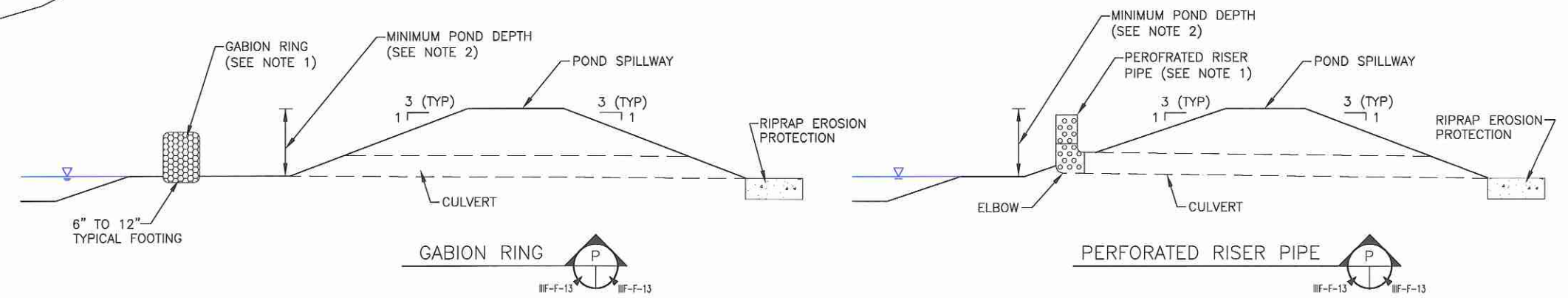
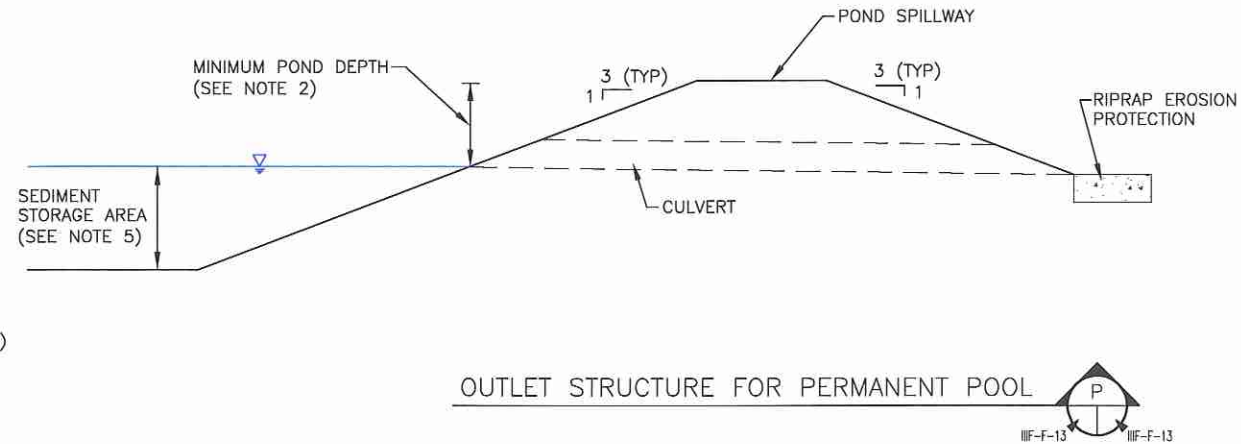
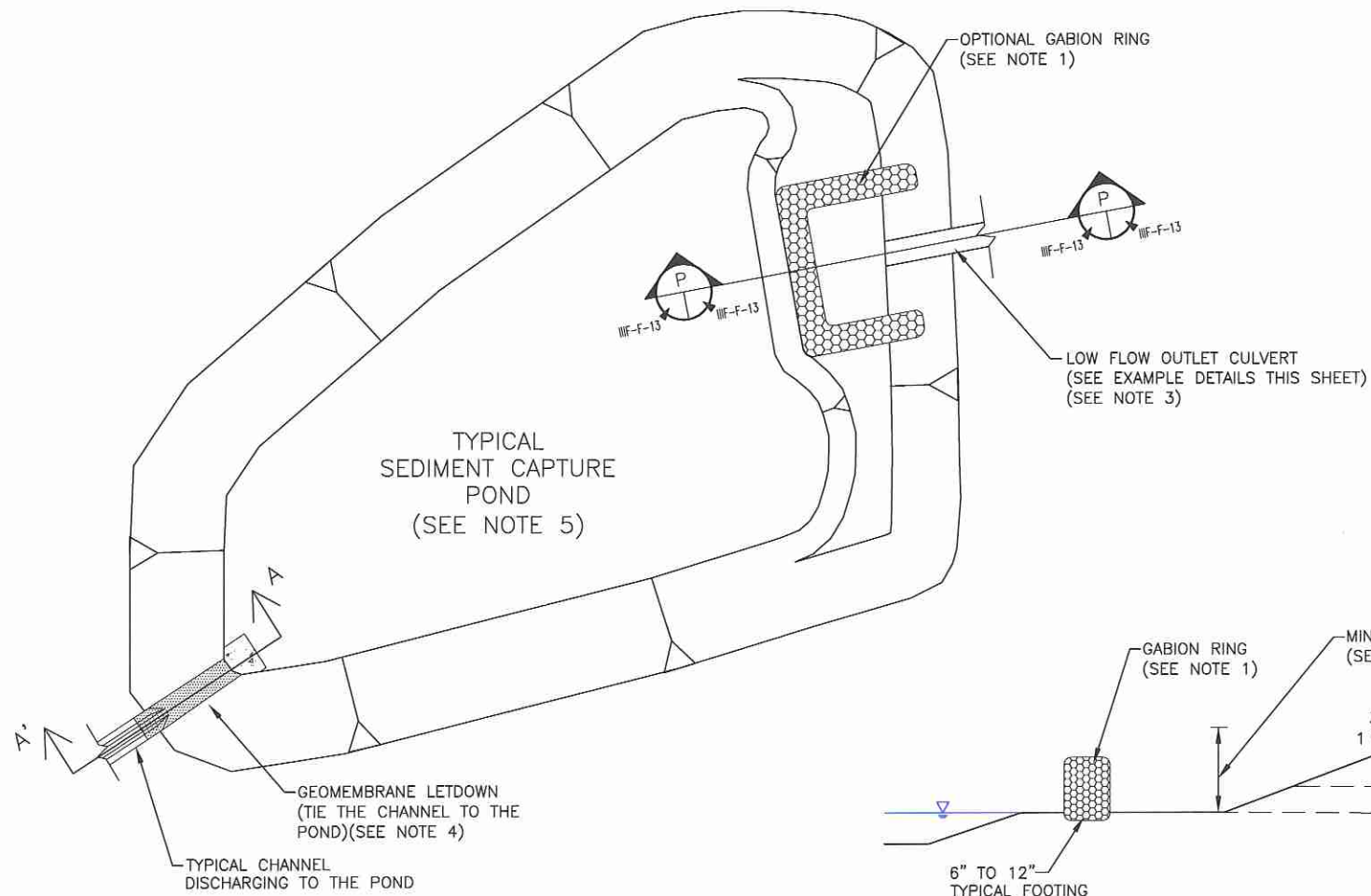
- EXTERNAL SIDE SLOPE TO PERMITTED GRADE
- LETDOWN
- DRAINAGE SWALE
- STORMWATER FLOW DIRECTION



[Signature]
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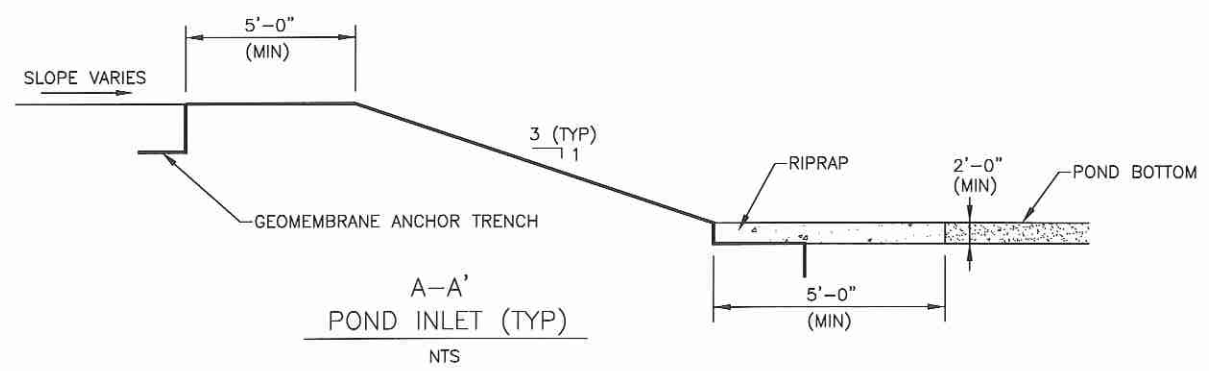
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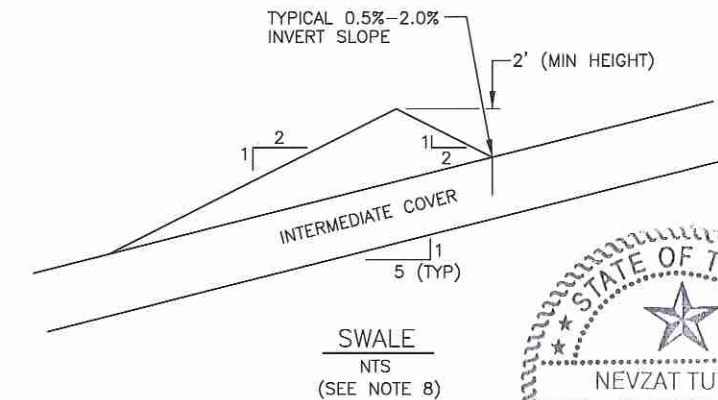
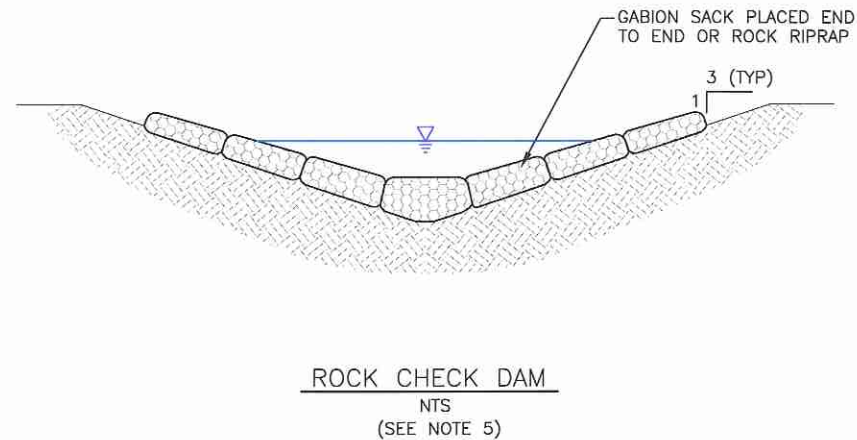
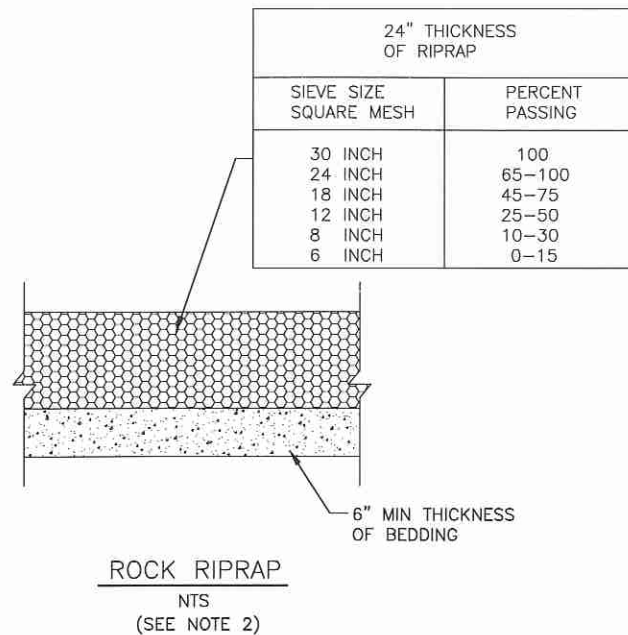
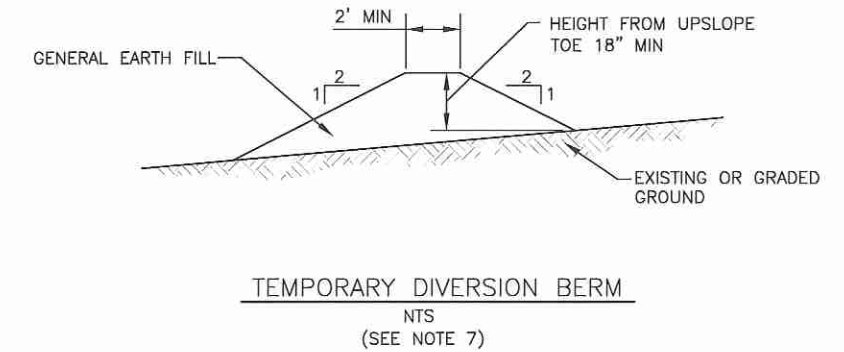
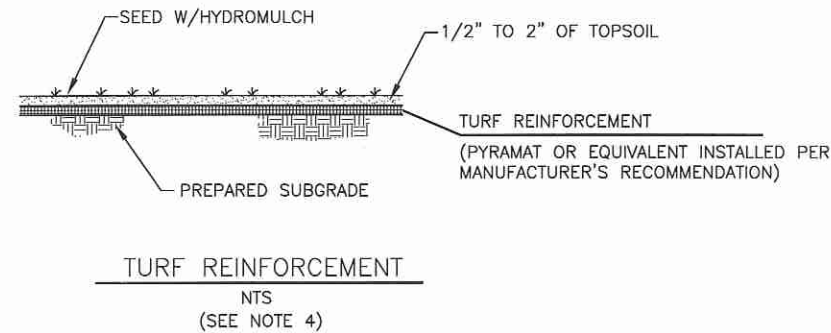
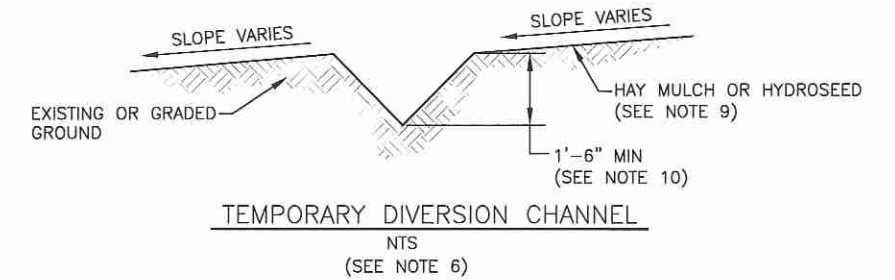
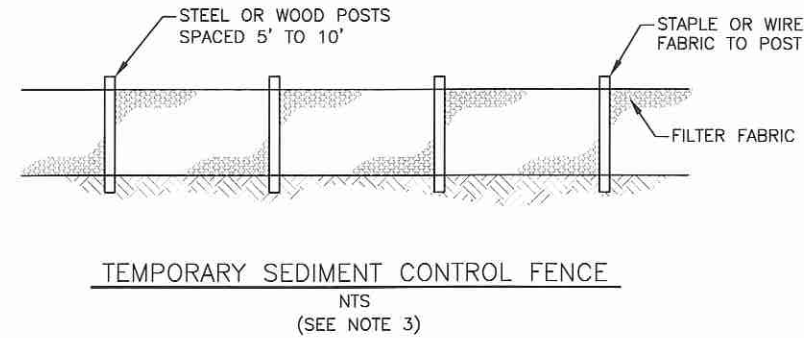
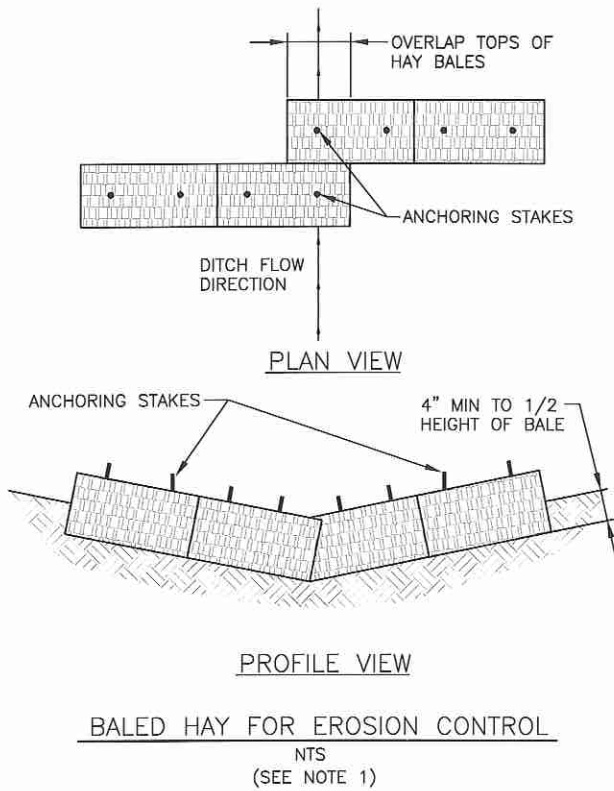


OPTIONS FOR DRY PONDS

- NOTES:**
1. AS AN OPTION TO THE GABION RING, A PERFORATED RISER PIPE (SHOWN ON THIS SHEET) MAY ALSO BE USED, AS WELL AS A ROCK CHECK DAM.
 2. MINIMUM POND DEPTH IS 4 FEET BETWEEN THE LOW FLOW OUTLET FLOW LINE AND POND SPILLWAY ELEVATION.
 3. IF THE POND IS INSTALLED WITHOUT A LOW FLOW OUTLET, THEN SEE NOTE 2 ON SHEET III-F-12.
 4. VEGETATIVE SURFACING, GROUDED RIPRAP, RIPRAP, GABIONS, OR TURF REINFORCEMENT MAY BE USED TO ENSURE THE STABILITY OF THE POND INLET.
 5. POND BOTTOM AREAS WILL BE EXCAVATED BELOW THE LOW FLOW OUTLET FLOW LINE ELEVATION TO PROVIDE SEDIMENT STORAGE. SEDIMENT ACCUMULATED IN POND WILL BE REMOVED AS NEEDED TO ENSURE SEDIMENT STORAGE CAPACITY BELOW THE FLOWLINE ELEVATION OF LOW FLOW OUTLET (REFER TO SECTION 2.4 FOR ADDITIONAL INFORMATION REGARDING SEDIMENT REMOVAL).



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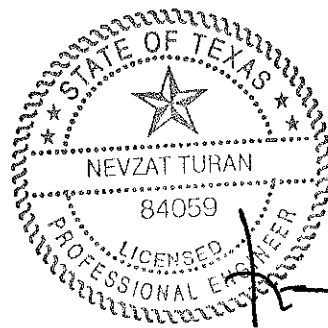
NOTES:

- BALED HAY MAY BE USED IN NEWLY ESTABLISHED COVER AREAS OR DISTURBED/REGRADED SURFACES TO MAINTAIN SHEET FLOW UNTIL VEGETATION IS ESTABLISHED.
- ROCK RIPRAP MAY BE USED IN AREAS WHERE CONCENTRATED FLOW WITH HIGH VELOCITIES MAY OCCUR (e.g., CULVERT INLETS/OUTLETS).
- A TEMPORARY SEDIMENT CONTROL FENCE MAY BE USED IN CAPTURING SEDIMENT TRANSPORTED BY SHEET FLOW AND FOR DIVERSION OF FLOW FOR CONTROLLING SEDIMENT DISCHARGE.
- TURF REINFORCEMENT MAY BE USED ON NEWLY ESTABLISHED SURFACES SUCH AS INTERMEDIATE COVER AND IN CHANNELS WHERE MODERATELY HIGH FLOW VELOCITIES ARE EXPECTED.
- A ROCK CHECK DAM MAY BE USED IN CHANNELS TO SLOW DOWN FLOW VELOCITIES AND IMPROVE SEDIMENT CAPTURE.
- A TEMPORARY DIVERSION CHANNEL MAY BE USED FOR SHORTENING SHEET FLOW DISTANCES IN UNDEVELOPED AREAS OR IN LARGER CHANNELS TO PROVIDE MEANDERING AND SLOWER FLOW VELOCITIES TO PREVENT IN-CHANNEL EROSION.
- A TEMPORARY DIVERSION BERM MAY BE USED IN AREAS TO DIVERT FLOW FROM ENTERING STEEP SLOPED AREAS (e.g., TOP OF EXCAVATION) AND TO REDUCE SHEET FLOW LENGTHS.
- A SWALE MAY BE USED IN AREAS TO DIVERT FLOW FROM ENTERING STEEP SLOPED AREAS (e.g., TOP OF EXCAVATION) AND TO REDUCE SHEET FLOW LENGTHS.
- HAY MULCH AND HYDROSEED MAY ALSO BE USED FOR NEWLY ESTABLISHED SURFACES TO PROMOTE VEGETATION ESTABLISHMENT AND PREVENT EROSION.
- THE VALUE SHOWN IS AT THE TIME OF CHANNEL INSTALLATION; CHANNEL WIDTH AND DEPTH MAY VARY.



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DATE: 02/2012 FILE: 0120-87-11 CAD: IIF-F-14-TYPICAL BMP.DWG	DRAWN BY: SRF DESIGN BY: CRM REVIEWED BY: JPY	Weaver Boos Consultants TBPE REGISTRATION NO. F-3727
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		SHEET IIF-F-14

APPENDIX III F-F-1
TEMPORARY ADD-ON SWALE DESIGN



2-28-12

Includes pages III F-F-1-1 through III F-F-1-13

SWALE DESIGN

This appendix includes the expected soil loss calculations for various swale spacing intervals on the side slopes and top dome surfaces. An example calculation is provided on pages III-F-1-2 through III-F-1-4 for a vegetative cover of 60 percent. For the results of various percent vegetative covers and swale spacing intervals, refer to the table on page III-F-1-5 and to Sheet III-F-10 – Swale Design Summary. If the required percent vegetation coverage is not achieved within the 180-day period, secondary erosion control measures such as mulch, wood chips, compost or straw/hay will be used to limit the soil loss to 50 tons/acre/year or less. In addition, a detention/sedimentation pond may also be used until the required vegetation coverage is achieved. Any secondary measure used will be documented in the Site Operating Record at the end of the 180-day period to document compliance with this plan. In addition, the date the required percent vegetation coverage is achieved and the secondary measure is no longer needed will also be documented in the Site Operating Record.

Also included in this appendix are the sheet flow velocities for all swale spacing intervals on the side slopes and top dome surfaces. As noted in these calculations (pages III-F-1-6 through III-F-1-8), all velocities are acceptable.

Additionally, this appendix includes a calculation for the maximum drainage area that each swale can drain, as well as the maximum swale length. These calculations are included on pages III-F-1-9 through III-F-1-13.

Required: Determine the required spacing of the drainage swales for different percentages of vegetative cover for top dome surfaces and external embankment side slopes.

Method:

1. Estimate soil loss per acre based on percent ground cover and swale spacing for top dome surface and external side slope.
2. Summary.

Notes:

1. The following example calculation procedure has been developed for 60 percent ground cover.
2. The table on page III-F-1-5 includes the results of the following procedure for 60, 70, 80, and 90 percent ground cover and various swale spacings. The results are also summarized on Figure 2 in Appendix III-F.

References:

1. SCS National Engineering Handbook, Chapter 3 - Erosion.
2. TNRC, *Use of the USLE in Final Cover/Configuration Design*, 1993.
3. United States Environmental Protection Agency, *Solid Waste Disposal Facility Criteria Technical Manual*, 1993.

Solution:

1. Estimate soil loss per acre based on percent ground cover and swale spacing for top dome surface and external side slope.

Soil Loss Equation: $A = RKL_sCP$

Where:

- A= Soil loss (tons/ac/yr)
- R= Rainfall factor
- K= Soil erodibility factor
- L_s = Slope length/slope gradient factor
- C= Plant cover or cropping management factor
- P= Erosion practice factor

The rainfall factor, R, represents the average intensity for the maximum intensity, 30 minute storms over a 22 year period of record compiled by the SCS. Using Figure 1 (Ref 2), Average Annual Values of the R Factor, the R factor for Denton County is:

$$R = 275$$

The soil erodibility factor, K, factor represents the resistance of a soil surface to erosion as a function of the soil's physical and chemical properties. Assume an organic matter content of 2% to determine the K factor. The intermediate soil will consist of soils comparable to sandy clay. Additionally, compost will be added to intermediate soil as necessary to protect against erosion. Therefore, the following is a conservative K value for the site (Table 1 on page 6, Ref. 2).

$$K = 0.15$$

The slope length/slope gradient factor, L_s , represents the erosion of the soil due to both slope length and degree of slope.

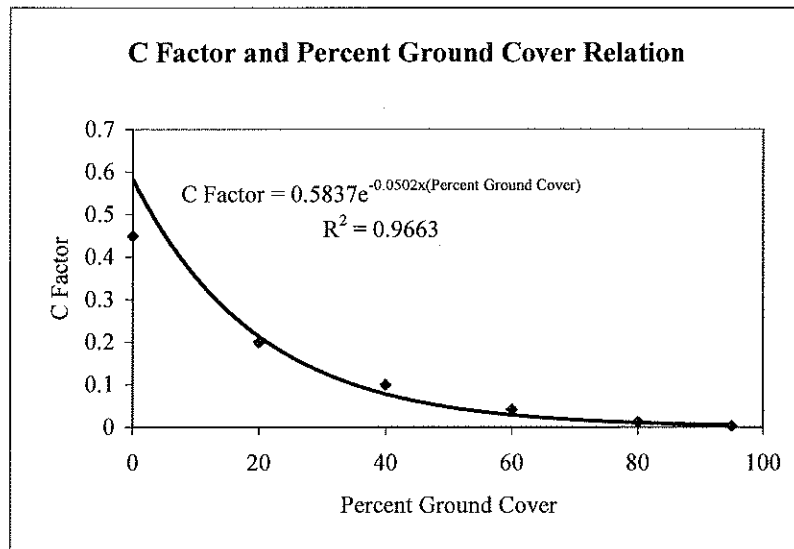
Case 1. Top Slope	Case 2. Side Slope
slope = 4 %	slope = 20 %
length = 500 ft	length = 300 ft
Case 3. Side Slope	Case 4. Top Slope
slope = 25 %	slope = 4 %
length = 300 ft	length = 600 ft
Case 5. Top Slope	Case 6. Top Slope
slope = 4 %	slope = 2 %
length = 700 ft	length = 700 ft

Using the above information and Figure 2 (Ref 2, p.9), the L_s factors are determined.

Case	Slope (%)	Slope Length (ft)	L_s
1. Top Slope	4	500	0.75
2. Side Slope	20	300	7.70
3. Side Slope	25	300	10.30
4. Top Slope	4	600	0.80
5. Top Slope	4	700	0.88
6. Top Slope	2	700	0.38

The plant cover or cropping management factor, C, represents the percentage of soil loss that would occur if the surface were partially protected by some combination of cover and management practices. C Factor for Permanent Pasture, Range, and Idle Land with No Appreciable Canopy has the following relation with percent ground cover (GC) (from Ref 2, p.7).

% GC	C Factor:
0	0.45
20	0.20
40	0.10
60	0.042
80	0.013
95	0.003



$C \text{ Factor} = 0.5837e^{(-0.0502 \times 60)}$
 $C \text{ Factor} = 0.0420$

The erosion control practice factor, P, measures the effect of control practices that reduce the erosion potential of the runoff by influencing drainage patterns, runoff concentration, and runoff velocity. Contouring for this site will be done only to establish vegetation.

$P = 1.00$

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0120-87-11-73-01
TEMPORARY ADD-ON SWALE DESIGN

Slope Condition	R	K	L_s	C	P	A (tons/ac/yr)
1. Top Slope 4% slope 500 ft length	275	0.15	0.75	0.0420	1.0	1.3
2. Side Slope 20% slope 300 ft length	275	0.15	7.70	0.0420	1.0	13.3
3. Side Slope 25% slope 300 ft length	275	0.15	10.30	0.0420	1.0	17.8
4. Top Slope 4% slope 600 ft length	275	0.15	0.80	0.0420	1.0	1.4
5. Top Slope 4% slope 700 ft length	275	0.15	0.88	0.0420	1.0	1.5
6. Top Slope 2% slope 700 ft length	275	0.15	0.38	0.0420	1.0	0.7

2. Summary

For a summary of soil loss rates for various percentages of ground cover, see Figure 2 in Appendix III-F and page III-F-1-5.

SOIL LOSS ESTIMATE SUMMARY TABLE

Case	Slope (%)	Length (ft)	L_s	Percent Ground Cover	C Factor	A (tons/ac/yr)
Top Slope	4	500	0.32	60	0.042	1.3
Top Slope	4	500	0.32	70	0.017	0.5
Top Slope	4	500	0.32	80	0.013	0.4
Top Slope	4	500	0.32	90	0.0064	0.2
Top Slope	4	600	0.80	60	0.042	1.4
Top Slope	4	600	0.80	70	0.017	0.6
Top Slope	4	600	0.80	80	0.013	0.4
Top Slope	4	600	0.80	90	0.0064	0.2
Top Slope	2	700	0.38	60	0.042	0.7
Top Slope	2	700	0.38	70	0.017	0.3
Top Slope	2	700	0.38	80	0.013	0.2
Top Slope	2	700	0.38	90	0.0064	0.1
Top Slope	4	700	0.88	60	0.042	1.5
Top Slope	4	700	0.88	70	0.017	0.6
Top Slope	4	700	0.88	80	0.013	0.5
Top Slope	4	700	0.88	90	0.0064	0.2
Side Slope	20	300	7.70	60	0.042	13.3
Side Slope	20	300	7.70	70	0.017	5.4
Side Slope	20	300	7.70	80	0.013	4.1
Side Slope	20	300	7.70	90	0.0064	2.0
Side Slope	25	300	10.30	70	0.017	17.8
Side Slope	25	300	10.30	80	0.013	7.2
Side Slope	25	300	10.30	90	0.0064	5.5
Side Slope	25	300	10.30	90	0.0064	2.7

Required: Determine the sheet flow velocity for the top dome surfaces and external embankment side slopes and compare to the permissible non-erodible flow velocity.

Method:

1. Determine the peak velocities for the cases listed on page III-F-1-2.
2. Compare to permissible velocities.
3. Conclusion.

References:

1. National Engineering Handbook, Section 4, Hydrology. *Chapter 15 - Travel Time, Time of Concentration and Lag.*

Solution: Use the typical case scenarios from the USLE calculation to determine the expected peak sheet flow velocity.

Case 1. Top Slope	Case 2. Side Slope
slope = 4 %	slope = 20 %
length = 500 ft	length = 300 ft
Case 3. Side Slope	Case 4. Top Slope
slope = 25 %	slope = 4 %
length = 300 ft	length = 600 ft
Case 5. Top Slope	Case 6. Top Slope
slope = 4 %	slope = 2 %
length = 700 ft	length = 700 ft

1. Determine the peak velocities for the cases listed on page III-F-1-2.

Cultivated Straight Row (Overland Flow)

From Figure 15.2 (page 15-8 in Ref. 1), determine the velocities for all cases.

Case 1.	V = 1.8 ft/s
Case 2.	V = 4.0 ft/s
Case 3.	V = 4.5 ft/s
Case 4.	V = 1.8 ft/s
Case 5.	V = 1.8 ft/s
Case 6.	V = 1.6 ft/s

Note: Figure 15.2 is reproduced on page III-F-1-8.

2. Compare to permissible velocities.

Summary of Velocities

	Condition	Equivalent Percent Ground Coverage	Peak Velocity (ft/s)	Permissible Velocity ¹ (ft/s)
	Cultivated Straight Row	4%, 500 ft	>60%	1.8
20%, 300 ft		>60%	4.0	5.0
25%, 300 ft		>60%	4.5	5.0
4%, 600 ft		>60%	1.8	5.0
4%, 700 ft		>60%	1.8	5.0
2%, 700 ft		>60%	1.6	5.0

¹ Permissible velocity information is from USACE EM 1110-0-1418, Chapter 5 - Evaluation of Stability.

3. Conclusion.

The peak velocities for each case are listed in the above summary table. As shown peak velocities are below permissible velocities for the conditions analyzed. After 180 days, at least 60 percent vegetation will be established in order to maintain permissible non-erodible velocities.

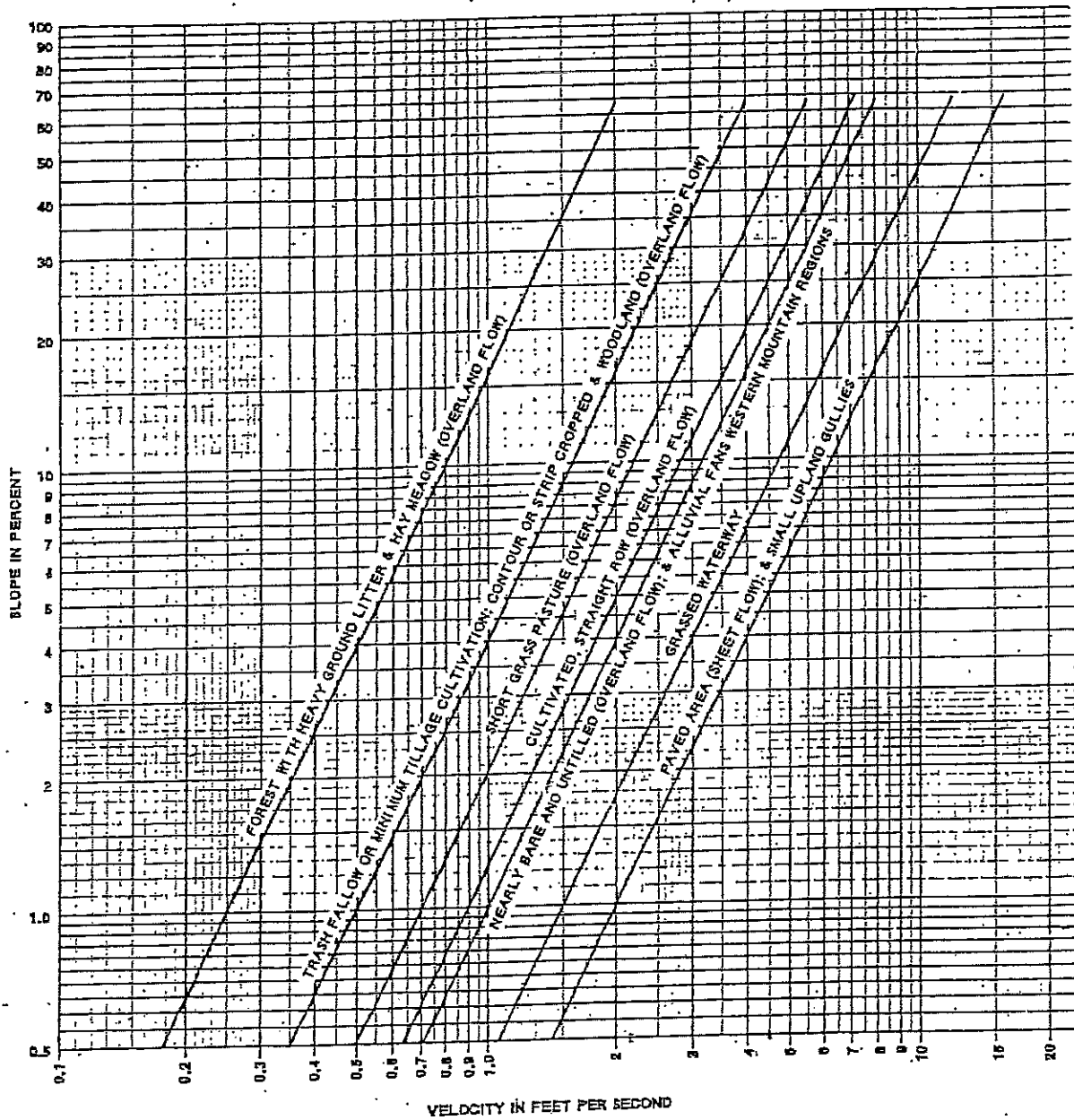


Figure 15.2.—Velocities for upland method of estimating T_c

Required: Analyze swales to determine the adequacy of the swale design.

Method:

1. Determine the 25-year, 24-hour flow rates for a maximum swale drainage area for top slopes and side slopes using the Rational Method.
2. Determine maximum swale length that corresponds to the maximum swale drainage area.

Reference:

1. State of Texas, Department of Transportation, Bridge Division, Hydraulic Manual, March 2004.

Solution:

1. Determine the 25-year, 24-hour flow rates for a maximum swale drainage area for top slopes and side slopes using the Rational Method.

$$Q = CIA$$

Where: C = 0.8 (runoff coefficient, Ref 1.)
I = intensity, in/hr
A = drainage area, ac

$$I = \frac{b}{(t_c + d)^2}$$

b = 90 From Ref. 1, for Denton County
d = 8.5 25-year storm event
e = 0.781
t_c is assumed to be 10 min.

$$I = 9.22 \text{ in/hr}$$

For Top Slope (2%) :

Maximum Drainage Area (2 ft swale) = 48.4 acres
Maximum Drainage Area (1.5 ft swale) = 22.3 acres
Maximum Drainage Area (1 ft swale) = 7.4 acres

Flow Rate (2 ft swale) =	357.0	cfs
Flow Rate (1.5 ft swale) =	165.0	cfs
Flow Rate (1 ft swale) =	55.0	cfs

For Top Slope (4%) :

Maximum Drainage Area (2 ft swale) = 25.3 acres
Maximum Drainage Area (1.5 ft swale) = 11.7 acres
Maximum Drainage Area (1 ft swale) = 3.9 acres

Flow Rate (2 ft swale) =	186.5	cfs
Flow Rate (1.5 ft swale) =	86.3	cfs
Flow Rate (1 ft swale) =	28.8	cfs

For Side Slope:

Maximum Drainage Area (25%) = 5.4 acres
Maximum Drainage Area (20%) = 6.3 acres

Flow Rate (2 ft swale, 25%) =	39.8	cfs
Flow Rate (2 ft swale, 20%) =	46.5	cfs

2. Determine maximum swale length that corresponds to the maximum swale drainage area.

Condition (swale height)	Maximum Drainage Area (acres)	Minimum Swale Spacing ¹ (ft)	Maximum Swale Length ² (ft)
Top Slope (2 ft swale, 2%)	48.4	500	4,216
Top Slope (1.5 ft swale, 2%)	22.3	500	1,942
Top Slope (1 ft swale, 2%)	7.4	500	644
Top Slope (2 ft swale, 4%)	25.3	500	2,204
Top Slope (1.5 ft swale, 4%)	11.7	500	1,019
Top Slope (1 ft swale, 4%)	3.9	500	340
Side Slope (2 ft swale, 23%)	5.4	300	784
Side Slope (2 ft swale, 20%)	6.3	300	915

¹ Minimum swale spacing is taken from calculations provided on page III-F-1-2.

² Maximum swale length calculated using the following equation:

$$\text{Maximum Drainage Area} \times (43,560 \text{ sf/acre}) / \text{Minimum Swale Spacing}$$

Prep By: TMB
Date: 2/21/2012

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0120-87-11-73-01
SWALE ANALYSIS

Chkd By: ICC
Date: 2-28-12

Flow Rate (cfs)	Bottom Slope (ft/ft)	n-value	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)	Froude No.	Velocity Head (ft)	Energy Head (ft)	Flow Area (sq. ft.)	Top Width of Flow (ft)
2 ft Top Slope and Side Slope Swale												
357	0.005	0.03	2	50	0	1.99	3.48	0.616	0.19	2.17	102.58	103.29
186.5	0.005	0.03	2	25	0	1.99	3.48	0.614	0.19	2.18	53.63	53.82
46.5	0.005	0.03	2	5	0	1.98	3.38	0.598	0.18	2.16	13.76	13.88
39.8	0.005	0.03	2	4	0	1.99	3.36	0.594	0.18	2.17	11.87	11.93
1.5 ft Top Slope Swale												
165.0	0.005	0.03	2	50	0	1.49	2.87	0.586	0.13	1.62	57.53	77.35
86.3	0.005	0.03	2	25	0	1.49	2.87	0.585	0.13	1.62	30.10	40.32
1 ft Top Slope Swale												
55.0	0.005	0.03	2	50	0.0	0.99	2.17	0.546	0.07	1.06	25.30	51.29
28.8	0.005	0.03	2	25	0	0.99	2.17	0.545	0.07	1.06	13.24	26.74

Note: Calculations were performed using the HYDROCALC HYDRAULICS program developed by Dodson and Associates (Version 1.2a, 1996).

Maximum flow depth is 1.99 ft < 2.0 ft (swale height).

Design is acceptable.

Example Calculation: Calculate the normal depth for the swale for the maximum size side slope drainage area.

List of Symbols

- Q_d = design flow rate for channel, cfs
- R = hydraulic radius, ft
- n = Manning's roughness coefficient
- S = channel slope, ft/ft
- b = bottom width of channel, ft
- z_r = z-ratio (ratio of run to rise for channel sideslope) for right side slope of swale
- z_l = z-ratio (ratio of run to rise for channel sideslope) for left side slope of swale
- A_f = flow area, sf
- g = gravitational acceleration = 32.2 ft/s²
- T = top width of flow, ft
- d = normal depth of swale, ft

The program uses an iterative process to calculate the normal depth of the swale to satisfy Manning's Equation

$$Q = \frac{1.486}{n} A R^{0.67} S^{0.5}$$

Design Inputs:

- $Q_d = 39.8$ cfs
- $S = 0.005$ ft/ft
- $b = 0$ ft
- $z_r = 4$ (H) : 1 (V)
- $z_l = 2$ (H) : 1 (V)
- $n = 0.03$

Step 1 - Based on the geometry of the swale cross-section, solve for R and A_f

$$R = \frac{bd + 1/2d^2(z_r + z_l)}{b + d((z_l^2 + 1)^{0.5} + (z_r^2 + 1)^{0.5})}$$

$$A_f = bd + 1/2d^2(z_r + z_l)$$

assume: $d = 1.99$ ft

$$R = 0.938 \text{ ft}$$

$$A_f = 11.87 \text{ sf}$$

solve for Q: Q = 39.8

if Q is not equal to Q_d , select a new d and repeat calculations

Step 2 - solve for velocity, T, Froude number, velocity head, and energy head

$$Q = VA \Rightarrow \quad V = Q/A$$

$$V = \quad 3.36 \text{ ft/s}$$

$$T = b + d(z_1 + z_r)$$

$$T = \quad 11.93 \text{ ft}$$

$$F_r = \frac{V}{(gA/T)^{0.5}}$$

$$F_r = \quad 0.594$$

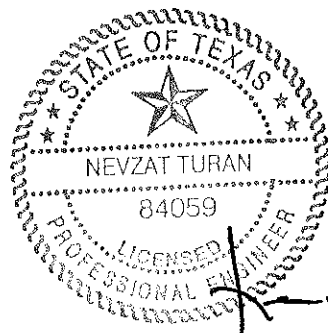
$$\text{Velocity Head} = \frac{V^2}{2g}$$

$$\text{Velocity Head} = \quad 0.18 \text{ ft}$$

Energy Head = water elevation + velocity head

$$\text{Energy Head} = \quad 2.17 \text{ ft}$$

APPENDIX III F-F-2
TEMPORARY LETDOWN DESIGN



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2-28-12

Includes Pages III F-F-2-1 through III F-F-2-52

LETDOWN (OR CHUTE) DESIGN

The temporary letdown structure options include open channel flow letdowns and pipe letdowns. Open channel flow letdowns will be lined with either geomembrane, turf reinforcement mat, gabions, grouted concrete riprap, or rock riprap. The pipe letdowns are typically corrugated plastic pipe. Both types of letdowns will have an energy dissipater structure at the bottom of the letdown. Typical letdown details are shown on Sheet III-F-11 – Letdown Design Summary.

This appendix includes a demonstration to show that the letdown structure sizes shown on Sheet III-F-11 will contain the peak flow rate produced by the 25-year storm event. The geomembrane-lined and gabion-lined chutes (as well as turf reinforcement, rock riprap, and grouted riprap-lined chutes) were analyzed for peak flow rates generated from drainage areas ranging from 5 acres to 35 acres. This analysis (pages III-F-2-2 and III-F-2-8) is summarized on Sheet III-F-11 and shows the maximum drainage areas that the 2-foot-deep chutes (8 feet minimum bottom width) are adequate to handle (i.e., the maximum flow depth calculated is less than 2.00 feet).

Also included in this appendix is an analysis for the 24-inch- and 36-inch-diameter temporary pipe letdowns for 25 percent slopes. The maximum flow that these pipes were capable of conveying was determined, and from this design flow rate a maximum drainage area size was calculated. The drainage area corresponds to the area that could drain to the pipe at each inlet. As noted on Sheet III-F-11, the use of pipe letdowns will be limited to 1 inlet per letdown. The design summary for geomembrane-lined letdowns and pipe letdowns is provided on Sheet III-F-11.

Required: Analyze chutes to determine size of chute for drainage area that ranges from 5 acres to 35 acres.

Method: 1. Determine the 25-year, 24-hour flow rates for various sizes of chute drainage areas using the Rational Method.

Reference: 1. State of Texas, Department of Transportation, Bridge Division, Hydraulic Manual, March 2004.

Solution: 1. Determine the 25-year intensity flow rates.

$$Q = CIA$$

Where: C = 0.8 (runoff coefficient, Ref 1.)
I = intensity, in/hr
A = drainage area, ac

$$I = \frac{b}{(t_c + d)^e}$$

b = 90 From Ref. 1, for Denton County
d = 8.5 25-year storm event
e = 0.781
 t_c is assumed to be 10 min.

$$I = 9.22 \text{ in/hr}$$

Area (ac)	Flow (cfs)
5.0	36.9
10.0	73.8
15.0	110.6
20.0	147.5
25.0	184.4
30.0	221.3
35.0	258.2

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1339-351-11-02-6B.6
EROSION CONTROL STRUCTURE DESIGN
GEOMEMBRANE-LINED CHUTE DESIGN

Uniform flow design for the geomembrane-lined chutes on 2% slope.

Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)	Froude Number	Velocity Head (ft)	Energy Head (ft)	Flow Area (sf)	Flow Top Width (ft)
36.9	0.02	0.01	2	2	8	0.40	10.60	3.100	1.75	2.14	3.48	9.58
73.8	0.02	0.01	2	2	8	0.60	13.49	3.276	2.83	3.42	5.47	10.38
110.6	0.02	0.01	2	2	8	0.75	15.45	3.378	3.71	4.46	7.16	11.01
147.5	0.02	0.01	2	2	8	0.89	16.97	3.451	4.48	5.37	8.69	11.55
184.4	0.02	0.01	2	2	8	1.01	18.23	3.506	5.16	6.17	10.12	12.04
221.3	0.02	0.01	2	2	8	1.12	19.31	3.552	5.79	6.91	11.46	12.48
258.2	0.02	0.01	2	2	8	1.22	20.26	3.590	6.38	7.60	12.75	12.88

Uniform flow design for the geomembrane-lined chutes on 4% slope.

Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)	Froude Number	Velocity Head (ft)	Energy Head (ft)	Flow Area (sf)	Flow Top Width (ft)
36.9	0.04	0.01	2	2	8	0.32	13.20	4.245	2.71	3.03	2.79	9.29
73.8	0.04	0.01	2	2	8	0.49	16.93	4.509	4.46	4.94	4.36	9.94
110.6	0.04	0.01	2	2	8	0.62	19.46	4.654	5.88	6.50	5.68	10.46
147.5	0.04	0.01	2	2	8	0.73	21.43	4.757	7.14	7.86	6.88	10.91
184.4	0.04	0.01	2	2	8	0.83	23.06	4.836	8.27	9.09	8.00	11.31
221.3	0.04	0.01	2	2	8	0.92	24.47	4.901	9.30	10.22	9.04	11.68
258.2	0.04	0.01	2	2	8	1.00	25.69	4.953	10.26	11.26	10.05	12.02

Uniform flow design for the geomembrane-lined chutes on 20% slope.

Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)	Froude Number	Velocity Head (ft)	Energy Head (ft)	Flow Area (sf)	Flow Top Width (ft)
36.9	0.20	0.01	2	2	8	0.20	21.92	8.839	7.47	7.67	1.68	8.80
73.8	0.20	0.01	2	2	8	0.30	28.35	9.401	12.49	12.79	2.60	9.21
110.6	0.20	0.01	2	2	8	0.38	32.88	9.760	16.80	17.79	3.36	9.53
147.5	0.20	0.01	2	2	8	0.45	36.41	9.992	20.60	21.05	4.05	9.82
184.4	0.20	0.01	2	2	8	0.52	39.35	10.171	24.06	24.58	4.69	10.07
221.3	0.20	0.01	2	2	8	0.58	41.90	10.318	27.28	27.85	5.28	10.31
258.2	0.20	0.01	2	2	8	0.63	44.15	10.441	30.29	30.92	5.85	10.53

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1339-351-11-02-6B.6
EROSION CONTROL STRUCTURE DESIGN
GEOMEMBRANE-LINED CHUTE DESIGN

Uniform flow design for the geomembrane-lined chutes on 25% slope.

Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)	Froude Number	Velocity Head (ft)	Energy Head (ft)	Flow Area (sf)	Flow Top Width (ft)
36.9	0.25	0.01	2	2	8	0.19	23.59	9.836	8.65	8.84	1.56	8.75
73.8	0.25	0.01	2	2	8	0.28	30.43	10.408	14.39	14.67	2.43	9.13
110.6	0.25	0.01	2	2	8	0.36	35.25	10.779	19.31	19.67	3.14	9.44
147.5	0.25	0.01	2	2	8	0.43	39.14	11.071	23.80	24.23	3.77	9.70
184.4	0.25	0.01	2	2	8	0.49	42.32	11.272	27.84	28.32	4.36	9.94
221.3	0.25	0.01	2	2	8	0.54	45.08	11.435	31.58	32.12	4.91	10.16
258.2	0.25	0.01	2	2	8	0.59	47.53	11.574	35.10	35.69	5.43	10.37

Conclusions: Maximum normal depth is 1.22 feet. Chute design depth is 2.0 feet; therefore, design is acceptable.

1. Calculations were performed using the HYDROCALC Hydraulics for Windows program developed by Dodson and Associates (Version 1.2a, 1996).

EROSION CONTROL STRUCTURE DESIGN
GABION, TURF REINFORCEMENT MAT, ROCK RIPRAP, OR GROUTED CONCRETE RIPRAP-LINED CHUTE DESIGN

Chute flow design for the gabion and rock riprap-lined chutes on 2% slope.

Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)	Froude Number	Velocity Head (ft)	Energy Head (ft)	Flow Area (sf)	Flow Top Width (ft)
36.9	0.02	0.04	2	2	8	0.89	4.24	0.863	0.28	1.17	8.69	11.56
73.8	0.02	0.04	2	2	8	1.32	5.28	0.906	0.43	1.75	13.99	13.26
110.6	0.02	0.04	2	2	8	1.64	5.96	0.931	0.55	2.20	18.56	14.58
147.5	0.02	0.04	2	2	8	1.92	6.48	0.949	0.65	2.57	22.76	15.69
184.4	0.02	0.04	2	2	8	2.16	6.91	0.962	0.74	2.91	26.69	16.66
221.3	0.02	0.04	2	2	8	2.38	7.28	0.974	0.82	3.21	30.42	17.53
258.2	0.02	0.04	2	2	8	2.58	7.60	0.983	0.90	3.48	33.99	18.33

Chute flow design for the gabion and rock riprap-lined chutes on 4% slope.

Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)	Froude Number	Velocity Head (ft)	Energy Head (ft)	Flow Area (sf)	Flow Top Width (ft)
36.9	0.04	0.04	2	2	8	0.73	5.36	1.189	0.45	1.17	6.89	10.91
73.8	0.04	0.04	2	2	8	1.08	6.70	1.251	0.70	1.78	11.01	12.33
110.6	0.04	0.04	2	2	8	1.36	7.60	1.286	0.90	2.26	14.56	13.43
147.5	0.04	0.04	2	2	8	1.59	8.28	1.311	1.07	2.66	17.81	14.37
184.4	0.04	0.04	2	2	8	1.80	8.84	1.331	1.22	3.01	20.85	15.19
221.3	0.04	0.04	2	2	8	1.98	9.32	1.347	1.35	3.33	23.73	15.93
258.2	0.04	0.04	2	2	8	2.15	9.74	1.360	1.48	3.63	26.50	16.61

Chute flow design for the gabion and rock riprap-lined chutes on 20% slope.

Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)	Froude Number	Velocity Head (ft)	Energy Head (ft)	Flow Area (sf)	Flow Top Width (ft)
36.9	0.20	0.04	2	2	8	0.45	9.10	2.498	1.29	1.74	4.05	9.82
73.8	0.20	0.04	2	2	8	0.68	11.55	2.637	2.07	2.75	6.39	10.73
110.6	0.20	0.04	2	2	8	0.86	13.19	2.718	2.70	3.57	8.38	11.45
147.5	0.20	0.04	2	2	8	1.02	14.46	2.774	3.25	4.27	10.20	12.07
184.4	0.20	0.04	2	2	8	1.15	15.52	2.819	3.74	4.90	11.88	12.61
221.3	0.20	0.04	2	2	8	1.28	16.42	2.854	4.19	5.47	13.48	13.11
258.2	0.20	0.04	2	2	8	1.39	17.21	2.885	4.60	5.99	15.00	13.57

EROSION CONTROL STRUCTURE DESIGN
GABION, TURF REINFORCEMENT MAT, ROCK RIPRAP, OR GROUTED CONCRETE RIPRAP-LINED CHUTE DESIGN

Chute flow design for the gabion and rock riprap-lined chutes on 25% slope.

Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)	Froude Number	Velocity Head (ft)	Energy Head (ft)	Flow Area (sf)	Flow Top Width (ft)
36.9	0.25	0.04	2	2	8	0.43	9.79	2.768	1.49	1.91	3.77	9.70
73.8	0.25	0.04	2	2	8	0.64	12.43	2.923	2.40	3.04	5.94	10.56
110.6	0.25	0.04	2	2	8	0.81	14.22	3.014	3.14	3.95	7.78	11.23
147.5	0.25	0.04	2	2	8	0.95	15.62	3.080	3.79	4.74	9.44	11.81
184.4	0.25	0.04	2	2	8	1.08	16.76	3.127	4.36	5.45	11.01	12.33
221.3	0.25	0.04	2	2	8	1.20	17.74	3.167	4.89	6.09	12.48	12.80
258.2	0.25	0.04	2	2	8	1.31	18.60	3.201	5.37	6.68	13.88	13.23

Conclusions: Maximum acceptable normal depth is 1.98 feet. Chute design depth is 2.0 feet; therefore, design is acceptable. Maximum velocity is 18.60 fps. As noted in footnote No. 2 below, the lining material will be selected so that the permissible velocity is not exceeded for erosion control. Maximum drainage area allowed on the top deck is 20 acres for a 2% slope and 30 acres for a 4% slope since the normal depth in chutes with these slopes is greater than 2.0 feet for larger drainage areas.

- Calculations were performed using the HYDROCALC Hydraulics for Windows program developed by Dodson and Associates (Version 1.2a, 1996).
- Permissible velocities are listed below, and lining material will be selected so that these are not exceeded.

Description	Permissible Velocity (fps)
Turf Reinforcement Mat (based on Pyramat or equivalent. Refer to Sheet 6B-D-2-6.)	25
Rock Riprap (based on Sheet III-F-2-20 and a D ₅₀ of 12 inches. If other riprap is used, it will meet the D ₅₀ requirements listed on Sheet III-F-2-7.)	9
Gabion/Concrete Grouted Riprap (based on Sheet III-F-2-21 and a D ₅₀ of 0.62 ft. If other gabion is used it will meet the D ₅₀ requirements listed on Sheet III-F-2-21. The permissible velocity for concrete grouted riprap will actually be greater than 21 fps because it is classified as a rigid channel lining material.	21

EROSION CONTROL STRUCTURE DESIGN
GABION, TURF REINFORCEMENT MAT, ROCK RIPRAP, OR GROUTED CONCRETE RIPRAP-LINED CHUTE DESIGN

Chute flow design for the grouted riprap and turf reinforcement-lined chutes on 2% slope.

Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)	Froude Number	Velocity Head (ft)	Energy Head (ft)	Flow Area (sf)	Flow Top Width (ft)
36.9	0.02	0.03	2	2	8	0.75	5.15	1.126	0.41	1.17	7.16	11.01
73.8	0.02	0.03	2	2	8	1.12	6.44	1.184	0.64	1.76	11.46	12.48
110.6	0.02	0.03	2	2	8	1.40	7.29	1.218	0.83	2.23	15.17	13.62
147.5	0.02	0.03	2	2	8	1.64	7.95	1.241	0.98	2.63	18.56	14.58
184.4	0.02	0.03	2	2	8	1.86	8.48	1.260	1.12	2.97	21.74	15.42
221.3	0.02	0.03	2	2	8	2.05	8.94	1.275	1.24	3.29	24.75	16.19
258.2	0.02	0.03	2	2	8	2.22	9.34	1.287	1.36	3.58	27.64	16.89

Chute flow design for the grouted riprap and turf reinforcement-lined chutes on 4% slope.

Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)	Froude Number	Velocity Head (ft)	Energy Head (ft)	Flow Area (sf)	Flow Top Width (ft)
36.9	0.04	0.03	2	2	8	0.62	6.49	1.551	0.65	1.27	5.69	10.46
73.8	0.04	0.03	2	2	8	0.92	8.16	1.634	1.03	1.95	9.05	11.68
110.6	0.04	0.03	2	2	8	1.16	9.27	1.681	1.34	2.49	11.93	12.63
147.5	0.04	0.03	2	2	8	1.36	10.13	1.715	1.59	2.95	14.56	13.44
184.4	0.04	0.03	2	2	8	1.54	10.83	1.741	1.82	3.36	17.02	14.15
221.3	0.04	0.03	2	2	8	1.70	11.43	1.762	2.03	3.73	19.35	14.79
258.2	0.04	0.03	2	2	8	1.85	11.96	1.780	2.22	4.07	21.59	15.38

Chute flow design for the grouted riprap and turf reinforcement-lined chutes on 20% slope.

Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)	Froude Number	Velocity Head (ft)	Energy Head (ft)	Flow Area (sf)	Flow Top Width (ft)
36.9	0.20	0.03	2	2	8	0.38	10.96	3.254	1.87	2.25	3.37	9.54
73.8	0.20	0.03	2	2	8	0.58	13.97	3.439	3.03	3.61	5.28	10.31
110.6	0.20	0.03	2	2	8	0.73	16.01	3.547	3.98	4.71	6.91	10.92
147.5	0.20	0.03	2	2	8	0.86	17.59	3.624	4.81	5.67	8.39	11.45
184.4	0.20	0.03	2	2	8	0.98	18.90	3.684	5.55	6.53	9.75	11.92
221.3	0.20	0.03	2	2	8	1.09	20.02	3.730	6.23	7.32	11.05	12.35
258.2	0.20	0.03	2	2	8	1.19	21.01	3.771	6.86	8.04	12.29	12.74

EROSION CONTROL STRUCTURE DESIGN
GABION, TURF REINFORCEMENT MAT, ROCK RIPRAP, OR GROUDED CONCRETE RIPRAP-LINED CHUTE DESIGN

Chute flow design for the grouted riprap and turf reinforcement-lined chutes on 25% slope.

Flow Rate (cfs)	Bottom Slope (ft/ft)	Manning's n	Side Slope (left)	Side Slope (right)	Bottom Width (ft)	Normal Depth (ft)	Flow Vel. (fps)	Froude Number	Velocity Head (ft)	Energy Head (ft)	Flow Area (sf)	Flow Top Width (ft)
36.9	0.25	0.03	2	2	8	0.36	11.75	3.593	2.15	2.51	3.14	9.44
73.8	0.25	0.03	2	2	8	0.54	15.03	3.812	3.51	4.05	4.91	10.16
110.6	0.25	0.03	2	2	8	0.68	17.24	3.933	4.62	5.30	6.41	10.74
147.5	0.25	0.03	2	2	8	0.81	18.96	4.018	5.59	6.40	7.78	11.23
184.4	0.25	0.03	2	2	8	0.92	20.39	4.084	6.46	7.38	9.04	11.68
221.3	0.25	0.03	2	2	8	1.02	21.61	4.137	7.25	8.27	10.24	12.08
258.2	0.25	0.03	2	2	8	1.11	22.69	4.138	8.00	9.11	11.38	12.45

Conclusions: Maximum acceptable normal depth is 1.86 feet. Chute design depth is 2.0 feet; therefore, design is acceptable. Maximum velocity is 22.69 fps. As noted in footnote No. 2 below, the lining material will be selected so that the permissible velocity is not exceeded for erosion control.
Maximum drainage area allowed on the top deck is 25 acres for a 2% slope since the normal depth in chutes with this slope is greater than 2.0 feet for larger drainage areas.

- Calculations were performed using the HYDROCALC Hydraulics for Windows program developed by Dodson and Associates (Version 1.2a, 1996).
- Permissible velocities are listed below, and lining material will be selected so that these are not exceeded.

Description	Permissible Velocity (fps)
Turf Reinforcement Mat (based on Pyramat or equivalent. Refer to Sheet III-F-2-19.)	25
Rock Riprap (based on Sheet III-F-2-20 and a D_{50} of 12 inches. If other riprap is used, it will meet the D_{50} requirements listed on Sheet III-F-2-20.)	9
Gabion/Concrete Grouted Riprap (based on Sheet III-F-2-21 and a D_{50} of 0.62 ft. If other gabion is used, it will meet the D_{50} requirements listed on Sheet III-F-2-21. The permissible velocity for concrete grouted riprap will actually be greater than 21 fps because it is classified as a rigid channel lining material.)	21

CAMELOT LANDFILL
1339-351-11-02-6B.6
OPEN CHANNEL LETDOWN
RIPRAP EROSION PROTECTION DESIGN

Required: Design the riprap erosion protection at the downstream end of the open channel letdown.

Method: Use HEC-RAS to model the open channel geomembrane-lined letdown to determine the hydraulic characteristics of the hydraulic jump that will occur at the downstream end of the letdown. Based on the results, design the riprap erosion protection area.

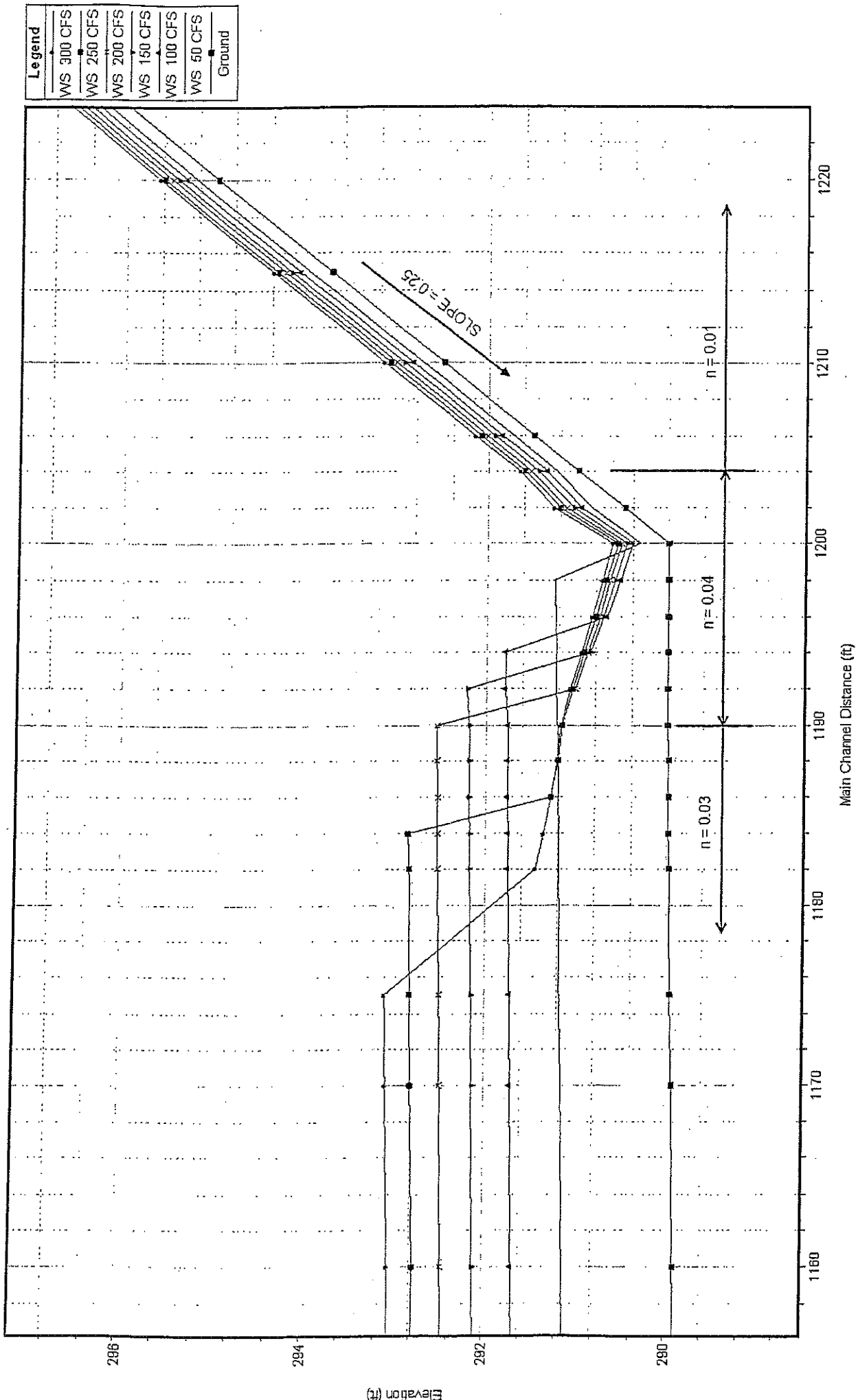
Note: This example calculation is shown for geomembrane-lined letdowns to conservatively estimate the length of riprap needed. As seen on pages III F-F-2-3 through III F-F-2-8, the geomembrane-lined letdowns have the highest velocities and represent the worst-case scenario. Therefore, this riprap design is applicable to all lined letdowns.

Solution: Page III F-F-2-10 shows the water surface profile for incremental flows up to 300 cfs for the geomembrane letdown into a channel, as modeled in HEC-RAS. The modeling output is presented on pages III F-F-2-11 through III F-F-2-21. The following table summarizes the erosion protection design for the various flows.

Flow (cfs)	Drainage Area* (ac)	Length of Hydraulic Jump (ft)	Specified Runout of Riprap (ft)
50	5	2	10
100	10	6	10
150	15	8	10
200	20	10	10
250	30	16	16
300	35	25	25

* Drainage areas are approximated based on corresponding flows/drainage areas listed on page III F-F-2-2.

The values listed in the above table are specified riprap lengths for letdowns terminating into a perimeter channel. If the letdown terminates into a pond, 10 feet of riprap erosion control will be sufficient because the water in the pond will provide additional energy dissipation.



III-F-2-10

HEC-RAS Version 4.0.0 March 2008
 U.S. Army Corps of Engineers
 Hydrologic Engineering Center
 609 Second Street
 Davis, California

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X   X   XXXXXX   XXXX   XXXX   XX   XXXX
X   X   X       X   X       X   X   X   X   X
X   X   X       X       X   X   X   X   X
XXXXXXXX XXXX   X       XXX XXXX XXXXXXX XXXX
X   X   X       X       X   X   X   X   X
X   X   X       X   X       X   X   X   X   X
X   X   XXXXXX   XXXX   X   X   X   X   XXXXX
  
```

PROJECT DATA

Project Title: Hydraulic Jump
 Project File : HydraulicJump.prj
 Run Date and Time: 12/16/2009 3:52:23 PM

Project in English units

PLAN DATA

Plan Title: RUNUP 0.34
 Plan File : s:\Chuck\HEC-RAS\HydraulicJump.p07
 Geometry Title: FML CHUTE with 4' RUNUP .003
 Geometry File : s:\Chuck\HEC-RAS\HydraulicJump.g07
 Flow Title : FML CHUTE 0.34
 Flow File : s:\Chuck\HEC-RAS\HydraulicJump.f03

Plan Summary Information:
 Number of: Cross Sections = 36 Multiple Openings = 0
 Culverts = 0 Inline Structures = 0
 Bridges = 0 Lateral Structures = 0

Computational Information
 Water surface calculation tolerance = 0.01
 Critical depth calculation tolerance = 0.01
 Maximum number of iterations = 20
 Maximum difference tolerance = 0.3
 Flow tolerance factor = 0.001

Computation Options
 Critical depth computed only where necessary
 Conveyance Calculation Method: At breaks in n values only
 Friction Slope Method: Average Conveyance
 Computational Flow Regime: Mixed Flow

FLOW DATA

Flow Title: FML CHUTE 0.34
 Flow File : s:\Chuck\HEC-RAS\HydraulicJump.f03

Flow Data (cfs)

River	Reach	RS	50 CFS	100 CFS	150 CFS	200 CFS	250 CFS	300 CFS
LF	FML Chute	5000	50	100	150	200	250	300

Boundary Conditions

River	Reach	Profile	Upstream	Downstream
LF	FML Chute	50 CFS	Normal S = 0.25	Normal S = 0.003
LF	FML Chute	100 CFS	Normal S = 0.25	Normal S = 0.003
LF	FML Chute	150 CFS	Normal S = 0.25	Normal S = 0.003
LF	FML Chute	200 CFS	Normal S = 0.25	Normal S = 0.003
LF	FML Chute	250 CFS	Normal S = 0.25	Normal S = 0.003
LF	FML Chute	300 CFS	Normal S = 0.25	Normal S = 0.003

GEOMETRY DATA

Geometry Title: FML CHUTE with 4' RUNUP .003
 Geometry File : s:\Chuck\HEC-RAS\HydraulicJump.g07

CROSS SECTION

RIVER: LF
 REACH: FML Chute RS: 5000

INPUT

Description:
 Station Elevation Data num= 4

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	500	20	490	28	490	48	500

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.01	0	.01	48	.01

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.

Left	Right	Left	Channel	Right	Coeff Contr.	Expan.
0	48	100	100	100	.1	.5

CROSS SECTION

RIVER: LF
 REACH: FML Chute RS: 4900

INPUT

Description:
 Station Elevation Data num= 4
 Sta Elev Sta Elev Sta Elev Sta Elev
 0 475 20 465 28 465 48 475

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 0 .01 0 .01 48 .01

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 48 100 100 100 .1 .5

CROSS SECTION

RIVER: LF
 REACH: FML Chute RS: 4800

INPUT

Description:
 Station Elevation Data num= 4
 Sta Elev Sta Elev Sta Elev Sta Elev
 0 450 20 440 28 440 48 450

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 0 .01 0 .01 48 .01

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 48 100 100 100 .1 .5

CROSS SECTION

RIVER: LF
 REACH: FML Chute RS: 4700

INPUT

Description:
 Station Elevation Data num= 4
 Sta Elev Sta Elev Sta Elev Sta Elev
 0 425 20 415 28 415 48 425

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 0 .01 0 .01 48 .01

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 48 100 100 100 .1 .5

CROSS SECTION

RIVER: LF
 REACH: FML Chute RS: 4600

INPUT

Description:
 Station Elevation Data num= 4
 Sta Elev Sta Elev Sta Elev Sta Elev
 0 400 20 390 28 390 48 400

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 0 .01 0 .01 48 .01

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 48 100 100 100 .1 .5

CROSS SECTION

RIVER: LF
 REACH: FML Chute RS: 4500

INPUT

Description:
 Station Elevation Data num= 4
 Sta Elev Sta Elev Sta Elev Sta Elev
 0 375 20 365 28 365 48 375

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 0 .01 0 .01 48 .01

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 48 100 100 100 .1 .5

CROSS SECTION

RIVER: LF
 REACH: FML Chute RS: 4400

INPUT

Description:
 Station Elevation Data num= 4
 Sta Elev Sta Elev Sta Elev Sta Elev
 0 350 20 340 28 340 48 350

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 0 .01 0 .01 48 .01

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 48 100 100 100 .1 .5

CROSS SECTION

RIVER: LF
 REACH: FML Chute RS: 4300

INPUT

Description:

Station Elevation Data		num=		4		Sta		Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	325	20	315	28	315	48	325		

Manning's n Values

num=		3		Sta		n Val	
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.01	0	.01	48	.01		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	0	48		75	75	.1	.5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4225

INPUT

Description:

Station Elevation Data		num=		4		Sta		Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	306.25	20	296.25	28	296.25	48	306.25		

Manning's n Values

num=		3		Sta		n Val	
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.01	0	.01	48	.01		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	0	48		5	5	.1	.5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4220

INPUT

Description:

Station Elevation Data		num=		4		Sta		Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	305	20	295	28	295	48	305		

Manning's n Values

num=		3		Sta		n Val	
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.01	0	.01	48	.01		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	0	48		5	5	.1	.5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4215

INPUT

Description:

Station Elevation Data		num=		4		Sta		Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	303.75	20	293.75	28	293.75	48	303.75		

Manning's n Values

num=		3		Sta		n Val	
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.01	0	.01	48	.01		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	0	48		5	5	.1	.5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4210

INPUT

Description:

Station Elevation Data		num=		4		Sta		Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	302.5	20	292.5	28	292.5	48	302.5		

Manning's n Values

num=		3		Sta		n Val	
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.01	0	.01	48	.01		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	0	48		4	4	.1	.5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4206

INPUT

Description:

Station Elevation Data		num=		4		Sta		Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	301.5	20	291.5	28	291.5	48	301.5		

Manning's n Values

num=		3		Sta		n Val	
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.01	0	.01	48	.01		

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	0	48		2	2	.1	.5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4204

INPUT

Description:

Station Elevation Data num= 4
 Sta Elev Sta Elev Sta Elev Sta Elev
 0 301 20 291 28 291 48 301

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 0 .04 0 .04 48 .04

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 48 2 2 2 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4202

INPUT

Description:

Station Elevation Data num= 4
 Sta Elev Sta Elev Sta Elev Sta Elev
 0 300.5 20 290.5 28 290.5 48 300.5

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 0 .04 0 .04 48 .04

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 48 2 2 2 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4200

INPUT

Description:

Station Elevation Data num= 4
 Sta Elev Sta Elev Sta Elev Sta Elev
 0 300 30 290 42 290 72 300

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 0 .04 0 .04 72 .04

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 72 2 2 2 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4198

INPUT

Description:

Station Elevation Data num= 4
 Sta Elev Sta Elev Sta Elev Sta Elev
 0 300 30 290 42 290 72 300

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 0 .04 0 .04 72 .04

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 72 2 2 2 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4196

INPUT

Description:

Station Elevation Data num= 4
 Sta Elev Sta Elev Sta Elev Sta Elev
 0 300 30 290 42 290 72 300

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 0 .04 0 .04 72 .04

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 72 2 2 2 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4194

INPUT

Description:

Station Elevation Data num= 4
 Sta Elev Sta Elev Sta Elev Sta Elev
 0 300 30 290 42 290 72 300

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 0 .04 0 .04 72 .04

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 72 2 2 2 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4192

INPUT

Description:

Station Elevation Data		num=		4		Sta		Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	300	30	290	42	290	72	300		

Manning's n Values

num=		3		Sta		n Val	
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.04	0	.04	72	.04		

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 72 2 2 2 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4190

INPUT

Description:

Station Elevation Data		num=		4		Sta		Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	310	60	290	72	290	132	310		

Manning's n Values

num=		3		Sta		n Val	
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.03	0	.03	72	.03		

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 72 2 2 2 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4188

INPUT

Description:

Station Elevation Data		num=		4		Sta		Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	309.994	60	289.994	72	289.994	132	309.994		

Manning's n Values

num=		3		Sta		n Val	
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.03	0	.03	132	.03		

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 132 2 2 2 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4186

INPUT

Description:

Station Elevation Data		num=		4		Sta		Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	309.988	60	289.988	72	289.988	132	309.988		

Manning's n Values

num=		3		Sta		n Val	
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.03	0	.03	132	.03		

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 132 2 2 2 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4184

INPUT

Description:

Station Elevation Data		num=		4		Sta		Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	309.982	60	289.982	72	289.982	132	309.982		

Manning's n Values

num=		3		Sta		n Val	
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.03	0	.03	132	.03		

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 132 2 2 2 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4182

INPUT

Description:

Station Elevation Data		num=		4		Sta		Elev	
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	309.976	60	289.976	72	289.976	132	309.976		

Manning's n Values

num=		3		Sta		n Val	
Sta	n Val	Sta	n Val	Sta	n Val	Sta	n Val
0	.03	0	.03	132	.03		

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 132 7 7 7 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4175

INPUT

Description:

Station Elevation Data num= 4
Sta Elev Sta Elev Sta Elev Sta Elev
0 309.955 60 289.955 72 289.955 132 309.955

Manning's n Values

num= 3
Sta n Val Sta n Val Sta n Val
0 .03 0 .03 132 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
0 132 5 5 5 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4170

INPUT

Description:

Station Elevation Data num= 4
Sta Elev Sta Elev Sta Elev Sta Elev
0 309.94 60 289.94 72 289.94 132 309.94

Manning's n Values

num= 3
Sta n Val Sta n Val Sta n Val
0 .03 0 .03 132 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
0 132 10 10 10 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4160

INPUT

Description:

Station Elevation Data num= 4
Sta Elev Sta Elev Sta Elev Sta Elev
0 309.91 60 289.91 72 289.91 132 309.91

Manning's n Values

num= 3
Sta n Val Sta n Val Sta n Val
0 .03 0 .03 132 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
0 132 10 10 10 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4150

INPUT

Description:

Station Elevation Data num= 4
Sta Elev Sta Elev Sta Elev Sta Elev
0 309.88 60 289.88 72 289.88 132 309.88

Manning's n Values

num= 3
Sta n Val Sta n Val Sta n Val
0 .03 0 .03 132 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
0 132 10 10 10 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4140

INPUT

Description:

Station Elevation Data num= 4
Sta Elev Sta Elev Sta Elev Sta Elev
0 309.85 60 289.85 72 289.85 132 309.85

Manning's n Values

num= 3
Sta n Val Sta n Val Sta n Val
0 .03 0 .03 132 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
0 132 10 10 10 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4130

INPUT

Description:

Station Elevation Data num= 4
Sta Elev Sta Elev Sta Elev Sta Elev
0 309.82 60 289.82 72 289.82 132 309.82

Manning's n Values

num= 3
Sta n Val Sta n Val Sta n Val
0 .03 0 .03 132 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
0 132 10 10 10 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4120

INPUT

Description:

Station Elevation Data num= 4
 Sta Elev Sta Elev Sta Elev Sta Elev
 0 309.79 60 289.79 72 289.79 132 309.79

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 0 .03 0 .03 132 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 132 10 10 10 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4110

INPUT

Description:

Station Elevation Data num= 4
 Sta Elev Sta Elev Sta Elev Sta Elev
 0 309.76 60 289.76 72 289.76 132 309.76

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 0 .03 0 .03 132 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 132 10 10 10 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4100

INPUT

Description:

Station Elevation Data num= 4
 Sta Elev Sta Elev Sta Elev Sta Elev
 0 309.73 60 289.73 72 289.73 132 309.73

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 0 .03 0 .03 132 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 132 100 100 100 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 4000

INPUT

Description:

Station Elevation Data num= 4
 Sta Elev Sta Elev Sta Elev Sta Elev
 0 309.43 60 289.43 72 289.43 132 309.43

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 0 .03 0 .03 132 .03

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.
 0 132 1000 1000 1000 .1 .5

CROSS SECTION

RIVER: LF

REACH: FML Chute RS: 3000

INPUT

Description:

Station Elevation Data num= 4
 Sta Elev Sta Elev Sta Elev Sta Elev
 0 306.43 60 286.43 72 286.43 132 306.43

Manning's n Values num= 3
 Sta n Val Sta n Val Sta n Val
 0 .03 0 .03 132 .03

Bank Sta: Left Right Coeff Contr. Expan.
 0 132 .1 .5

SUMMARY OF MANNING'S N VALUES

River: LF

Reach	River Sta.	n1	n2	n3
FML Chute	5000	.01	.01	.01
FML Chute	4900	.01	.01	.01
FML Chute	4800	.01	.01	.01
FML Chute	4700	.01	.01	.01
FML Chute	4600	.01	.01	.01
FML Chute	4500	.01	.01	.01
FML Chute	4400	.01	.01	.01
FML Chute	4300	.01	.01	.01
FML Chute	4225	.01	.01	.01
FML Chute	4220	.01	.01	.01
FML Chute	4215	.01	.01	.01
FML Chute	4210	.01	.01	.01
FML Chute	4206	.01	.01	.01
FML Chute	4204	.04	.04	.04
FML Chute	4202	.04	.04	.04
FML Chute	4200	.04	.04	.04

FML Chute	4198	.04	.04	.04
FML Chute	4196	.04	.04	.04
FML Chute	4194	.04	.04	.04
FML Chute	4192	.04	.04	.04
FML Chute	4190	.03	.03	.03
FML Chute	4188	.03	.03	.03
FML Chute	4186	.03	.03	.03
FML Chute	4184	.03	.03	.03
FML Chute	4182	.03	.03	.03
FML Chute	4175	.03	.03	.03
FML Chute	4170	.03	.03	.03
FML Chute	4160	.03	.03	.03
FML Chute	4150	.03	.03	.03
FML Chute	4140	.03	.03	.03
FML Chute	4130	.03	.03	.03
FML Chute	4120	.03	.03	.03
FML Chute	4110	.03	.03	.03
FML Chute	4100	.03	.03	.03
FML Chute	4000	.03	.03	.03
FML Chute	3000	.03	.03	.03

SUMMARY OF REACH LENGTHS

River: LF

Reach	River Sta.	Left	Channel	Right
FML Chute	5000	100	100	100
FML Chute	4900	100	100	100
FML Chute	4800	100	100	100
FML Chute	4700	100	100	100
FML Chute	4600	100	100	100
FML Chute	4500	100	100	100
FML Chute	4400	100	100	100
FML Chute	4300	75	75	75
FML Chute	4225	5	5	5
FML Chute	4220	5	5	5
FML Chute	4215	5	5	5
FML Chute	4210	4	4	4
FML Chute	4206	2	2	2
FML Chute	4204	2	2	2
FML Chute	4202	2	2	2
FML Chute	4200	2	2	2
FML Chute	4198	2	2	2
FML Chute	4196	2	2	2
FML Chute	4194	2	2	2
FML Chute	4192	2	2	2
FML Chute	4190	2	2	2
FML Chute	4188	2	2	2
FML Chute	4186	2	2	2
FML Chute	4184	2	2	2
FML Chute	4182	7	7	7
FML Chute	4175	5	5	5
FML Chute	4170	10	10	10
FML Chute	4160	10	10	10
FML Chute	4150	10	10	10
FML Chute	4140	10	10	10
FML Chute	4130	10	10	10
FML Chute	4120	10	10	10
FML Chute	4110	10	10	10
FML Chute	4100	100	100	100
FML Chute	4000	1000	1000	1000
FML Chute	3000			

SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS

River: LF

Reach	River Sta.	Contr.	Expan.
FML Chute	5000	.1	.5
FML Chute	4900	.1	.5
FML Chute	4800	.1	.5
FML Chute	4700	.1	.5
FML Chute	4600	.1	.5
FML Chute	4500	.1	.5
FML Chute	4400	.1	.5
FML Chute	4300	.1	.5
FML Chute	4225	.1	.5
FML Chute	4220	.1	.5
FML Chute	4215	.1	.5
FML Chute	4210	.1	.5
FML Chute	4206	.1	.5
FML Chute	4204	.1	.5
FML Chute	4202	.1	.5
FML Chute	4200	.1	.5
FML Chute	4198	.1	.5
FML Chute	4196	.1	.5
FML Chute	4194	.1	.5
FML Chute	4192	.1	.5
FML Chute	4190	.1	.5
FML Chute	4188	.1	.5
FML Chute	4186	.1	.5
FML Chute	4184	.1	.5
FML Chute	4182	.1	.5
FML Chute	4175	.1	.5
FML Chute	4170	.1	.5
FML Chute	4160	.1	.5
FML Chute	4150	.1	.5
FML Chute	4140	.1	.5
FML Chute	4130	.1	.5
FML Chute	4120	.1	.5
FML Chute	4110	.1	.5
FML Chute	4100	.1	.5
FML Chute	4000	.1	.5
FML Chute	3000	.1	.5

Profile Output Table - Standard Table 1

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
FML Chute	5000	50 CFS	50.00	490.00	490.22	490.98	500.99	0.250200	26.33	1.90	8.90	10.05
FML Chute	5000	100 CFS	100.00	490.00	490.34	491.48	508.27	0.250152	33.98	2.94	9.36	10.68
FML Chute	5000	150 CFS	150.00	490.00	490.43	491.87	514.41	0.250103	39.30	3.82	9.72	11.05
FML Chute	5000	200 CFS	200.00	490.00	490.51	492.21	519.86	0.250072	43.47	4.60	10.04	11.32
FML Chute	5000	250 CFS	250.00	490.00	490.58	492.50	524.82	0.250092	46.96	5.32	10.32	11.52
FML Chute	5000	300 CFS	300.00	490.00	490.65	492.77	529.41	0.250044	49.96	6.00	10.58	11.69
FML Chute	4900	50 CFS	50.00	465.00	465.98	465.98	466.39	0.001647	5.14	9.73	11.91	1.00
FML Chute	4900	100 CFS	100.00	465.00	465.34	466.48	483.26	0.249924	33.97	2.94	9.36	10.67
FML Chute	4900	150 CFS	150.00	465.00	465.43	466.87	489.40	0.249922	39.29	3.82	9.72	11.05
FML Chute	4900	200 CFS	200.00	465.00	465.51	467.21	494.84	0.249919	43.46	4.60	10.04	11.31
FML Chute	4900	250 CFS	250.00	465.00	465.58	467.50	499.80	0.249911	46.95	5.32	10.32	11.52
FML Chute	4900	300 CFS	300.00	465.00	465.65	467.77	504.40	0.250003	49.96	6.00	10.58	11.69
FML Chute	4800	50 CFS	50.00	440.00	440.16	440.98	463.50	0.867039	38.77	1.29	8.62	17.67
FML Chute	4800	100 CFS	100.00	440.00	440.34	441.48	458.26	0.249924	33.97	2.94	9.36	10.67
FML Chute	4800	150 CFS	150.00	440.00	440.43	441.87	464.40	0.249922	39.29	3.82	9.72	11.05
FML Chute	4800	200 CFS	200.00	440.00	440.51	442.21	469.85	0.249970	43.47	4.60	10.04	11.32
FML Chute	4800	250 CFS	250.00	440.00	440.58	442.50	474.80	0.249911	46.95	5.32	10.32	11.52
FML Chute	4800	300 CFS	300.00	440.00	440.65	442.77	479.40	0.250003	49.96	6.00	10.58	11.69
FML Chute	4700	50 CFS	50.00	415.00	415.25	415.98	423.63	0.167904	23.23	2.15	9.01	8.38
FML Chute	4700	100 CFS	100.00	415.00	415.34	416.48	433.27	0.250000	33.98	2.94	9.36	10.68
FML Chute	4700	150 CFS	150.00	415.00	415.43	416.87	439.41	0.250043	39.29	3.82	9.72	11.05
FML Chute	4700	200 CFS	200.00	415.00	415.51	417.21	444.85	0.249970	43.47	4.60	10.04	11.32
FML Chute	4700	250 CFS	250.00	415.00	415.58	417.50	449.81	0.249956	46.95	5.32	10.32	11.52
FML Chute	4700	300 CFS	300.00	415.00	415.65	417.77	454.40	0.250003	49.96	6.00	10.58	11.69
FML Chute	4600	50 CFS	50.00	390.00	390.22	390.98	401.86	0.281536	27.38	1.83	8.87	10.63
FML Chute	4600	100 CFS	100.00	390.00	390.34	391.48	408.27	0.250000	33.98	2.94	9.36	10.68
FML Chute	4600	150 CFS	150.00	390.00	390.43	391.87	414.41	0.250043	39.29	3.82	9.72	11.05
FML Chute	4600	200 CFS	200.00	390.00	390.51	392.21	419.85	0.249970	43.47	4.60	10.04	11.32
FML Chute	4600	250 CFS	250.00	390.00	390.58	392.50	424.82	0.250046	46.95	5.32	10.32	11.52
FML Chute	4600	300 CFS	300.00	390.00	390.65	392.77	429.40	0.250003	49.96	6.00	10.58	11.69
FML Chute	4500	50 CFS	50.00	365.00	365.23	365.98	375.54	0.233381	25.76	1.94	8.92	9.73
FML Chute	4500	100 CFS	100.00	365.00	365.34	366.48	383.27	0.250000	33.98	2.94	9.36	10.68
FML Chute	4500	150 CFS	150.00	365.00	365.43	366.87	389.41	0.250043	39.29	3.82	9.72	11.05
FML Chute	4500	200 CFS	200.00	365.00	365.51	367.21	394.85	0.249970	43.47	4.60	10.04	11.32
FML Chute	4500	250 CFS	250.00	365.00	365.58	367.50	399.82	0.250046	46.95	5.32	10.32	11.52
FML Chute	4500	300 CFS	300.00	365.00	365.65	367.77	404.40	0.250003	49.96	6.00	10.58	11.69
FML Chute	4400	50 CFS	50.00	340.00	340.22	340.98	351.11	0.254706	26.48	1.89	8.89	10.13
FML Chute	4400	100 CFS	100.00	340.00	340.34	341.48	358.27	0.250000	33.98	2.94	9.36	10.68
FML Chute	4400	150 CFS	150.00	340.00	340.43	341.87	364.41	0.250043	39.29	3.82	9.72	11.05
FML Chute	4400	200 CFS	200.00	340.00	340.51	342.21	369.85	0.249970	43.47	4.60	10.04	11.32
FML Chute	4400	250 CFS	250.00	340.00	340.58	342.50	374.82	0.250046	46.95	5.32	10.32	11.52
FML Chute	4400	300 CFS	300.00	340.00	340.65	342.77	379.40	0.250003	49.96	6.00	10.58	11.69
FML Chute	4300	50 CFS	50.00	315.00	315.23	315.98	325.92	0.247365	26.24	1.91	8.90	9.99
FML Chute	4300	100 CFS	100.00	315.00	315.34	316.48	333.27	0.250000	33.98	2.94	9.36	10.68
FML Chute	4300	150 CFS	150.00	315.00	315.43	316.87	339.41	0.250043	39.29	3.82	9.72	11.05
FML Chute	4300	200 CFS	200.00	315.00	315.51	317.21	344.85	0.249970	43.47	4.60	10.04	11.32
FML Chute	4300	250 CFS	250.00	315.00	315.58	317.50	349.82	0.250046	46.95	5.32	10.32	11.52
FML Chute	4300	300 CFS	300.00	315.00	315.65	317.77	354.40	0.250003	49.96	6.00	10.58	11.69
FML Chute	4225	50 CFS	50.00	296.25	296.47	297.23	307.24	0.250314	26.34	1.90	8.90	10.05
FML Chute	4225	100 CFS	100.00	296.25	296.59	297.73	314.52	0.250000	33.98	2.94	9.36	10.68
FML Chute	4225	150 CFS	150.00	296.25	296.68	298.12	320.66	0.250043	39.29	3.82	9.72	11.05
FML Chute	4225	200 CFS	200.00	296.25	296.76	298.46	326.91	0.249970	43.47	4.60	10.04	11.32
FML Chute	4225	250 CFS	250.00	296.25	296.83	298.75	331.07	0.250046	46.95	5.32	10.32	11.52
FML Chute	4225	300 CFS	300.00	296.25	296.90	299.02	335.65	0.250003	49.96	6.00	10.58	11.69
FML Chute	4220	50 CFS	50.00	295.00	295.22	295.98	305.99	0.250314	26.34	1.90	8.90	10.05
FML Chute	4220	100 CFS	100.00	295.00	295.34	296.48	313.27	0.250000	33.98	2.94	9.36	10.68
FML Chute	4220	150 CFS	150.00	295.00	295.43	296.87	319.41	0.250043	39.29	3.82	9.72	11.05
FML Chute	4220	200 CFS	200.00	295.00	295.51	297.21	324.85	0.249970	43.47	4.60	10.04	11.32
FML Chute	4220	250 CFS	250.00	295.00	295.58	297.50	329.82	0.250046	46.95	5.32	10.32	11.52
FML Chute	4220	300 CFS	300.00	295.00	295.65	297.77	334.40	0.250003	49.96	6.00	10.58	11.69
FML Chute	4215	50 CFS	50.00	293.75	293.97	294.73	304.74	0.250314	26.34	1.90	8.90	10.05
FML Chute	4215	100 CFS	100.00	293.75	294.09	295.23	312.02	0.250000	33.98	2.94	9.36	10.68
FML Chute	4215	150 CFS	150.00	293.75	294.18	295.62	318.16	0.250043	39.29	3.82	9.72	11.05
FML Chute	4215	200 CFS	200.00	293.75	294.26	295.96	323.60	0.249970	43.47	4.60	10.04	11.32
FML Chute	4215	250 CFS	250.00	293.75	294.33	296.25	328.57	0.250046	46.95	5.32	10.32	11.52
FML Chute	4215	300 CFS	300.00	293.75	294.40	296.52	333.15	0.250003	49.96	6.00	10.58	11.69
FML Chute	4210	50 CFS	50.00	292.50	292.72	293.48	303.49	0.250314	26.34	1.90	8.90	10.05
FML Chute	4210	100 CFS	100.00	292.50	292.84	293.98	310.77	0.250000	33.98	2.94	9.36	10.68
FML Chute	4210	150 CFS	150.00	292.50	292.93	294.37	316.91	0.250043	39.29	3.82	9.72	11.05
FML Chute	4210	200 CFS	200.00	292.50	293.01	294.71	321.35	0.249970	43.47	4.60	10.04	11.32
FML Chute	4210	250 CFS	250.00	292.50	293.08	295.00	327.32	0.250046	46.95	5.32	10.32	11.52
FML Chute	4210	300 CFS	300.00	292.50	293.15	295.27	331.90	0.250003	49.96	6.00	10.58	11.69
FML Chute	4206	50 CFS	50.00	291.50	291.72	292.48	302.49	0.250314	26.34	1.90	8.90	10.05
FML Chute	4206	100 CFS	100.00	291.50	291.84	292.98	309.77	0.250000	33.98	2.94	9.36	10.68
FML Chute	4206	150 CFS	150.00	291.50	291.93	293.37	315.91	0.250043	39.29	3.82	9.72	11.05
FML Chute	4206	200 CFS	200.00	291.50	292.01	293.71	321.33	0.249766	43.46	4.60	10.04	11.31
FML Chute	4206	250 CFS	250.00	291.50	292.08	294.00	326.32	0.250046	46.95	5.32	10.32	11.52
FML Chute	4206	300 CFS	300.00	291.50	292.15	294.27	330.90	0.250003	49.96	6.00	10.58	11.69
FML Chute	4204	50 CFS	50.00	291.00	291.24	291.98	300.54	3.168811	24.47	2.04	8.96	9.03
FML Chute	4204	100 CFS	100.00	291.00	291.35	292.48	307.76	3.483119	32.51	3.08	9.41	10.02
FML Chute	4204	150 CFS	150.00	291.00	291.44	292.87	313.89	3.611811	38.02	3.95	9.78	10.55
FML Chute	4204	200 CFS	200.00	291.00	291.52	293.21	319.31	3.680328	42.30	4.73	10.09	10.89
FML Chute	4204	250 CFS	250.00	291.00	291.59	293.50	324.29	3.729970	45.88	5.45	10.37	11.16
FML Chute	4204	300 CFS	300.00	291.00	291.66	293.77	328.87	3.761746	48.95	6.13	10.63	11.36
FML Chute	4202	50 CFS	50.00	290.50	290.85	291.48	294.95	0.867986	16.24	4.18	9.41	5.00
FML Chute	4202	100 CFS	100.00	290.50	291.07	291.98	299.92	1.358543	24.01	3.06	9.86	6.51
FML Chute	4202	150 CFS	150.00	290.50	291.05	292.37	304.74	1.689534	29.65	5.05	10.22	7.44
FML Chute	4202	200 CFS	200.00	290.50	291.13	292.71	309.32	1.929858	34.22	5.84	10.52	8.09

FML Chute	4200	250 CFS	250.00	290.00	290.57	291.99	306.39	1.851131	31.91	7.83	15.43	7.89
FML Chute	4200	300 CFS	300.00	290.00	290.62	292.21	309.82	2.054209	35.16	8.53	15.70	8.40
FML Chute	4198	50 CFS	50.00	290.00	291.26	290.76	291.36	0.004652	2.52	19.82	19.54	0.44
FML Chute	4198	100 CFS	100.00	290.00	290.53	291.17	293.48	0.373613	13.77	7.26	15.20	3.51
FML Chute	4198	150 CFS	150.00	290.00	290.59	291.48	295.84	0.589034	18.39	8.16	15.55	4.48
FML Chute	4198	200 CFS	200.00	290.00	290.64	291.75	298.40	0.789548	22.35	8.95	15.86	5.24
FML Chute	4198	250 CFS	250.00	290.00	290.69	291.59	301.04	0.971954	25.82	9.68	16.13	5.87
FML Chute	4198	300 CFS	300.00	290.00	290.73	292.21	303.72	1.136831	28.92	10.37	16.39	6.41
FML Chute	4196	50 CFS	50.00	290.00	291.25	291.17	291.35	0.004810	2.55	19.59	19.47	0.45
FML Chute	4196	100 CFS	100.00	290.00	290.58	291.17	292.39	0.153054	10.49	9.53	16.07	2.40
FML Chute	4196	150 CFS	150.00	290.00	290.72	291.48	294.10	0.301701	14.75	10.17	16.31	3.29
FML Chute	4196	200 CFS	200.00	290.00	290.76	291.75	296.00	0.436547	18.37	10.89	16.57	3.99
FML Chute	4196	250 CFS	250.00	290.00	290.80	291.99	298.02	0.564262	21.55	11.60	16.83	4.57
FML Chute	4196	300 CFS	300.00	290.00	290.84	292.21	300.13	0.687054	24.45	12.27	17.07	5.08
FML Chute	4194	50 CFS	50.00	290.00	291.23	291.34	291.34	0.004982	2.58	19.36	19.40	0.46
FML Chute	4194	100 CFS	100.00	290.00	291.80	291.17	291.96	0.005042	3.20	31.24	22.78	0.48
FML Chute	4194	150 CFS	150.00	290.00	291.85	291.48	293.10	0.153928	12.04	12.46	17.13	2.49
FML Chute	4194	200 CFS	200.00	290.00	290.89	291.75	294.57	0.257977	15.49	12.98	17.32	3.13
FML Chute	4194	250 CFS	250.00	290.00	290.92	291.99	296.16	0.350291	18.37	13.61	17.53	3.67
FML Chute	4194	300 CFS	300.00	290.00	290.96	292.21	297.85	0.441518	21.07	14.24	17.74	4.14
FML Chute	4192	50 CFS	50.00	290.00	291.22	291.33	291.33	0.005160	2.61	19.13	19.33	0.46
FML Chute	4192	100 CFS	100.00	290.00	291.78	291.95	291.95	0.005172	3.23	30.95	22.70	0.49
FML Chute	4192	150 CFS	150.00	290.00	292.21	291.48	292.42	0.005182	3.64	41.24	25.28	0.50
FML Chute	4192	200 CFS	200.00	290.00	291.02	291.75	293.65	0.157016	13.02	15.36	18.12	2.49
FML Chute	4192	250 CFS	250.00	290.00	291.04	291.99	294.93	0.225868	15.83	15.79	18.26	3.00
FML Chute	4192	300 CFS	300.00	290.00	291.07	292.21	296.32	0.294959	18.37	16.33	18.44	3.44
FML Chute	4190	50 CFS	50.00	290.00	291.21	291.32	291.32	0.002884	2.76	18.87	19.25	0.47
FML Chute	4190	100 CFS	100.00	290.00	291.77	291.94	291.94	0.002881	3.44	30.54	22.60	0.50
FML Chute	4190	150 CFS	150.00	290.00	292.19	292.41	292.41	0.002883	3.89	40.70	25.15	0.51
FML Chute	4190	200 CFS	200.00	290.00	292.55	291.77	292.81	0.002884	4.24	50.02	27.28	0.52
FML Chute	4190	250 CFS	250.00	290.00	291.15	292.01	294.31	0.085151	14.57	17.83	18.92	2.54
FML Chute	4190	300 CFS	300.00	290.00	291.17	292.23	295.52	0.114969	17.11	18.23	19.05	2.96
FML Chute	4188	50 CFS	50.00	289.99	291.20	291.31	291.31	0.002999	2.64	18.91	19.26	0.47
FML Chute	4188	100 CFS	100.00	289.99	291.75	291.93	291.93	0.003001	3.27	30.62	22.61	0.49
FML Chute	4188	150 CFS	150.00	289.99	292.19	292.40	292.40	0.003001	3.68	40.81	25.17	0.51
FML Chute	4188	200 CFS	200.00	289.99	292.55	292.79	292.79	0.002998	3.99	50.16	27.31	0.52
FML Chute	4188	250 CFS	250.00	289.99	291.20	291.99	293.94	0.075860	13.27	16.83	19.24	2.36
FML Chute	4188	300 CFS	300.00	289.99	291.22	292.20	295.03	0.104249	15.67	19.14	19.33	2.78
FML Chute	4186	50 CFS	50.00	289.99	291.20	291.31	291.31	0.003000	2.64	18.91	19.26	0.47
FML Chute	4186	100 CFS	100.00	289.99	291.76	291.92	291.92	0.003001	3.27	30.62	22.61	0.49
FML Chute	4186	150 CFS	150.00	289.99	292.18	292.39	292.39	0.003001	3.68	40.81	25.17	0.51
FML Chute	4186	200 CFS	200.00	289.99	292.54	292.79	292.79	0.002998	3.99	50.16	27.31	0.52
FML Chute	4186	250 CFS	250.00	289.99	291.29	291.98	293.57	0.058292	12.12	20.62	19.79	2.09
FML Chute	4186	300 CFS	300.00	289.99	291.29	292.20	294.57	0.083984	14.55	20.62	19.78	2.51
FML Chute	4184	50 CFS	50.00	289.98	291.19	291.30	291.30	0.003000	2.64	18.91	19.26	0.47
FML Chute	4184	100 CFS	100.00	289.98	291.75	291.92	291.92	0.003001	3.27	30.62	22.61	0.49
FML Chute	4184	150 CFS	150.00	289.98	292.18	292.39	292.39	0.003001	3.68	40.81	25.17	0.51
FML Chute	4184	200 CFS	200.00	289.98	292.53	292.78	292.78	0.002997	3.99	50.17	27.31	0.52
FML Chute	4184	250 CFS	250.00	289.98	292.84	293.12	293.12	0.002997	4.24	58.92	29.17	0.53
FML Chute	4184	300 CFS	300.00	289.98	291.36	292.19	294.19	0.067522	13.49	22.23	20.27	2.27
FML Chute	4182	50 CFS	50.00	289.98	291.19	291.29	291.29	0.003000	2.64	18.91	19.26	0.47
FML Chute	4182	100 CFS	100.00	289.98	291.75	291.91	291.91	0.003001	3.27	30.62	22.61	0.49
FML Chute	4182	150 CFS	150.00	289.98	292.17	292.38	292.38	0.003001	3.68	40.81	25.17	0.51
FML Chute	4182	200 CFS	200.00	289.98	292.53	292.77	292.77	0.002997	3.99	50.17	27.31	0.52
FML Chute	4182	250 CFS	250.00	289.98	292.84	293.12	293.12	0.002997	4.24	58.92	29.17	0.53
FML Chute	4182	300 CFS	300.00	289.98	291.44	292.13	293.86	0.053993	12.48	24.03	20.79	2.05
FML Chute	4175	50 CFS	50.00	289.96	291.16	291.27	291.27	0.003000	2.64	18.91	19.26	0.47
FML Chute	4175	100 CFS	100.00	289.96	291.72	291.89	291.89	0.003001	3.27	30.62	22.61	0.49
FML Chute	4175	150 CFS	150.00	289.96	292.15	292.36	292.36	0.003001	3.68	40.81	25.17	0.51
FML Chute	4175	200 CFS	200.00	289.96	292.51	292.75	292.75	0.002997	3.99	50.17	27.31	0.52
FML Chute	4175	250 CFS	250.00	289.96	292.82	293.10	293.10	0.002997	4.24	58.92	29.17	0.53
FML Chute	4175	300 CFS	300.00	289.96	293.09	292.17	293.40	0.003000	4.46	67.21	30.83	0.53
FML Chute	4170	50 CFS	50.00	289.94	291.15	291.26	291.26	0.003000	2.64	18.91	19.26	0.47
FML Chute	4170	100 CFS	100.00	289.94	291.71	291.87	291.87	0.003001	3.27	30.62	22.61	0.49
FML Chute	4170	150 CFS	150.00	289.94	292.14	292.35	292.35	0.003001	3.68	40.81	25.17	0.51
FML Chute	4170	200 CFS	200.00	289.94	292.49	292.74	292.74	0.002997	3.99	50.17	27.31	0.52
FML Chute	4170	250 CFS	250.00	289.94	292.80	293.08	293.08	0.002997	4.24	58.92	29.17	0.53
FML Chute	4170	300 CFS	300.00	289.94	293.08	293.39	293.39	0.003000	4.46	67.21	30.83	0.53
FML Chute	4160	50 CFS	50.00	289.91	291.12	291.23	291.23	0.003000	2.64	18.91	19.26	0.47
FML Chute	4160	100 CFS	100.00	289.91	291.68	291.84	291.84	0.003002	3.27	30.62	22.61	0.49
FML Chute	4160	150 CFS	150.00	289.91	292.11	292.32	292.32	0.003001	3.68	40.81	25.17	0.51
FML Chute	4160	200 CFS	200.00	289.91	292.46	292.71	292.71	0.002997	3.99	50.17	27.31	0.52
FML Chute	4160	250 CFS	250.00	289.91	292.77	293.05	293.05	0.002997	4.24	58.92	29.17	0.53
FML Chute	4160	300 CFS	300.00	289.91	293.05	293.36	293.36	0.003000	4.46	67.21	30.83	0.53
FML Chute	4150	50 CFS	50.00	289.88	291.09	291.20	291.20	0.003000	2.64	18.91	19.26	0.47
FML Chute	4150	100 CFS	100.00	289.88	291.65	291.81	291.81	0.003002	3.27	30.62	22.61	0.49
FML Chute	4150	150 CFS	150.00	289.88	292.08	292.29	292.29	0.003001	3.68	40.81	25.17	0.51
FML Chute	4150	200 CFS	200.00	289.88	292.43	292.68	292.68	0.002997	3.99	50.17	27.31	0.52
FML Chute	4150	250 CFS	250.00	289.88	292.74	293.02	293.02	0.002996	4.24	58.93	29.17	0.53
FML Chute	4150	300 CFS	300.00	289.88	293.02	293.33	293.33	0.003000	4.46	67.21	30.83	0.53
FML Chute	4140	50 CFS	50.00	289.85	291.06	291.17	291.17	0.003000	2.64	18.91	19.26	0.47
FML Chute	4140	100 CFS	100.00	289.85	291.62	291.78	291.78	0.003002	3.27	30.62	22.61	0.49
FML Chute	4140	150 CFS	150.00	289.85	292.05	292.26	292.26	0.003001	3.68	40.81	25.17	0.51
FML Chute	4140	200 CFS	200.00	289.85	292.40	292.65	292.65	0.002997	3.99	50.17	27.31	0.52
FML Chute	4140	250 CFS	250.00	289.85	292.71	292.99	292.99	0.002996	4.24	58.93	29.17	0.53
FML Chute	4140	300 CFS	300.00	289.85	292.99	293.30	293.30	0.003000	4.46	67.21	30.83	0.53
FML Chute	4130	50 CFS	50.00	289.82	291.03	291.14	291.14	0.003000	2.64	18.91	19.26	0.47
FML Chute	4130	100 CFS	100.00	289.82	291.59	291.75	291.75	0.003002	3.27	30.62	22.61	0.49
FML Chute	4130	150 CFS	150.00	289.82	292.02	292.23	292.23	0.003001	3.68	40.81	25.17	0.51
FML Chute	4130	200 CFS	200.00	289.82	292.37	292.62						

FML Chute	4110	50 CFS	50.00	289.76	290.97	291.08	0.003000	2.64	18.91	19.26	0.47
FML Chute	4110	100 CFS	100.00	289.76	291.53	291.69	0.003003	3.27	30.61	22.61	0.49
FML Chute	4110	150 CFS	150.00	289.76	291.96	292.17	0.003002	3.68	40.81	25.17	0.51
FML Chute	4110	200 CFS	200.00	289.76	292.31	292.56	0.002996	3.99	50.17	27.31	0.52
FML Chute	4110	250 CFS	250.00	289.76	292.62	292.90	0.002996	4.24	58.93	29.17	0.53
FML Chute	4110	300 CFS	300.00	289.76	292.90	293.21	0.003000	4.46	67.21	30.83	0.53
FML Chute	4100	50 CFS	50.00	289.73	290.94	291.05	0.003000	2.64	18.91	19.26	0.47
FML Chute	4100	100 CFS	100.00	289.73	291.50	291.66	0.003003	3.27	30.61	22.61	0.49
FML Chute	4100	150 CFS	150.00	289.73	291.93	292.14	0.003002	3.68	40.81	25.17	0.51
FML Chute	4100	200 CFS	200.00	289.73	292.28	292.53	0.002996	3.99	50.17	27.31	0.52
FML Chute	4100	250 CFS	250.00	289.73	292.59	292.87	0.002996	4.24	58.93	29.17	0.53
FML Chute	4100	300 CFS	300.00	289.73	292.87	293.18	0.003000	4.46	67.21	30.83	0.53
FML Chute	4000	50 CFS	50.00	289.43	290.64	290.75	0.002994	2.64	18.92	19.26	0.47
FML Chute	4000	100 CFS	100.00	289.43	291.20	291.36	0.003007	3.27	30.60	22.61	0.50
FML Chute	4000	150 CFS	150.00	289.43	291.63	290.51	0.003003	3.68	40.80	25.17	0.51
FML Chute	4000	200 CFS	200.00	289.43	291.98	291.18	0.002993	3.98	50.19	27.32	0.52
FML Chute	4000	250 CFS	250.00	289.43	292.29	292.57	0.002993	4.24	58.95	29.18	0.53
FML Chute	4000	300 CFS	300.00	289.43	292.57	292.88	0.003001	4.46	67.21	30.83	0.53
FML Chute	3000	50 CFS	50.00	286.43	287.64	287.13	0.003001	2.64	18.91	19.26	0.47
FML Chute	3000	100 CFS	100.00	286.43	288.20	287.60	0.003002	3.27	30.62	22.61	0.49
FML Chute	3000	150 CFS	150.00	286.43	288.63	287.91	0.003004	3.68	40.80	25.17	0.51
FML Chute	3000	200 CFS	200.00	286.43	288.98	288.18	0.003001	3.99	50.14	27.31	0.52
FML Chute	3000	250 CFS	250.00	286.43	289.29	288.42	0.003000	4.24	58.90	29.17	0.53
FML Chute	3000	300 CFS	300.00	286.43	289.57	288.64	0.003004	4.47	67.18	30.82	0.53

PYRAMAT high performance turf reinforcement mat (HPTRM) is a three-dimensional, lofty, woven polypropylene geotextile that is available in green or tan which is specially designed for erosion control applications on steep slopes and vegetated waterways. The matrix is composed of polypropylene monofilament yarns featuring X3® technology woven into a uniform configuration of resilient pyramid-like projections. The material exhibits very high interlock and reinforcement capacity with both soil and root systems, demonstrates superior UV resistance, and enhances seedling emergence.

PYRAMAT conforms to the property values listed below¹ and is manufactured at a Propex facility having achieved ISO 9001:2000 certification. Propex performs internal Manufacturing Quality Control (MQC) tests that have been accredited by the Geosynthetic Accreditation Institute - Laboratory Accreditation Program (GAI-LAP).

PRODUCT TEST DATA		
Property	Test Method	MARV ²
Physical		
Mass Per Unit Area	ASTM D-6566	13.5 oz sq yd (455 g sq m)
Thickness	ASTM D-6525	.4 in (10.2 mm)
Light Penetration (% Passing)	ASTM D-6567	10% (10%)
Color	Visual	Green, Tan
Mechanical		
Tensile Strength (Grab)	ASTM D-6818	4000 x 3000 lbs/ft (58.4 x 43.8 kN/m)
Elongation	ASTM D-6818	65% max (65% max)
Resiliency	ASTM D-6524	80% (80%)
Flexibility	ASTM D-6575	.534 in/lbs (615000 mg-cm) avg
Endurance		
UV Resistance @ 6000 hrs	ASTM D-4355	90% (90%)
Performance		
Velocity ³ (Vegetated)	Large Scale	25 ft/sec (7.6 m/sec)
Shear Stress ³ (Vegetated)	Large Scale	15 lbs sq ft (718 Pa)
Manning's "n" ⁴ (Unvegetated)	Calculated	.028 (.028)
Seedling Emergence	ECTC Draft Method #4	296% (296%)

NOTES

1. The property values listed are effective 08/2006 and are subject to change without notice.
2. MARV indicates minimum average roll value calculated as the typical minus two standard deviations. Statistically, it yields a 97.7% degree of confidence that any sample taken during quality assurance testing will exceed the value reported.
3. Maximum permissible velocity and shear stress has been obtained through vegetated testing programs featuring specific soil types, vegetation classes, flow conditions, and failure criteria. These conditions may not be relevant to every project nor are they replicated by other manufacturers. Please contact Propex for further information.
4. Calculated as typical values from large-scale flexible channel lining test programs with a flow depth of 6 to 12 inches.

The information presented herein, while not guaranteed, is to the best of our knowledge true and accurate. Except when agreed to in writing for specific conditions of use, no warranty or guarantee expressed or implied is made regarding the performance of any product, since the manner of use and handling are beyond our control. Nothing contained herein is to be construed as permission or as a recommendation to infringe any patent.

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HIF-F-2-22

Type	Thickness		Size	d_s	velocity		velocity	
	m	ft			m	ft	m/s	ft/sec
Reno mattress	0.15 - 0.17		70 - 100	0.085	3.5		6.2	
			70 - 150	0.110	4.2		4.5	
	0.23 - 0.25		70 - 100	0.085	3.6		5.5	
			70 - 150	0.120	4.5		6.1	
	0.30		70 - 120	0.100	4.2		5.5	
			100 - 150	0.125	5.0		6.4	
Gabions	0.50	1.64	100 - 200	0.150	5.8	11	7.5	25
			120 - 250	0.190	6.4	21	8.0	26

Where the revetment has to be placed under water the thickness of the Reno mattress remains the same since it can be launched from a pontoon whereas rip rap has to be increased by 50% [12, 13, 49, 50, 51].

The big reduction in the revetment thickness, which is achieved using Reno mattress instead of rip rap, is of economic significance in protection projects in large rivers, given the same area of work and, therefore, the quantity of material used.

2.2 Semi permeable and impermeable linings with sand asphalt mastic.

a) General characteristics of sand asphalt mastic grouted Reno mattress.

The combination of the stone filled Reno mattress and sand asphalt mastic has the characteristics of both gabion work and asphalt concrete. The addition of bituminous mastic to the Reno mattress produces a structure which combines the properties and performance of both materials. The mattress retains its flexibility, while the density of the filling is increased and therefore the efficiency of the protection. If all the voids between the stones in the layer are filled and the surface of the mattress covered, the lining will be completely impervious. The mastic also protects the wire mesh against corrosion and from abrasion by transported material.

The wire mesh reinforces the grouted stone layer and gives it strength in tension. Hence, the thickness of the combined structure can be considerably less than that of ordinary mastic grouted stone to withstand the same stresses. The resulting saving in bitumen and aggregate, and the increased flexibility due to the reduced thickness, have given rise to extensive use of this type of lining for protection in a variety of waterways.

b) Mix design of sand asphalt mastic.

To avoid excessive detail, only the fundamental data on mix design is given here. For fuller information, reference should be made to the specific publications listed in the bibliography [5, 6].

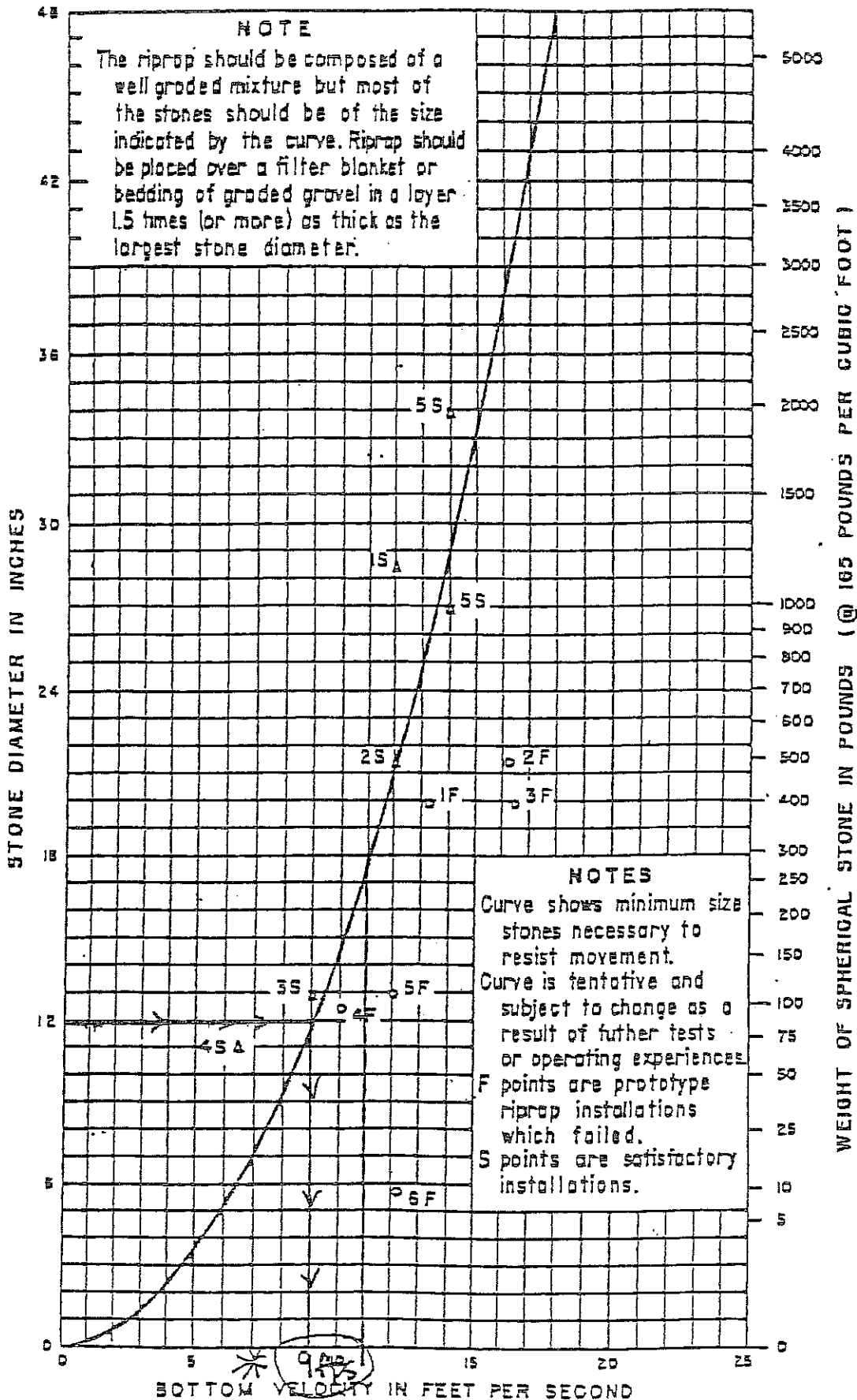


FIGURE 165.—Curves to determine maximum stone size in riprap mixture.

SOURCE: HYDRAULIC DESIGN OF STILLING BASINS AND ENERGY DISSIPATORS. US DEPT OF THE INTERIOR - BUREAU OF LAND RECLAMATION, 1957.

Required: Determine the maximum drainage area for 24-inch and 36-inch diameter letdown pipes using the BCAP computer program.

Method:

1. Determine the maximum flow for 24-inch and 36-inch diameter letdown pipes on the 20% side slope.
2. Determine the maximum drainage areas for the flows calculated in Step 1.

Reference:

1. State of Texas, Department of Transportation, Bridge Division, Hydraulic Manual, March 2004.

Note: The pipe letdown analysis has been performed using "Broken-Back" Culvert Analysis Program (BCAP) which is available from the Federal Highway Administration Web Page:
<http://www.dor.state.ne.us/roadway-design/> [follow link to downloadable files and info]

The program was developed to analyze culverts with changing slopes.

Solution:

1. Determine the maximum flow for 24-inch and 36-inch diameter letdown pipes on the 20% side slope.

The following pages include the program outputs for the 24-in diameter culvert and 36-in diameter culvert. Pages III-F-2-27 and III-F-2-32 include rating tables that show if the hydraulic jump occurs within the pipe or not [YES/NO]. The results also include pipe outlet velocity for each flow rate as well as the tailwater depth and velocity in the channel ("Tailwater Velocity").

The flow ratings are used to calculate the maximum allowable top dome drainage area for each pipe size analyzed (Step 2). The maximum flow rate that has hydraulic jump within the culvert is used for allowable drainage area calculations on page III-F-2-36. The computer program does not have corrugated plastic pipe option; therefore, the corrugated metal pipe option has been used with a Manning's Coefficient of 0.024.

The pipe design was analyzed using 10-feet of runoff with a -2.5 percent slope at the toe of the 20 percent side slope (See Figures on pages III-F-2-30 and III-F-2-35).

Results:

Q24 =	23.0	cfs	maximum allowable flow in 24-in-dia pipe
Q36 =	26.0	cfs	maximum allowable flow in 36-in-dia pipe

NEBRASKA DEPARTMENT OF ROADS
Broken-Back Culvert Analysis Program (BCAP)

PROJECT INFO

Project: Camelot
Station or Location: Lewisville, TX
Date: 06 / 17 / 2011

DISCHARGE DATA

Minimum: 15.00 cfs
Design Discharge: 23.00 cfs
Maximum: 25.00 cfs
Number of Barrels: 1

TAILWATER DATA

Type: Downstream
Channel Shape: Trapezoid
Left Side Slope: 3 H:1V
Right Side Slope: 3 H:1V
Bottom Width: 6 ft
Bottom Slope: 0.0001 ft/ft
Roughness Coefficient: 0.04

CULVERT DATA

Type: Circular Pipe
Pipe Diameter: 2 ft
Culvert Material: Corr. Metal Pipe
Inlet Type: Mitered to Conform to Slope
Roughness Coefficient: 0.024
Outlet Section Roughness Coeff.: 0.024
Inlet Section Slope: 0.04 ft/ft
Steep Section Slope: 0.2 ft/ft
Outlet Section Slope: -0.025 ft/ft

CULVERT PROFILE DATA

Type: Double Broken-Back
Inlet Station: 1490.00 ft
Inlet Elevation: 510.80 ft
Upper Break Station: 1510.00 ft
Upper Break Elevation: 510.00 ft
Lower Break Station: 1760.00 ft
Lower Break Elevation: 460.00 ft
Outlet Station: 1770.00 ft
Outlet Elevation: 460.25 ft

NEBRASKA DEPARTMENT OF ROADS
Broken-Back Culvert Analysis Program (BCAP)

Project: Camelot
Station or Location: Lewisville, TX
Date: 06/17/2011

Discharge	Headwater Depth	Inlet Control Elevation	Break Control Elevation	Critical Depth	Outlet Depth	Outlet Velocity	Outlet Froude Number	Tailwater Depth	Tailwater Velocity	Hydraulic Jump
cfs	ft	ft	ft	ft	ft	ft/s		ft	ft/s	
16.0	2.52	513.32	513.02	1.41	.74	15.14	3.6	2.45	.49	YES
17.0	2.69	513.49	513.14	1.46	.78	15.12	3.5	2.51	.50	YES
18.0	2.88	513.68	513.27	1.50	.80	15.34	3.5	2.59	.50	YES
19.0	3.07	513.87	513.39	1.54	.82	15.67	3.5	2.65	.51	YES
20.0	3.27	514.07	513.53	1.58	.85	15.85	3.5	2.71	.52	YES
21.0	3.48	514.28	513.67	1.62	.88	15.89	3.4	2.77	.53	YES
22.0	3.71	514.51	513.81	1.66	.90	16.05	3.4	2.83	.54	YES
23.0	3.94	514.74	513.95	1.69	.93	16.19	3.3	2.89	.54	YES
24.0	4.18	514.98	514.10	1.73	.95	16.43	3.3	2.95	.55	YES
25.0	4.43	515.23	514.23	1.77	.97	16.66	3.3	3.01	.55	YES

NEBRASKA DEPARTMENT OF ROADS
Broken-Back Culvert Analysis Program (BCAP)

PROJECT INFO

Project: Camelot
Station or Location: Lewisville, TX
Date: 06/17/2011

CULVERT DATA

Discharge: 23.0 cfs
Shape: Circular
Material: Corr. Metal Pipe
Size: 1-2.0 ft x 2.0 ft
Inlet Type: Mitered to Conform to Slope

WATER SURFACE PROFILE

Inlet Depth: 1.69 ft
Inlet Velocity: 8.11 ft/s
Upper Break Depth: 1.54 ft
Upper Break Velocity: 8.86 ft/s
Lower Break Depth: 0.90 ft
Lower Break Velocity: 16.77 ft/s
Depth at End of Hydraulic Jump: 2.00 ft
Velocity at End of Hydraulic Jump: 16.19 ft/s
Depth at End of Hydraulic Jump: 2.89 ft
Velocity at End of Hydraulic Jump: 0.54 ft/s

OUTPUT DATA

Head Water Depth: 3.94 ft
Inlet Control Elevation: 514.74 ft
Break Control Elevation: 513.95 ft
Critical Depth: 1.69 ft
Tailwater Depth: 2.89 ft
Hydraulic Jump? YES
 Jump Station: 271.24 ft
 Jump Length: 18.59 ft
Outlet Depth: 0.93 ft
Outlet Velocity: 16.19 ft/s
Outlet Froude No.: 3.3

Circle Pipe Culvert

Inlet Type

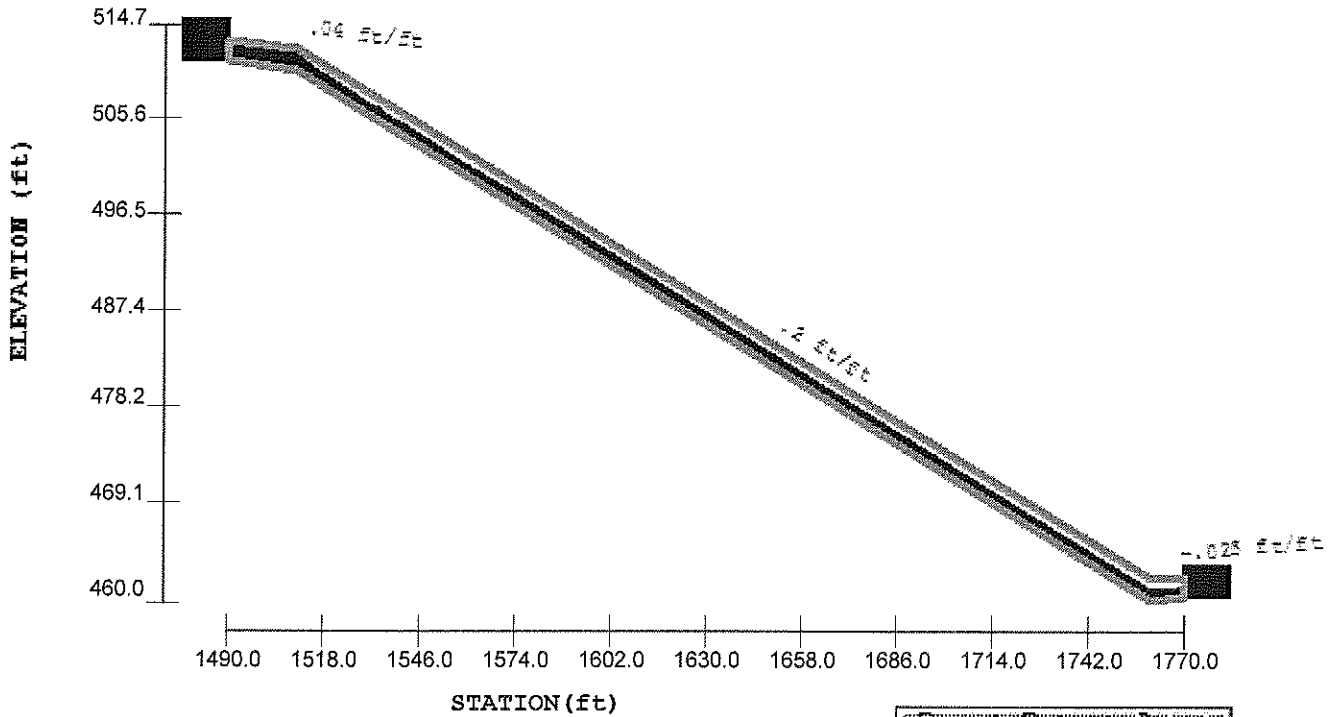
Diameter=2 ft

Mitered to Conform to Slope

Culvert Material: Corr. Metal Pipe Rough. Coeff.= 0.024

Outlet Sec. Rough. Coeff.= 0.024

Q = 23 cfs



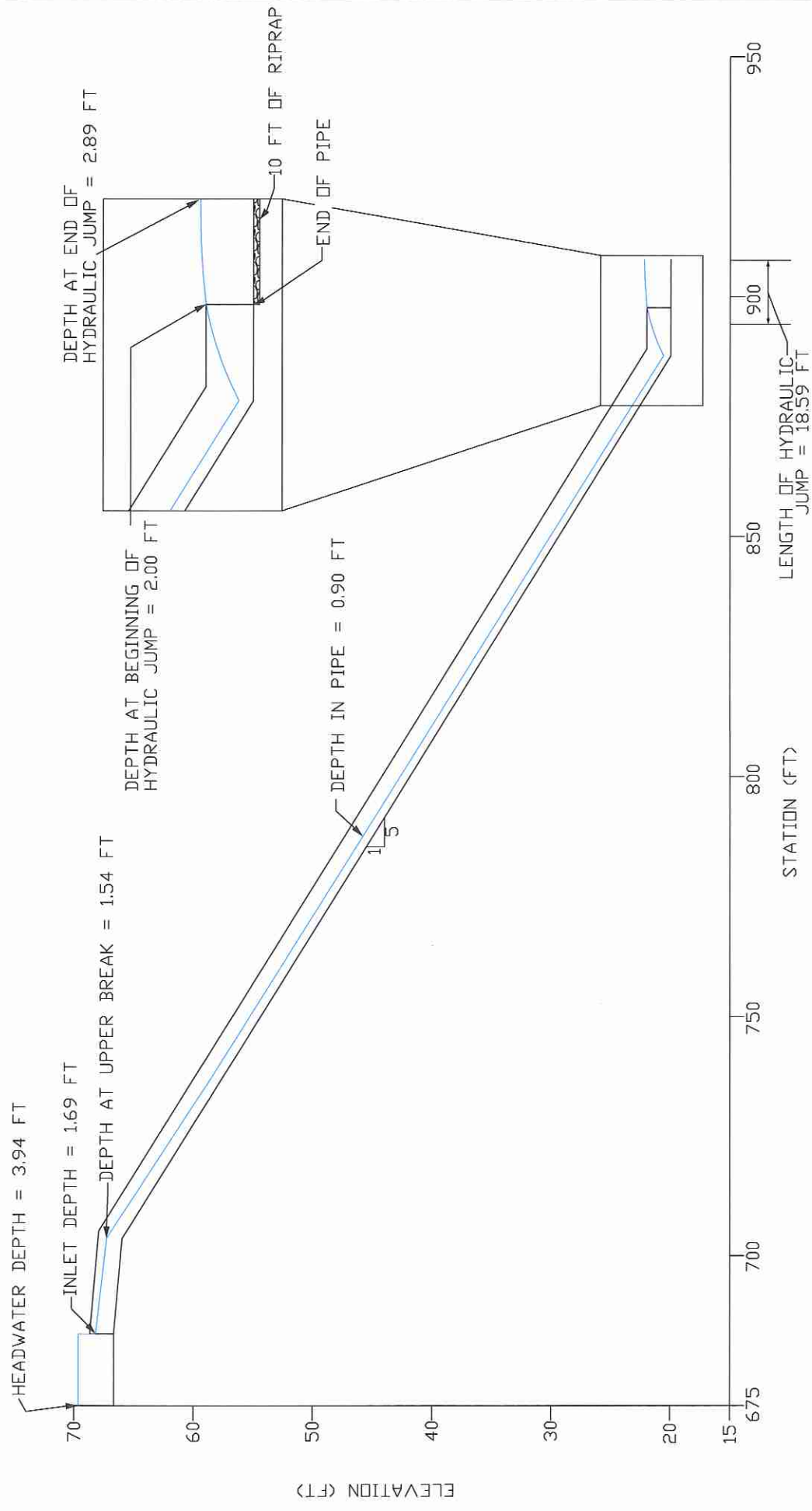
Source:

P:\SOLID WASTE\CITY OF FARMERS BRANCH\EXPANSION 2

Press to Return to Output Farm

IX IIF

WATER SURFACE PROFILE



P:\Solid waste\City of Farmers Branch\Expansion 2009\Part III-SDP\Appendix III\IIIF-F\BCAP\20 Percent\Pipe Water Profile 2 ft pipe.dwg, 6/21/2011 3:08:03 PM, jwilson, 1:0.117

NEBRASKA DEPARTMENT OF ROADS
Broken-Back Culvert Analysis Program (BCAP)

PROJECT INFO

Project: Camelot
Station or Location: Lewisville, TX
Date: 06 / 17 / 2011

DISCHARGE DATA

Minimum: 20.00 cfs
Design Discharge: 26.00 cfs
Maximum: 30.00 cfs
Number of Barrels: 1

TAILWATER DATA

Type: Downstream
Channel Shape: Trapezoid
Left Side Slope: 3 H:1V
Right Side Slope: 3 H:1V
Bottom Width: 6 ft
Bottom Slope: 0.0001 ft/ft
Roughness Coefficient: 0.04

CULVERT DATA

Type: Circular Pipe
Pipe Diameter: 3 ft
Culvert Material: Corr. Metal Pipe
Inlet Type: Mitered to Conform to Slope
Roughness Coefficient: 0.024
Outlet Section Roughness Coeff.: 0.024
Inlet Section Slope: 0.04 ft/ft
Steep Section Slope: 0.2 ft/ft
Outlet Section Slope: -0.025 ft/ft

CULVERT PROFILE DATA

Type: Double Broken-Back
Inlet Station: 1490.00 ft
Inlet Elevation: 510.80 ft
Upper Break Station: 1510.00 ft
Upper Break Elevation: 510.00 ft
Lower Break Station: 1760.00 ft
Lower Break Elevation: 460.00 ft
Outlet Station: 1770.00 ft
Outlet Elevation: 460.25 ft

NEBRASKA DEPARTMENT OF ROADS
Broken-Back Culvert Analysis Program (BCAP)

Project:

Station or Location:

Date:

Camelot
Lewisville, TX
06/17/2011

Discharge	Headwater Depth	Inlet Control Elevation	Break Control Elevation	Critical Depth	Outlet Depth	Outlet Velocity	Outlet Froude Number	Tailwater Depth	Tailwater Velocity	Hydraulic Jump
cfs	ft	ft	ft	ft	ft	ft/s		ft	ft/s	
21.0	2.41	512.97	513.21	1.46	.73	15.89	4.0	2.77	.53	YES
22.0	2.45	513.03	513.25	1.50	.74	16.22	4.1	2.83	.54	YES
23.0	2.50	513.09	513.30	1.53	.76	16.34	4.0	2.89	.54	YES
24.0	2.54	513.15	513.34	1.56	.78	16.43	4.0	2.95	.55	YES
25.0	2.59	513.21	513.39	1.59	.80	16.52	4.0	3.01	.55	YES
26.0	2.63	513.27	513.43	1.63	.82	16.60	3.9	3.07	.56	YES
27.0	2.68	513.33	513.48	1.66	.82	17.24	4.1	3.11	.57	YES
28.0	2.73	513.39	513.53	1.69	.84	17.28	4.0	3.17	.57	YES
29.0	2.77	513.46	513.57	1.72	.86	17.32	4.0	3.23	.57	YES
30.0	2.82	513.52	513.62	1.75	.88	17.35	3.9	3.27	.58	YES

**NEBRASKA DEPARTMENT OF ROADS
Broken-Back Culvert Analysis Program (BCAP)**

PROJECT INFO

Project: Camelot
Station or Location: Lewisville, TX
Date: 06/17/2011

CULVERT DATA

Discharge: 26.0 cfs
Shape: Circular
Material: Corr. Metal Pipe
Size: 1-3.0 ft x 3.0 ft
Inlet Type: Mitered to Conform to Slope

WATER SURFACE PROFILE

Inlet Depth: 2.70 ft
Inlet Velocity: 3.88 ft/s
Upper Break Depth: 1.63 ft
Upper Break Velocity: 6.64 ft/s
Lower Break Depth: 0.82 ft
Lower Break Velocity: 16.60 ft/s
Depth at End of Hydraulic Jump: 3.00 ft
Velocity at End of Hydraulic Jump: 16.60 ft/s
Depth at End of Hydraulic Jump: 3.07 ft
Velocity at End of Hydraulic Jump: 0.56 ft/s

OUTPUT DATA

Head Water Depth: 2.63 ft
Inlet Control Elevation: 513.27 ft
Break Control Elevation: 513.43 ft
Critical Depth: 1.63 ft
Tailwater Depth: 3.07 ft
Hydraulic Jump? YES
 Jump Station: 270.00 ft
 Jump Length: 19.36 ft
Outlet Depth: 0.82 ft
Outlet Velocity: 16.60 ft/s
Outlet Froude No.: 3.9

Circle Pipe Culvert

Inlet Type

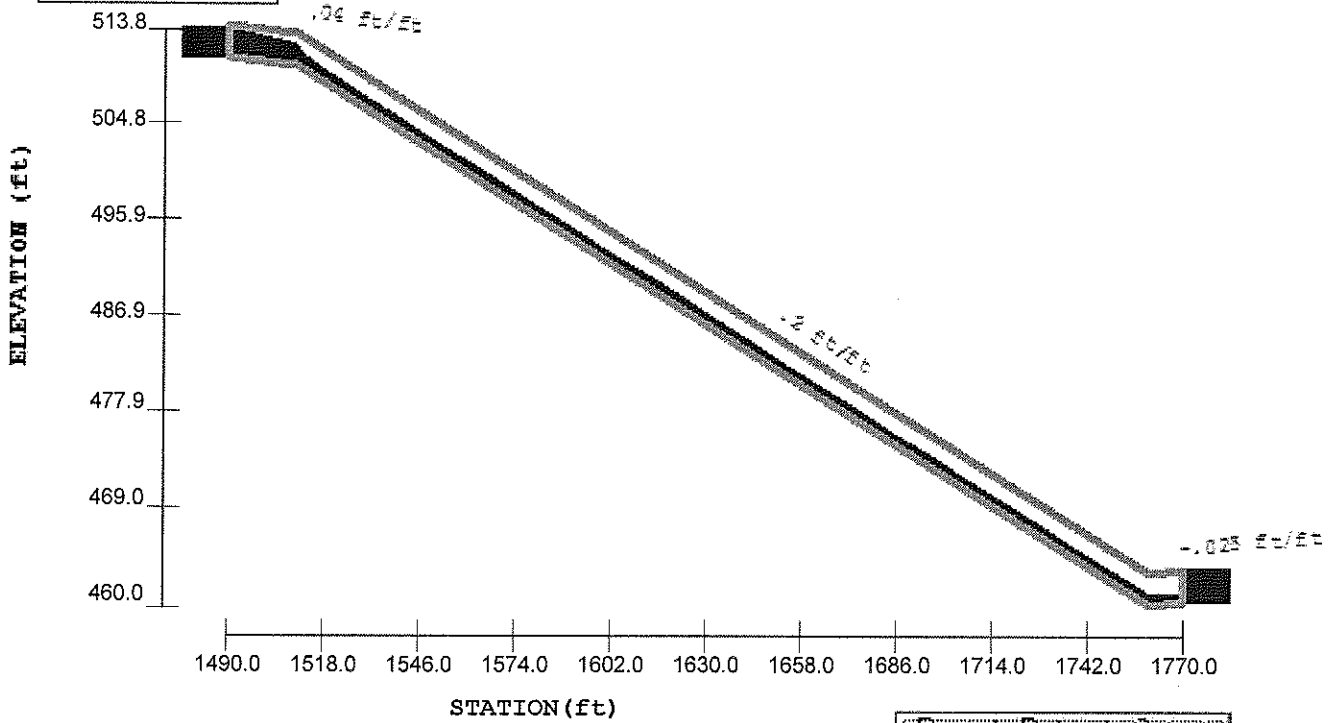
Diameter=3 ft

Mitered to Conform to Slope

Culvert Material: Corr. Metal Pipe Rough. Coeff.= 0.024

Outlet Sec. Rough. Coeff.= 0.024

Q = 26 cfs



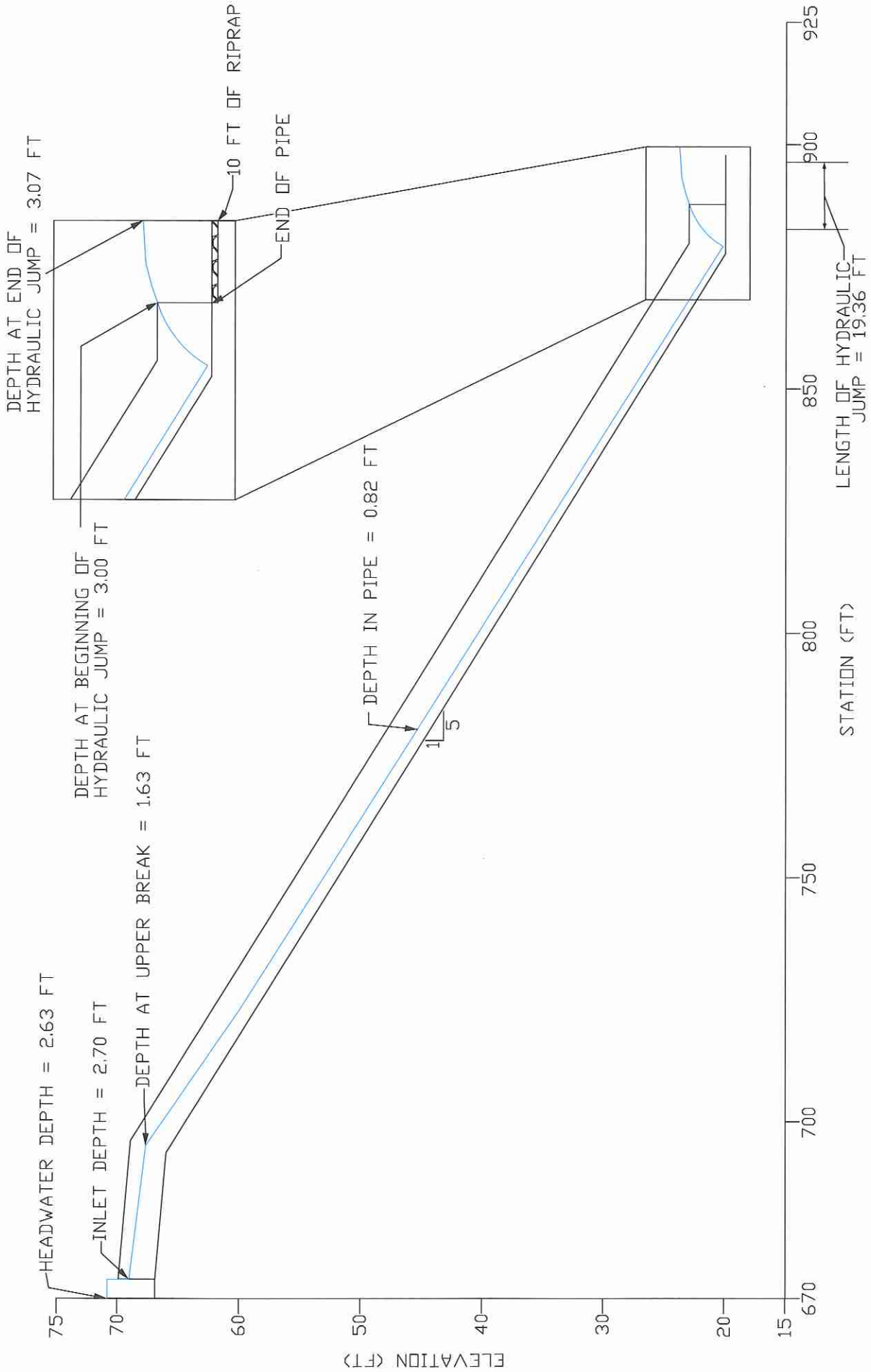
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Press to Return to Output Form

IX IIF

WATER SURFACE PROFILE



2. Determine the maximum drainage areas for the flows calculated in Step 1.

$$Q = CIA$$

Where: C = 0.8 (runoff coefficient, Ref 1.)
I = intensity, in/hr
A = drainage area, ac

$$I = \frac{b}{(t_c + d)^e}$$

b = 90 From Ref. 1, for Denton County
d = 8.5 25-year storm event
e = 0.781
t_c is assumed to be 10 min.

$$I = 9.22 \text{ in/hr}$$

$$A = Q / (CI)$$

Pipe Diameter (in)	Flow (cfs)	Area (ac)
24	23.0	3.1
36	26.0	3.5

Conclusion:

The maximum allowable drainage area for a 24-inch diameter letdown pipe is 3.1 acres for each inlet and for a 36-inch diameter letdown pipe is 3.5 acres for each inlet. The minimum berm height is 3 feet for a 24-inch diameter pipe and 4 feet for 36-inch diameter pipe. (Figure 3 details indicate 1 foot berm above the pipe).

CAMELOT LANDFILL
1339-351-11-02
PIPE LETDOWN RIPRAP DESIGN

Required: Determine the riprap size and dimensions for 24-inch and 36-inch diameter letdown pipes using riprap apron design provided by the Reference 1.

Method:

1. Determine the hydraulic conditions at the outlet of 24-inch and 36-inch diameter letdown pipes using the hydraulic design developed using the BCAP computer simulation.
2. Determine the riprap size and apron dimensions for each pipe letdown

Reference:

1. U.S. Department of Transportation - Federal Highway Administration. Hydraulic Engineering Circular No. 14, Third Edition. *Hydraulic Design of Energy Dissipators for Culverts and Channels*. Publication No. FHWA-NHI-06-086, July 2006.

Solution:

1. Determine the hydraulic parameters from pages III-F-2-28 (pipe diameter 24-inches) and III-F-2-33 (pipe diameter 36-inches):

Parameter	Symbol	24-inch Dia. Culvert	36-inch Dia. Culvert
Design flow rate, cfs	Q	23.0	26.0
Pipe Diameter, ft	D	2	3
Depth at the pipe outlet, ft	y_n	0.93	0.82
Adjusted culvert rise, ft	D'	1.465	1.91
Tailwater Depth ¹ , ft	TW	2	3

¹Tailwater depth is the pipe diameter when the calculated tailwater depth is higher per Reference 1.

$$D_{50} = 0.2 \times D \left[\frac{Q}{\sqrt{g} \times D^{2.5}} \right]^{4/3} \times \left[\frac{D}{TW} \right] \quad \text{Eq. 10.4 (page 10-17 of Ref. 1)}$$

$$D' = \frac{D + y_n}{2} \quad \text{Eq. 10.5 (page 10-17 of Ref. 1)}$$

D_{50} = Riprap size in feet

CAMELOT LANDFILL
1339-351-11-02
PIPE LETDOWN RIPRAP DESIGN

Riprap Classes and Apron Dimensions¹

Class	D ₅₀ (in)	Apron Length ² (ft)	Apron Depth (ft)
1	5	4xD'	3.5xD ₅₀
2	6	4xD'	3.3xD ₅₀
3	10	5xD'	2.4xD ₅₀
4	14	6xD'	2.2xD ₅₀
5	20	7xD'	2.0xD ₅₀
6	22	8xD'	2.0xD ₅₀

¹This table has been reproduced from Table 10.1 included on page 10-18 of Reference 1.

²D' is the culvert rise.

Design Parameter	24-inch Dia. Culvert	36-inch Dia. Culvert
D ₅₀ , calculated, inches =	4.7	2.6
D ₅₀ , selected, inches =	5	5
Apron Length, calculated, feet =	5.86	7.64
Apron Length, selected, feet =	10	10
Apron Depth, calculated, inches =	17.5	17.5
Apron Depth, selected, inches =	18	18

Conclusion:

Riprap sizes for pipe diameters of 24-inches and 36-inches are selected conservatively. The calculated apron length is increased to 10 feet in the design. The apron depth used is higher than the calculated apron depth. Therefore, the design of the pipe letdown outlet energy dissipater calculations are acceptable and channels at the pipe outlets will be stable.

Required: Determine the maximum drainage area for 24-inch and 36-inch diameter letdown pipes using the BCAP computer program.

Method:

1. Determine the maximum flow for 24-inch and 36-inch diameter letdown pipes on the 25% side slope.
2. Determine the maximum drainage areas for the flows calculated in Step 1.

Reference: 1. State of Texas, Department of Transportation, Bridge Division, Hydraulic Manual, March 2004.

Note: The pipe letdown analysis has been performed using "Broken-Back" Culvert Analysis Program (BCAP) which is available from the Federal Highway Administration Web Page:
<http://www.dor.state.ne.us/roadway-design/> [follow link to downloadable files and info]

The program was developed to analyze culverts with changing slopes.

Solution: 1. Determine the maximum flow for 24-inch and 36-inch diameter letdown pipes on the 25% side slope.

The following pages include the program outputs for the 24-in dia culvert and 36-in diameter culvert. Pages III-F-2-41 and III-F-2-46 include rating tables that show if the hydraulic jump occurs within the pipe or not [YES/NO]. The results also include pipe outlet velocity for each flow rate as well as the tailwater depth and velocity in the channel ("Tailwater Velocity").

The flow ratings are used to calculate the maximum allowable top dome drainage area for each pipe size analyzed (Step 2). The maximum flow rate that has hydraulic jump within the culvert is used for allowable drainage area calculations on page III-F-2-50. The computer program does not have corrugated plastic pipe option; therefore, the corrugated metal pipe option has been used with a Manning's Coefficient of 0.024.

The pipe design was analyzed using 10-feet of runoff with a -2.5 percent slope at the toe of the 25 percent sideslope (See Figures on pages III-F-2-44 and III-F-2-49).

Results:

Q24 =	16.0	cfs	maximum allowable flow in 24-in-dia pipe
Q36 =	21.0	cfs	maximum allowable flow in 36-in-dia pipe

NEBRASKA DEPARTMENT OF ROADS
Broken-Back Culvert Analysis Program (BCAP)

PROJECT INFO

Project: Camelot
Station or Location: Lewisville, TX
Date: 06 / 17 / 2011

DISCHARGE DATA

Minimum: 10.00 cfs
Design Discharge: 16.00 cfs
Maximum: 20.00 cfs
Number of Barrels: 1

TAILWATER DATA

Type: Downstream
Channel Shape: Trapezoid
Left Side Slope: 3 H:1V
Right Side Slope: 3 H:1V
Bottom Width: 6 ft
Bottom Slope: 0.0001 ft/ft
Roughness Coefficient: 0.04

CULVERT DATA

Type: Circular Pipe
Pipe Diameter: 2 ft
Culvert Material: Corr. Metal Pipe
Inlet Type: Mitered to Conform to Slope
Roughness Coefficient: 0.024
Outlet Section Roughness Coeff.: 0.024
Inlet Section Slope: 0.04 ft/ft
Steep Section Slope: 0.25 ft/ft
Outlet Section Slope: -0.025 ft/ft

CULVERT PROFILE DATA

Type: Double Broken-Back
Inlet Station: 1490.00 ft
Inlet Elevation: 510.80 ft
Upper Break Station: 1510.00 ft
Upper Break Elevation: 510.00 ft
Lower Break Station: 1710.00 ft
Lower Break Elevation: 460.00 ft
Outlet Station: 1720.00 ft
Outlet Elevation: 460.25 ft

NEBRASKA DEPARTMENT OF ROADS
Broken-Back Culvert Analysis Program (BCAP)

Project: Camelot
Station or Location: Lewisville, TX
Date: 06/17/2011

Discharge	Headwater		Inlet		Break		Critical		Outlet		Tailwater		Hydraulic Jump			
	Depth	ft	Control	Elevation	Control	Elevation	Depth	ft	Depth	ft	Velocity	ft/s		Depth	ft	Velocity
11.0	1.83		512.63	512.48	1.17	512.48	1.17		.62	13.41	3.6	2.03		.45		YES
12.0	1.95		512.75	512.58	1.22	512.58	1.22		.65	13.55	3.5	2.13		.45		YES
13.0	2.08		512.88	512.69	1.27	512.69	1.27		.69	13.66	3.4	2.21		.47		YES
14.0	2.22		513.02	512.80	1.32	512.80	1.32		.72	13.75	3.4	2.29		.48		YES
15.0	2.36		513.16	512.91	1.37	512.91	1.37		.74	14.33	3.5	2.37		.48		YES
16.0	2.52		513.32	513.02	1.41	513.02	1.41		.77	14.48	3.4	2.45		.49		YES
17.0	2.69		513.49	513.14	1.46	513.14	1.46		.80	14.49	3.3	2.51		.50		YES
18.0	2.88		513.68	513.27	1.50	513.27	1.50		.83	14.72	3.3	2.59		.50		YES
19.0	3.07		513.87	513.39	1.54	513.39	1.54		.86	14.82	3.2	2.65		.51		YES
20.0	3.27		514.07	513.53	1.58	513.53	1.58		.89	14.91	3.2	2.71		.52		YES

NEBRASKA DEPARTMENT OF ROADS
Broken-Back Culvert Analysis Program (BCAP)

PROJECT INFO

Project: Camelot
Station or Location: Lewisville, TX
Date: 06/17/2011

CULVERT DATA

Discharge: 16.0 cfs
Shape: Circular
Material: Corr. Metal Pipe
Size: 1-2.0 ft x 2.0 ft
Inlet Type: Mitered to Conform to Slope

WATER SURFACE PROFILE

Inlet Depth: 1.41 ft
Inlet Velocity: 6.75 ft/s
Upper Break Depth: 1.19 ft
Upper Break Velocity: 8.24 ft/s
Lower Break Depth: 0.70 ft
Lower Break Velocity: 16.33 ft/s
Depth at End of Hydraulic Jump: 2.00 ft
Velocity at End of Hydraulic Jump: 14.48 ft/s
Depth at End of Hydraulic Jump: 2.45 ft
Velocity at End of Hydraulic Jump: 0.49 ft/s

OUTPUT DATA

Head Water Depth: 2.52 ft
Inlet Control Elevation: 513.32 ft
Break Control Elevation: 513.02 ft
Critical Depth: 1.41 ft
Tailwater Depth: 2.45 ft
Hydraulic Jump? YES
 Jump Station: 223.58 ft
 Jump Length: 15.64 ft
Outlet Depth: 0.77 ft
Outlet Velocity: 14.48 ft/s
Outlet Froude No.: 3.4

Circle Pipe Culvert

Inlet Type

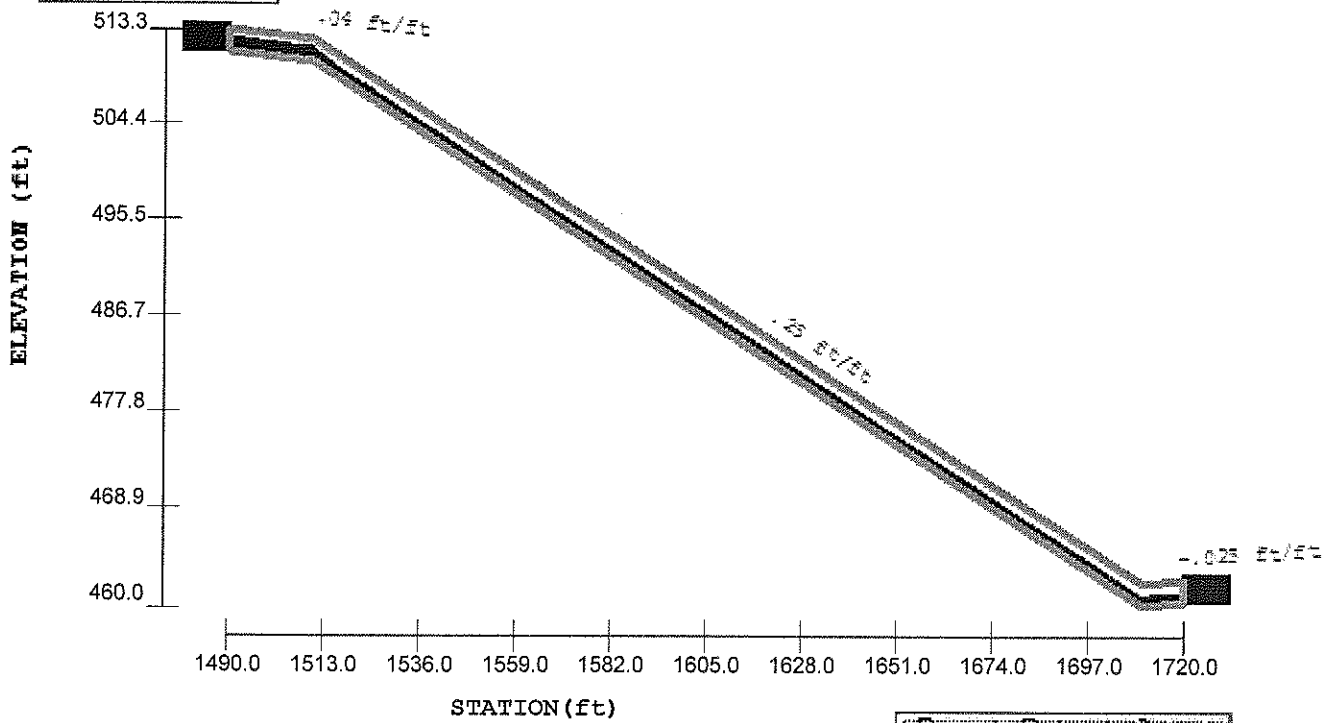
Diameter=2 ft

Mitered to Conform to Slope

Culvert Material: Corr. Metal Pipe Rough. Coeff.= 0.024

Outlet Sec. Rough. Coeff.= 0.024

Q = 16 cfs



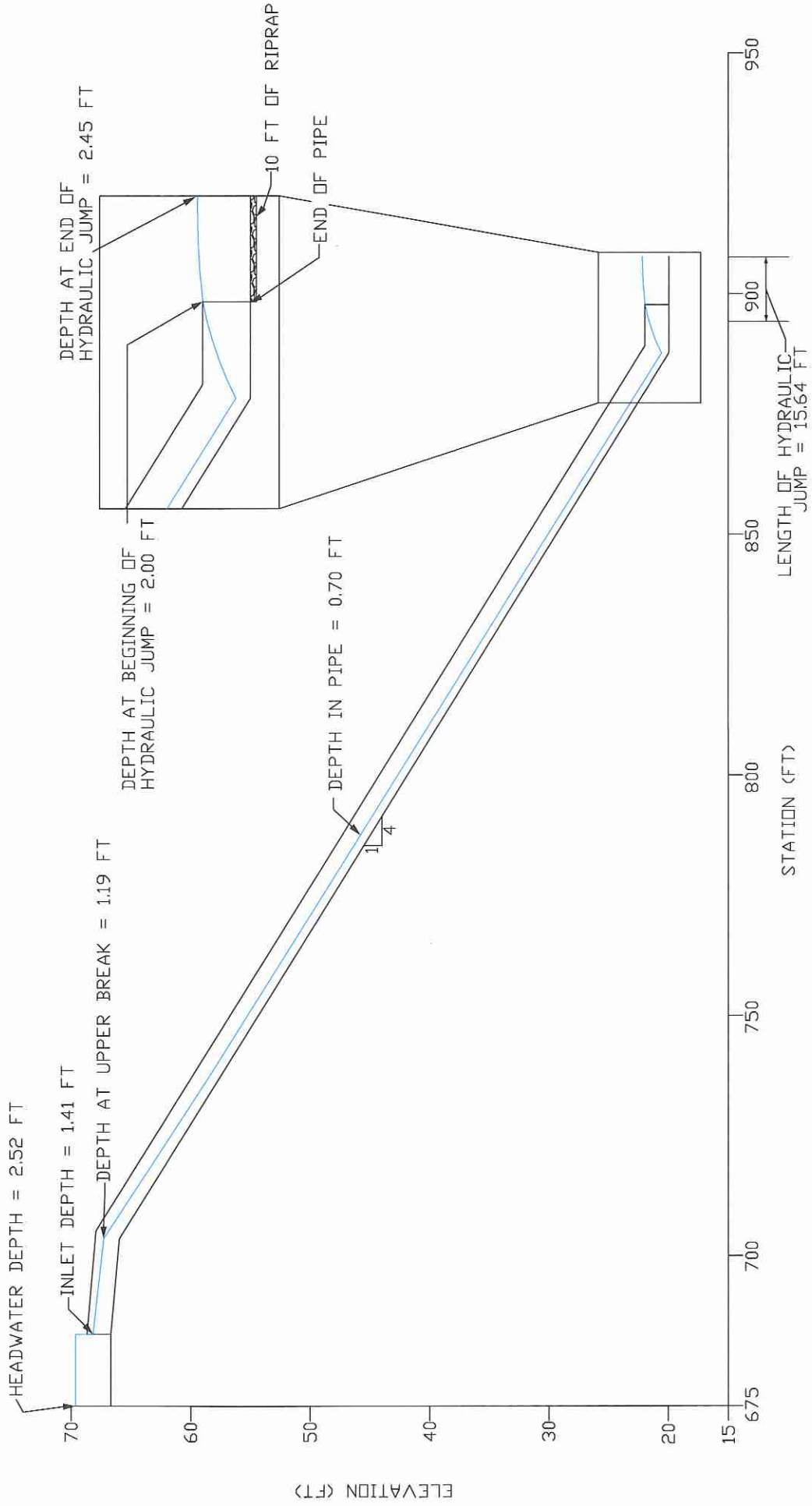
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IX IIF

WATER SURFACE PROFILE



IIIF-F-2-44

NEBRASKA DEPARTMENT OF ROADS
Broken-Back Culvert Analysis Program (BCAP)

PROJECT INFO

Project: Camelot
Station or Location: Lewisville, TX
Date: 06 / 17 / 2011

DISCHARGE DATA

Minimum: 20.00 cfs
Design Discharge: 21.00 cfs
Maximum: 30.00 cfs
Number of Barrels: 1

TAILWATER DATA

Type: Downstream
Channel Shape: Trapezoid
Left Side Slope: 3 H:1V
Right Side Slope: 3 H:1V
Bottom Width: 6 ft
Bottom Slope: 0.0001 ft/ft
Roughness Coefficient: 0.04

CULVERT DATA

Type: Circular Pipe
Pipe Diameter: 3 ft
Culvert Material: Corr. Metal Pipe
Inlet Type: Mitered to Conform to Slope
Roughness Coefficient: 0.024
Outlet Section Roughness Coeff.: 0.024
Inlet Section Slope: 0.04 ft/ft
Steep Section Slope: 0.25 ft/ft
Outlet Section Slope: -0.025 ft/ft

CULVERT PROFILE DATA

Type: Double Broken-Back
Inlet Station: 1490.00 ft
Inlet Elevation: 510.80 ft
Upper Break Station: 1510.00 ft
Upper Break Elevation: 510.00 ft
Lower Break Station: 1710.00 ft
Lower Break Elevation: 460.00 ft
Outlet Station: 1720.00 ft
Outlet Elevation: 460.25 ft

NEBRASKA DEPARTMENT OF ROADS
Broken-Back Culvert Analysis Program (BCAP)

Project:

Station or Location:

Date:

Camelot
Lewisville, TX
06/17/2011

Discharge	Headwater Depth	Inlet Control Elevation	Break Control Elevation	Critical Depth	Outlet Depth	Outlet Velocity	Outlet Froude Number	Tailwater Depth	Tailwater Velocity	Hydraulic Jump
cfs	ft	ft	ft	ft	ft	ft/s		ft	ft/s	
21.0	2.41	512.97	513.21	1.46	.72	16.10	4.1	2.77	.53	YES
22.0	2.45	513.03	513.25	1.50	.75	15.92	4.0	2.83	.54	YES
23.0	2.50	513.09	513.30	1.53	.77	16.19	4.0	2.89	.54	YES
24.0	2.54	513.15	513.34	1.56	.78	16.43	4.0	2.95	.55	YES
25.0	2.59	513.21	513.39	1.59	.80	16.67	4.0	3.01	.55	YES
26.0	2.63	513.27	513.43	1.63	.83	16.46	3.9	3.07	.56	YES
27.0	2.68	513.33	513.48	1.66	.85	16.39	3.8	3.11	.57	YES
28.0	2.73	513.39	513.53	1.69	.86	16.72	3.8	3.17	.57	YES
29.0	2.77	513.46	513.57	1.72	.87	17.04	3.9	3.23	.57	YES
30.0	2.82	513.52	513.62	1.75	.91	16.69	3.7	3.27	.58	YES

**NEBRASKA DEPARTMENT OF ROADS
Broken-Back Culvert Analysis Program (BCAP)**

PROJECT INFO

Project: Camelot
Station or Location: Lewisville, TX
Date: 06/17/2011

CULVERT DATA

Discharge: 21.0 cfs
Shape: Circular
Material: Corr. Metal Pipe
Size: 1-3.0 ft x 3.0 ft
Inlet Type: Mitered to Conform to Slope

WATER SURFACE PROFILE

Inlet Depth: 2.49 ft
Inlet Velocity: 3.35 ft/s
Upper Break Depth: 1.46 ft
Upper Break Velocity: 6.14 ft/s
Lower Break Depth: 0.69 ft
Lower Break Velocity: 17.10 ft/s
Depth at End of Hydraulic Jump: 2.77 ft
Velocity at End of Hydraulic Jump: 16.10 ft/s
Depth at End of Hydraulic Jump: 2.77 ft
Velocity at End of Hydraulic Jump: 0.53 ft/s

OUTPUT DATA

Head Water Depth: 2.41 ft
Inlet Control Elevation: 512.97 ft
Break Control Elevation: 513.21 ft
Critical Depth: 1.46 ft
Tailwater Depth: 2.77 ft
Hydraulic Jump? YES
 Jump Station: 222.06 ft
 Jump Length: 17.81 ft
Outlet Depth: 0.72 ft
Outlet Velocity: 16.10 ft/s
Outlet Froude No.: 4.1

Circle Pipe Culvert

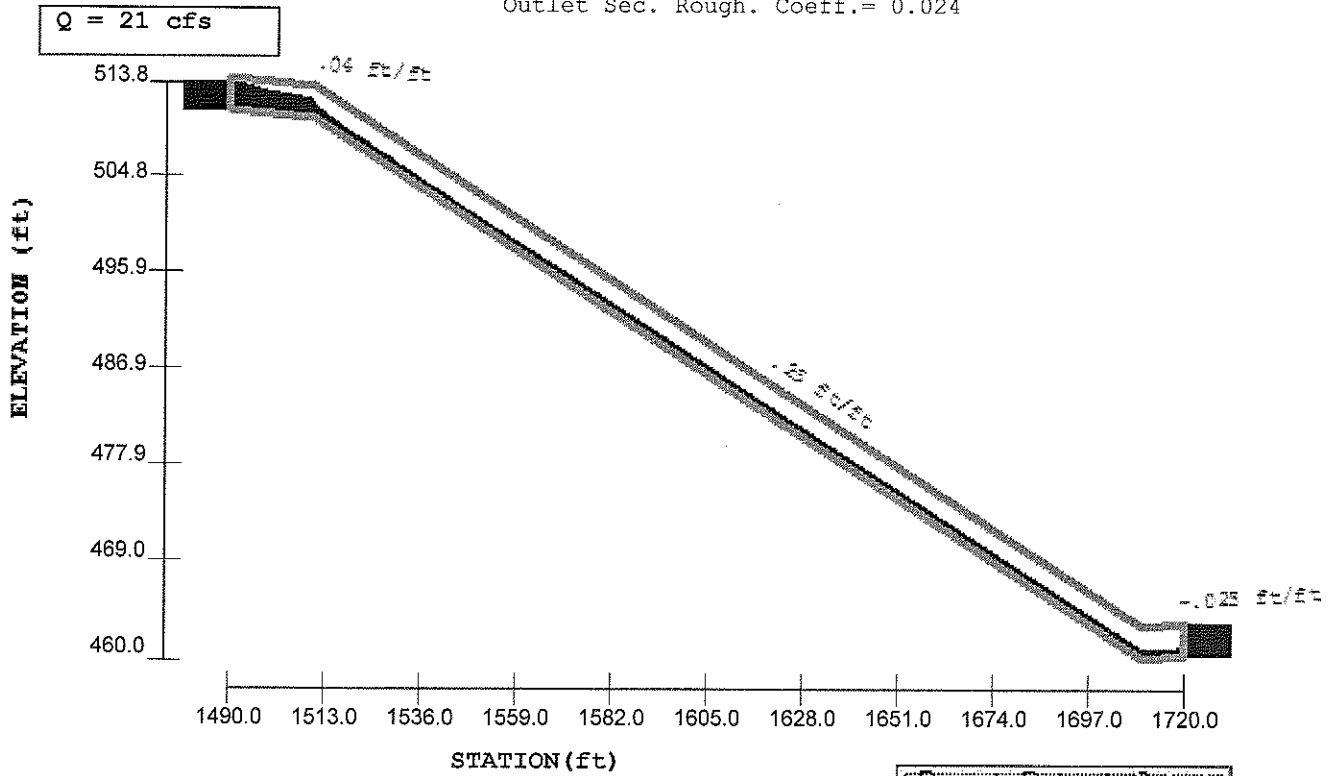
Diameter=3 ft

Culvert Material: Corr. Metal Pipe Rough. Coeff.= 0.024

Inlet Type

Mitered to Conform to Slope

Outlet Sec. Rough. Coeff.= 0.024



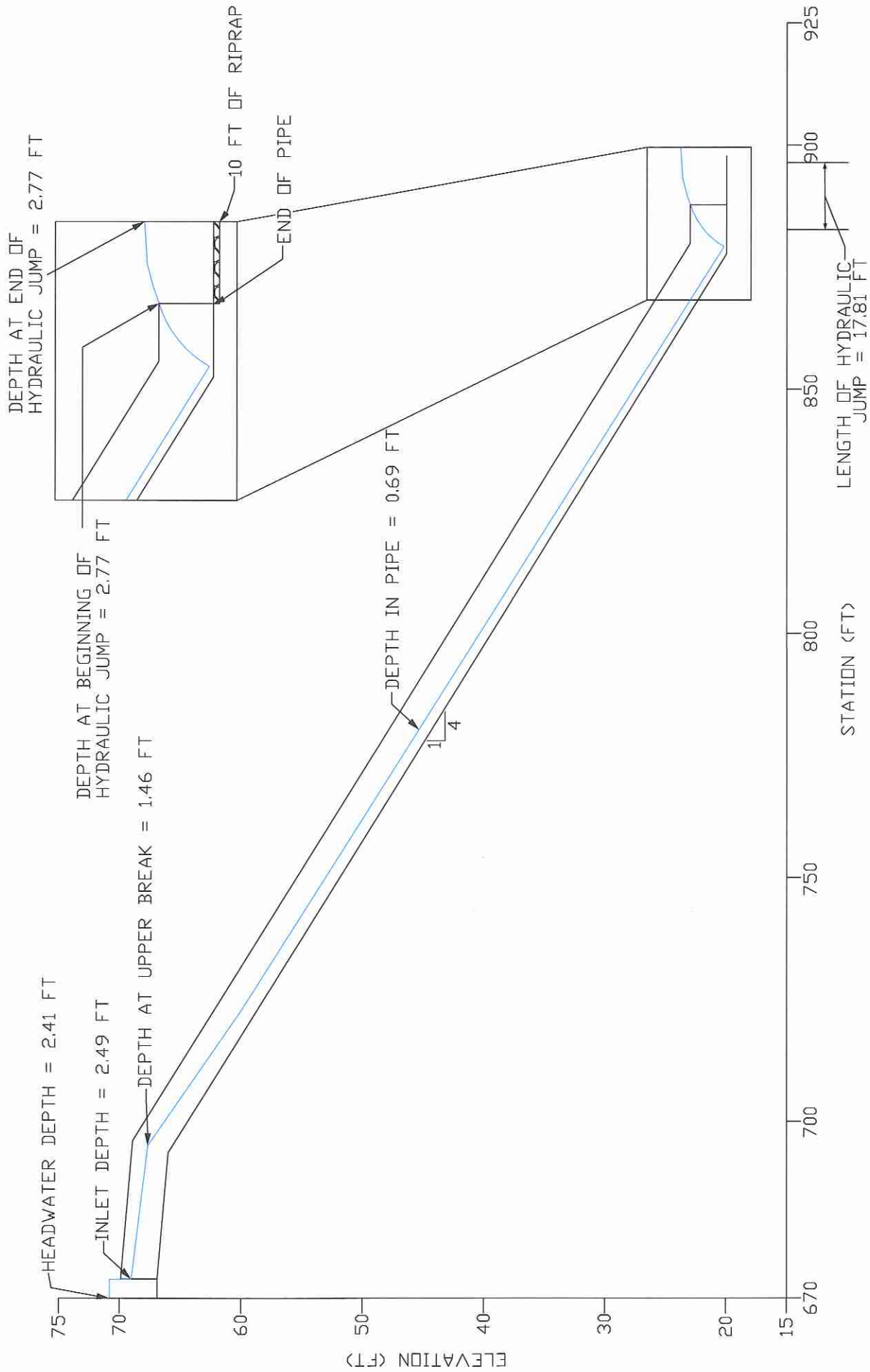
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IX IIII

WATER SURFACE PROFILE



2. Determine the maximum drainage areas for the flows calculated in Step 1.

$$Q = CIA$$

Where: C = 0.8 (runoff coefficient, Ref 1.)
I = intensity, in/hr
A = drainage area, ac

$$I = \frac{b}{(t_c + d)^e}$$

b = 90 From Ref. 1, for Denton County
d = 8.5 25-year storm event
e = 0.781
t_c is assumed to be 10 min.

$$I = 9.22 \text{ in/hr}$$

$$A = Q / (CI)$$

Pipe Diameter (in)	Flow (cfs)	Area (ac)
24	16.0	2.2
36	21.0	2.8

Conclusion:

The maximum allowable drainage area for a 24-inch diameter letdown pipe is 2.2 acres for each inlet and for a 36-inch diameter letdown pipe is 2.8 acres for each inlet. The minimum berm height is 3 feet for a 24-inch diameter pipe and 4 feet for 36-inch diameter pipe. (Figure 3 details indicate 1 foot berm above the pipe).

CAMELOT LANDFILL
1339-351-11-02
PIPE LETDOWN RIPRAP DESIGN

Required: Determine the Riprap size and Dimensions for 24-inch and 36-inch diameter letdown pipes using Riprap Apron Design provided by the Reference 1.

Method:

1. Determine the hydraulic conditions at the outlet of 24-inch and 36-inch diameter letdown pipes using the hydraulic design developed using the BCAP computer simulation.
2. Determine the riprap size and apron dimensions for each pipe letdown

Reference:

1. U.S. Department of Transportation - Federal Highway Administration. Hydraulic Engineering Circular No. 14, Third Edition. *Hydraulic Design of Energy Dissipators for Culverts and Channels*. Publication No. FHWA-NHI-06-086, July 2006.

Solution:

1. Determine the hydraulic parameters from pages IIF-F-2-42 (pipe diameter 24-inches) and IIF-F-2-47 (pipe diameter 36-inches):

Parameter	Symbol	24-inch Dia. Culvert	36-inch Dia. Culvert
Design flow rates, cfs	Q=	16.0	21.0
Pipe Diameters, ft	D=	2	3
Depth at the pipe outlet, ft	y _n =	0.77	0.72
Adjusted culvert rise, ft	D'=	1.385	1.86
Tailwater Depth ¹ , ft	TW=	2.00	3.00

¹Tailwater depth is the pipe diameter when the calculated tailwater depth is higher per Reference 1.

$$D_{50} = 0.2 \times D \left[\frac{Q}{\sqrt{g} \times D^{2.5}} \right]^{4/3} \times \left[\frac{D}{TW} \right] \quad \text{Eq. 10.4 (page 10-17 of Ref. 1)}$$

$$D' = \frac{D \times y_n}{2} \quad \text{Eq. 10.5 (page 10-17 of Ref. 1)}$$

D₅₀ = Riprap Size in feet

CAMELOT LANDFILL
1339-351-11-02
PIPE LETDOWN RIPRAP DESIGN

Riprap Classes and Apron Dimensions¹

Class	D ₅₀ (in)	Apron Length ² (ft)	Apron Depth (ft)
1	5	4xD	3.5xD ₅₀
2	6	4xD	3.3xD ₅₀
3	10	5xD	2.4xD ₅₀
4	14	6xD	2.2xD ₅₀
5	20	7xD	2.0xD ₅₀
6	22	8xD	2.0xD ₅₀

¹This table has been reproduced from Table 10.1 included on page 10-18 of Reference 1.

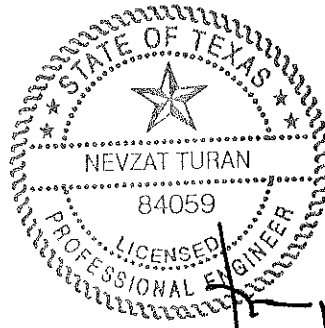
²D is the culvert rise.

Design Parameter	24-inch Dia. Culvert	36-inch Dia. Culvert
D ₅₀ , calculated, inches =	3.1	2.0
D ₅₀ , selected, inches =	5	5
Apron Length, calculated, feet =	5.54	7.44
Apron Length, selected, feet =	10	10
Apron Depth, calculated, inches =	17.5	17.5
Apron Depth, selected, inches =	18	18

Conclusion:

Riprap sizes for pipe diameters of 24-inches and 36-inches are selected conservatively. The calculated apron length is increased to 10 feet in the design. The apron depth used is higher than the calculated apron depth. Therefore, the design of the pipe letdown outlet energy dissipater calculations are acceptable and channels at the pipe outlets will be stable.

APPENDIX III F-F-3
SEDIMENT CONTROL POND DESIGN



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2-28-12

Includes Pages III F-F-3-1 through III F-F-3-7

SEDIMENT CONTROL POND DESIGN

This appendix includes supporting information for the sedimentation pond sizing procedure presented on Sheet III-F-12 (refer to Section 2.2 of the Erosion Control Plan for All Phases of Development). In the event that certain percent ground cover that limits the soil loss to 50/tons/acres/year is not achieved and soil loss is temporarily greater than 50 tons/acre/year, a sedimentation pond will be used along with other structural and non-structural BMPs approved as part of this plan to limit the discharge of eroded soil. The sedimentation pond option is a secondary erosion control option, similar to mulch, wood chips, compost, or straw/hay, and will only be used if the required percent vegetation specification is not met. If the sedimentation pond option is implemented, the swales and letdowns specified will remain in-place. The sedimentation pond option simply allows for the control of sediment while vegetation is being established. The pond design procedure has been developed for reducing discharge of eroded soil to less than the allowable amount for external side slopes (i.e., 50 tons/acre/year) if the required percent vegetation coverage is not obtained soil loss is greater than 50 tons/acre/year. The stormwater sedimentation pond design provided is for a 25-year frequency storm event. This provides for a conservative design because the efficiency of the pond will be higher for more frequent storms (e.g., one year frequency). The example calculation included on pages III-F-3-2 through III-F-3-6 demonstrates that a 0.5-acre detention pond is capable of reducing the discharge of 60 tons/acre/year of soil to less than 50 tons/acre/year of soil from the external slopes for a 20-acre area. A factor has been calculated that will be used to determine the required pond size for a specified external slope area. For a summary of the efficiencies of ponds for various required soil loss reduction amounts, refer to Sheet III-F-12 – Sediment Control Pond Plan as well as the table on page III-F-3-7.

Required: Develop a procedure to size a sedimentation pond to reduce sediment discharge from the external embankment area to 50 tons/acre/year or less.

Method:

1. Determine the 25-year frequency peak flow rate upstream of the sediment control pond using the Rational Method.
2. Calculate the settling velocity of sediment particles using Stokes equation.
3. Calculate the fraction of sediment trapped under dynamic conditions.
4. Calculate the fraction of sediment trapped under quiescent conditions.
5. Calculate the total fraction of sediment trapped under combined conditions.
6. Verify that pond design is adequate to reduce given soil loss to 50 tons/acre/year or less.

Reference:

1. State of Texas, Department of Transportation, Bridge Division, Hydraulic Manual, 3rd Edition, December 1985.
2. Chin, David. A. Water-Resources Engineering. Prentice Hall, Inc., 2000.
3. Haan, C.T., et al. Design Hydrology and Sedimentology for Small Catchments, 1994.
4. Cooperative Studies Section, Hydrologic Services Division. U.S. Department of Commerce. *Technical Paper No. 40*.

Solution:

1. Determine the 25-year frequency peak flow rate upstream of the sediment control pond.

$$Q = CIA$$

Where: C = 0.8 (runoff coefficient, Ref. 1)
I = intensity (in/hr)
A = upstream drainage area (ac)

Note: A runoff coefficient of 0.8 is used for all areas regardless of slope.

$$I = \frac{b}{(t_c + d)^e}$$

b = 90 From Ref. 1, for Denton County
d = 8.5 25-year frequency storm event
e = 0.781
t_c is assumed to be 10 min.

$$I = 9.22 \text{ in/hr}$$

$$A = 20.0 \text{ acres}$$

$$Q = 147.47 \text{ cfs}$$

2. Calculate the settling velocity, V_s (ft/hr), of sediment particles using Stokes equation.

$$V_s = \frac{\alpha (\rho_s / \rho_w - 1) g \phi^2}{18 \nu_w} \quad (\text{Ref. 2})$$

Where:

α = factor that measures the effect of particle shape (assume spherical, α = 1)
ρ_s = density of sediment particle (pcf)
ρ_w = density of ambient water (62.4 pcf)
g = gravity (32.2 ft/s²)
φ = particle diameter (ft)
ν_w = kinematic viscosity of the ambient water (ft²/s)

α = 1
ρ_s = 165 pcf
ν_w = 1.08E-05 ft²/s

Particle Class ¹	Percent in Class	Particle Diameter ² (ft)	Settling Velocity, V _s (ft/hr)
1	10	1.31E-05	0.17
2	20	1.97E-05	0.38
3	30	2.62E-05	0.68
4	20	3.28E-05	1.06
5	20	3.94E-05	1.52
Total	100		

¹ Particle class corresponds to particle diameter.

² Particle diameter ranges from 4μm to 12μm, which is typical for clay and silt particles.

3. Calculate the fraction of sediment trapped under dynamic conditions.

a. Determine the overflow rate.

$$V_o = Q/A_p \quad (\text{EPA Pond Performance Model from Ref. 3})$$

Where:

V_o = overflow rate

A_p = area of sediment control pond (ac)

Q = 147.47 cfs (from Step 2)

A_p = 0.50 acre

V_o = 24.38 ft/hr

b. Determine the fraction of sediment removed.

$$F = 1 - (1 + 1/\beta * V_o/V_s)^{-\beta} \quad (\text{Ref. 3})$$

Where:

F = single-storm trapping of sediment

β = turbulence or short-circuiting parameter reflecting non-ideal performance of pond (assume good performance, $\beta = 3$)

β = 3

$$D_R = L_F [(1/CV_Q^2) / (1/CV_Q^2 - \ln(E_m/L_F))]^{(1/CV_Q^2)+1} \quad (\text{Ref. 3})$$

Where:

D_R = long-term dynamic removal fraction for stormwater

L_F = removal ratio for very low flow rates

E_m = mean storm removal fraction

CV_Q = coefficient of variation of flows

L_F = 1

E_m = assume equals single-storm trapping, F

CV_Q = 1.74 (from Table 9B.1, p. 570, Ref. 3)

Table 1 - Summary for Dynamic Conditions

Particle Class	Percent in Class	Particle Diameter (ft)	Settling Velocity, V_s (ft/hr)	Single-storm Trapping, F	Fraction Removed Over All Storms, D_R	Fraction Captured Under Dynamic Conditions, E_D ¹
1	10	1.31E-05	0.17	0.007	0.025	0.25
2	20	1.97E-05	0.38	0.015	0.031	0.62
3	30	2.62E-05	0.68	0.027	0.037	1.11
4	20	3.28E-05	1.06	0.042	0.043	0.87
5	20	3.94E-05	1.52	0.060	0.050	1.00
Total	100					3.8

¹ E_D is the product of percent in class and D_R .

4. Calculate the fraction of sediment trapped under quiescent conditions.

$$RR = \frac{T_{IA} V_s A_Q}{V_R} \quad (\text{Ref. 3})$$

$$V_R = RA$$

Where:

- RR = removal ratio
- T_{IA} = average time interval between storms (hr)
- V_s = settling velocity (ft/hr) from Step 2
- A_Q = average surface area under quiescent conditions (ft²)
- V_R = mean runoff volume (ft³)
- R = runoff depth for 25-year, 24-hour storm (ft)
- A = upstream drainage area (ac)

A_Q = 21,780 ft² (assume equal to A_p)
 T_{IA} = 108 hrs (from Table 9B.1, p. 570 of Ref. 3)
 R = 0.61 ft (Ref. 4)
 A = 20.0 ac (from Step 1)

V_R = 529,980 ft³

Table 2 - Summary for Quiescent Conditions

Particle Class	Percent in Class	Settling Velocity, V _s (ft/hr)	Removal Ratio, RR (ft ³ /hr)	Effective Volume Ratio, V _E /V _R ¹	Fraction Removed Under Quiescent Conditions ²	Fraction Captured Under Quiescent Conditions, E _Q
1	10	0.17	0.75	0.120	0.12	1.20
2	20	0.38	1.69	0.130	0.12	2.40
3	30	0.68	3.00	0.140	0.13	3.90
4	20	1.06	4.68	0.145	0.14	2.80
5	20	1.52	6.74	0.150	0.15	3.00
Total	100					13.3

¹ Based on Figure 9.29 from Ref. 3, using RR and V_B/V_R.

V_B = reservoir volume = 87,120 ft³, assuming a 0.5-acre pond with an average depth of 4 feet.
 V_B/V_R = 0.164

² Based on Figure 9.30 from Ref. 3 with CV_R = 1.74.

5. Calculate the total fraction of sediment trapped under combined conditions, E_T.

$$E_T = 1 - (1 - E_D) * (1 - E_Q) \quad (\text{Ref. 3})$$

$$E_T = 16.6 \%$$

Refer to page III-F-3-7 for the total efficiency of ponds for different soil loss reduction amounts.

6. Verify that pond design is adequate to reduce given soil loss to 50 tons/acre/year or less.

a. Calculate net soil loss (i.e., sediment not captured by pond).

$$\begin{aligned} \text{Total Soil Loss} &= 60.0 \text{ tons/ac/yr} \\ E_T &= 16.6 \% \quad (\text{from Step 5}) \end{aligned}$$

$$\begin{aligned} \text{Net Soil Loss} &= \text{Total Soil Loss} \times (1 - E_T/100) \\ \text{Net Soil Loss} &= 50.0 \text{ tons/ac/yr} \end{aligned}$$

Refer to page III-F-3-7 for the net soil loss for different soil loss reduction amounts.

b. Calculate the required pond size per unit drainage area factor.

$$\text{Drainage Area} = 20.0 \text{ acres} \quad (\text{from Step 1})$$

$$\text{Pond Area} = 0.5 \text{ acres} \quad (\text{from Step 3})$$

$$\begin{aligned} \text{Required Pond Size /} \\ \text{Unit Drainage Area Factor} &= 0.025 \end{aligned}$$

This factor was calculated using a drainage area of 20 acres and a pond area of 0.5 acres. If a 40-acre drainage area drains to the pond, then a 1.0-acre pond will be required to achieve the above efficiency and net soil loss estimate (40 acres \times 0.025 = 1.0 acre). Refer to page III-F-3-7 for the required pond size/unit drainage area factor for different soil loss reduction amounts.

Conclusion:

A 0.5-acre pond will sufficiently capture enough sediment from a 20-acre drainage area so that no more than 50 tons/acre/year of net soil loss occurs on external embankment slopes. If the size of the drainage area changes, this procedure will need to be updated. Refer to the table on page III-F-3-7 for a summary of the pond efficiencies and net soil loss estimates for different soil loss reduction amounts.

SEDIMENT CONTROL POND SUMMARY

External Slope Area Soil Loss (Tons/Acre/Year)	Percent Efficiency of Pond (Dynamic Conditions)	Percent Efficiency of Pond (Quiescent Conditions)	Total Efficiency of Pond (%)	Net Soil Loss (Tons/Acre/Year)	Pond Area Required Per Unit Drainage Area ¹	50 Tons/Acre/Year or Less?
60	3.8	13.3	16.6	50.0	0.025	YES
70	4.6	25.5	28.9	49.8	0.040	YES
80	5.4	34.0	37.6	49.9	0.060	YES
90	6.0	41.5	45.0	49.5	0.075	YES
100	7.2	46.4	50.3	49.7	0.110	YES
200	13.3	71.2	75.0	49.9	0.300	YES

¹ This factor multiplied by a given drainage area will give the required pond size to achieve the efficiencies shown in the table.